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Supplement of

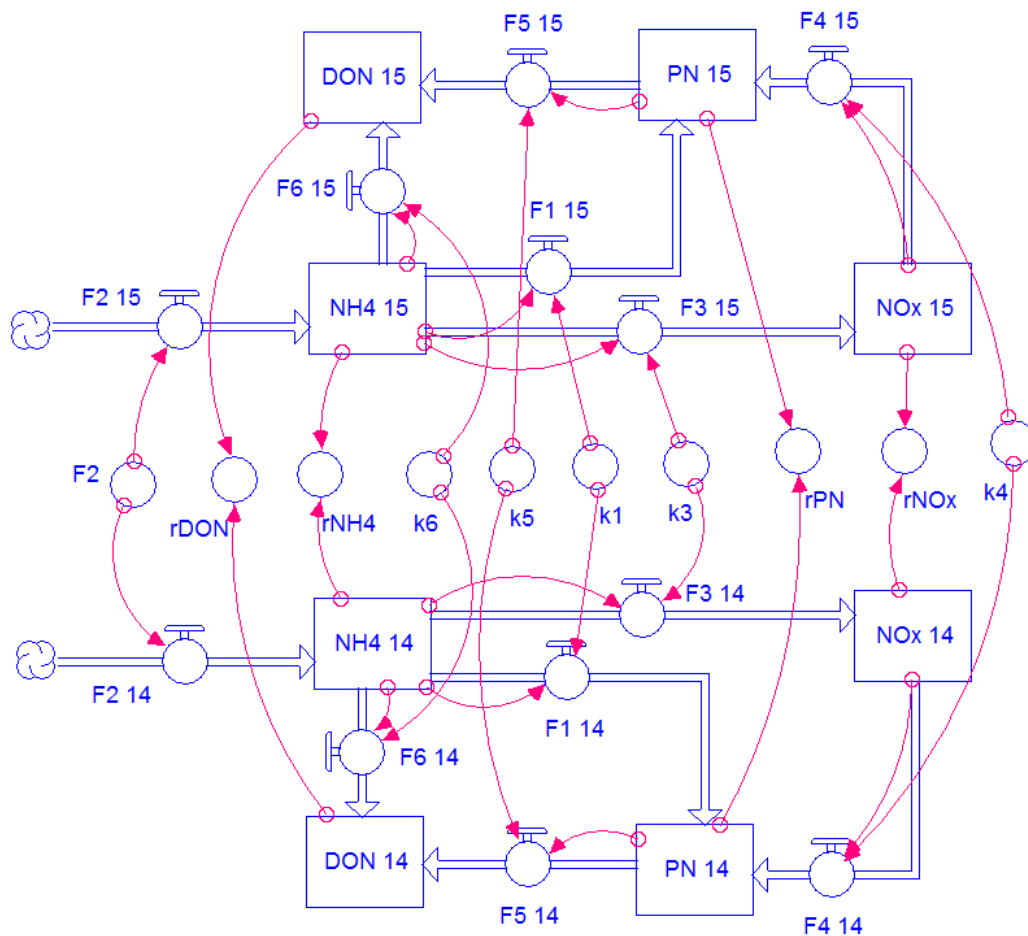
Quantification of multiple simultaneously occurring nitrogen flows in the euphotic ocean

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Figure S1. Structure of the equation based STELLA box model (Version 9.14) for the low nutrient case. Square represents pool. Pools of NH_4^+ , NO_x^- and PN were separated into two modules (i.e., ^{14}N and ^{15}N). Faucet (F_i , $i = 1\sim 6$, was for N process rate) stands for regulator controlled by associated arrows determined by rate constant (k_i , $i = 1\sim 6$) and reactant concentration. Fractionation between ^{14}N and ^{15}N was not considered, thus, k_i is the same for both ^{14}N and ^{15}N . The output, r , stands for the ratio of ^{15}N to $^{14}\text{N}+^{15}\text{N}$ derived from instantaneous ^{15}N and ^{14}N amounts in pools. Exported equations were shown below.



Low nutrient case Equations:

$$\text{DON}_{14}(t) = \text{DON}_{14}(t - dt) + (F6_{14} + F5_{14}) * dt$$

$$\text{INIT DON}_{14} = 5376.4$$

INFLOWS:

$$F6_{14} = k6 * \text{NH4}_{14}$$

$$F5_{14} = k5 * \text{PN}_{14}$$

$$\text{DON}_{15}(t) = \text{DON}_{15}(t - dt) + (F5_{15} + F6_{15}) * dt$$

$$\text{INIT DON}_{15} = 19.8$$

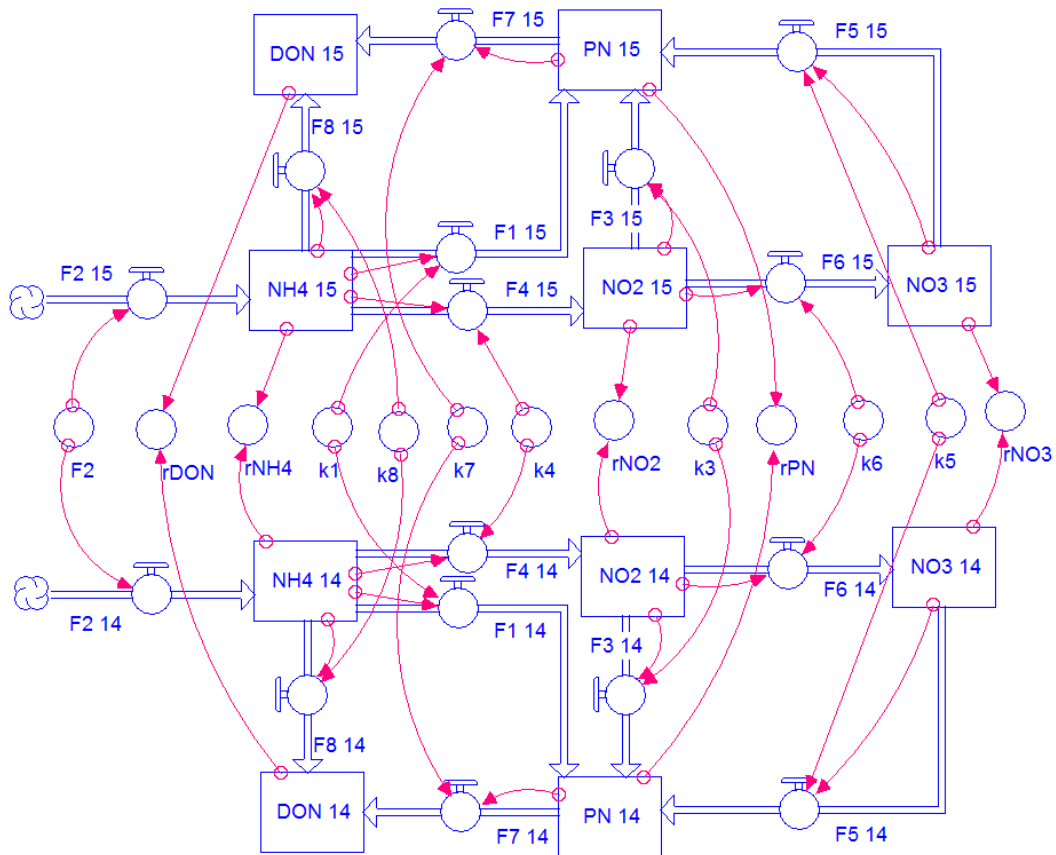
INFLOWS:

$$F5_{15} = \text{PN}_{15} * k5$$

$F6_{15} = NH4_{15} * k6$
 $NH4_{14}(t) = NH4_{14}(t - dt) + (F2_{14} - F6_{14} - F1_{14} - F3_{14}) * dt$
 INIT $NH4_{14} = 112.9$
 INFLOWS:
 $F2_{14} = F2 * (1 - 0.00366)$
 OUTFLOWS:
 $F6_{14} = k6 * NH4_{14}$
 $F1_{14} = k1 * NH4_{14}$
 $F3_{14} = k3 * NH4_{14}$
 $NH4_{15}(t) = NH4_{15}(t - dt) + (F2_{15} - F3_{15} - F1_{15} - F6_{15}) * dt$
 INIT $NH4_{15} = 29.8$
 INFLOWS:
 $F2_{15} = F2 * 0.00366$
 OUTFLOWS:
 $F3_{15} = NH4_{15} * k3$
 $F1_{15} = NH4_{15} * k1$
 $F6_{15} = NH4_{15} * k6$
 $NOx_{14}(t) = NOx_{14}(t - dt) + (F3_{14} - F4_{14}) * dt$
 INIT $NOx_{14} = 518.8$
 INFLOWS:
 $F3_{14} = k3 * NH4_{14}$
 OUTFLOWS:
 $F4_{14} = k4 * NOx_{14}$
 $NOx_{15}(t) = NOx_{15}(t - dt) + (F3_{15} - F4_{15}) * dt$
 INIT $NOx_{15} = 1.9$
 INFLOWS:
 $F3_{15} = NH4_{15} * k3$
 OUTFLOWS:
 $F4_{15} = NOx_{15} * k4$
 $PN_{14}(t) = PN_{14}(t - dt) + (F4_{14} + F1_{14} - F5_{14}) * dt$
 INIT $PN_{14} = 435.1$
 INFLOWS:
 $F4_{14} = k4 * NOx_{14}$
 $F1_{14} = k1 * NH4_{14}$
 OUTFLOWS:
 $F5_{14} = k5 * PN_{14}$
 $PN_{15}(t) = PN_{15}(t - dt) + (F4_{15} + F1_{15} - F5_{15}) * dt$
 INIT $PN_{15} = 1.7$
 INFLOWS:
 $F4_{15} = NOx_{15} * k4$
 $F1_{15} = NH4_{15} * k1$
 OUTFLOWS:
 $F5_{15} = PN_{15} * k5$

$rDON = DON_{15} / (DON_{14} + DON_{15})$
 $rNH4 = NH4_{15} / (NH4_{14} + NH4_{15})$
 $rNOx = NOx_{15} / (NOx_{14} + NOx_{15})$
 $rPN = PN_{15} / (PN_{14} + PN_{15})$

Figure S2. The STELLA model (Version 9.14) for high nutrient case. The F_i ($i = 1\sim 8$) indicates rate of the relevant N process controlled by multiplying rate constant (k_i , $i = 1\sim 8$) with substrate concentration. Similar to low nutrient case, NH_4^+ , NO_2^- , NO_3^- and PN pools were separated into two modules (i.e., ^{14}N and ^{15}N). Exported equations were shown below the figure.



High nutrient case equations (e.g. 80%PAR case):

$$\text{DON}_{14}(t) = \text{DON}_{14}(t - dt) + (F8_{14} + F7_{14}) * dt$$

$$\text{INIT DON}_{14} = 17.39$$

INFLOWS:

$$F8_{14} = k8 * \text{NH4}_{14}$$

$$F7_{14} = k7 * \text{PN}_{14}$$

$$\text{DON}_{15}(t) = \text{DON}_{15}(t - dt) + (F7_{15} + F8_{15}) * dt$$

$$\text{INIT DON}_{15} = 0.064$$

INFLOWS:

$$F7_{15} = k7 * \text{PN}_{15}$$

$$F8_{15} = k8 * \text{NH4}_{15}$$

$$\text{NH4}_{14}(t) = \text{NH4}_{14}(t - dt) + (F2_{14} - F8_{14} - F1_{14} - F4_{14}) * dt$$

$$\text{INIT NH4}_{14} = 25.54$$

INFLOWS:

$$F2_{14} = F2 * (1 - 0.00366)$$

OUTFLOWS:

$$F8_{14} = k8 * \text{NH4}_{14}$$

$$F1_{14} = k1 * \text{NH4}_{14}$$

$F4_14 = k4 * NH4_14$
 $NH4_15(t) = NH4_15(t - dt) + (F2_15 - F4_15 - F8_15 - F1_15) * dt$
 INIT NH4_15 = 1.09
 INFLOWS:
 $F2_15 = F2 * 0.00366$
 OUTFLOWS:
 $F4_15 = k4 * NH4_15$
 $F8_15 = k8 * NH4_15$
 $F1_15 = k1 * NH4_15$
 $NO2_14(t) = NO2_14(t - dt) + (F4_14 - F6_14 - F3_14) * dt$
 INIT NO2_14 = 5.56
 INFLOWS:
 $F4_14 = k4 * NH4_14$
 OUTFLOWS:
 $F6_14 = k6 * NO2_14$
 $F3_14 = k3 * NO2_14$
 $NO2_15(t) = NO2_15(t - dt) + (F4_15 - F6_15 - F3_15) * dt$
 INIT NO2_15 = 0.020
 INFLOWS:
 $F4_15 = k4 * NH4_15$
 OUTFLOWS:
 $F6_15 = k6 * NO2_15$
 $F3_15 = k3 * NO2_15$
 $NO3_14(t) = NO3_14(t - dt) + (F6_14 - F5_14) * dt$
 INIT NO3_14 = 30.02
 INFLOWS:
 $F6_14 = k6 * NO2_14$
 OUTFLOWS:
 $F5_14 = k5 * NO3_14$
 $NO3_15(t) = NO3_15(t - dt) + (F6_15 - F5_15) * dt$
 INIT NO3_15 = 0.11
 INFLOWS:
 $F6_15 = k6 * NO2_15$
 OUTFLOWS:
 $F5_15 = k5 * NO3_15$
 $PN_14(t) = PN_14(t - dt) + (F5_14 + F1_14 + F3_14 - F7_14) * dt$
 INIT PN_14 = 8.72
 INFLOWS:
 $F5_14 = k5 * NO3_14$
 $F1_14 = k1 * NH4_14$
 $F3_14 = k3 * NO2_14$
 OUTFLOWS:
 $F7_14 = k7 * PN_14$
 $PN_15(t) = PN_15(t - dt) + (F5_15 + F3_15 + F1_15 - F7_15) * dt$
 INIT PN_15 = 0.032
 INFLOWS:
 $F5_15 = k5 * NO3_15$
 $F3_15 = k3 * NO2_15$
 $F1_15 = k1 * NH4_15$
 OUTFLOWS:
 $F7_15 = k7 * PN_15$
 $rDON = DON_15 / (DON_14 + DON_15)$
 $rNH4 = NH4_15 / (NH4_14 + NH4_15)$
 $rNO2 = NO2_15 / (NO2_14 + NO2_15)$
 $rNO3 = NO3_15 / (NO3_14 + NO3_15)$
 $rPN = PN_15 / (PN_14 + PN_15)$

Figure S3. The temporal variations of pico-eukaryote and *Synechococcus* in the low-nutrient incubations.

