

Normalized productivity response	Region	ln SOC 0–20 cm (%)	ln N stock 0–20 cm (g m <sup>-2</sup> )	Soil C : N ratio 0–20 cm	ln soil C : N ratio 0–10 cm	Mineral soil sand (%)	Mineral soil clay (%)	ln TEB stock 0–20 cm (cmol <sub>+</sub> m <sup>-2</sup> )	pH <sub>KCl</sub> 0–20 cm
Residual MAI (method 1)	N (n = 542)	quad = -0.16 ± 0.02 P < 0.01 lin = 0.49 ± 0.08 P < 0.01 intercept = -0.19 ± 0.08 P = 0.03 R <sup>2</sup> <sub>tot</sub> = 0.145	slope = 0.29 ± 0.06 P < 0.01 intercept = -1.5 ± 0.3 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.012	slope = -0.014 ± 0.004 P < 0.01 intercept = 0.3 ± 0.1 P < 0.01 R <sup>2</sup> = 0.021	n/a	slope = 0.003 ± 0.001 P = 0.01 intercept = -0.2 ± 0.1 P = 0.03 R <sup>2</sup> <sub>tot</sub> = 0.008	slope = 0.009 ± 0.004 P = 0.02 intercept = -0.05 ± 0.03 P = 0.14 R <sup>2</sup> <sub>tot</sub> = 0.002	P = 0.11	quad = -0.71 ± 0.06 P < 0.01 lin = 5.3 ± 0.4 P < 0.01 intercept = -9.7 ± 0.9 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.099
	M (n = 777)	quad = -0.16 ± 0.02 P < 0.01 lin = 0.35 ± 0.08 P < 0.01 intercept = -0.03 ± 0.08 P = 0.71 R <sup>2</sup> <sub>tot</sub> = 0.145	slope = 0.29 ± 0.06 P < 0.01 intercept = -1.5 ± 0.3 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.012	slope = -0.027 ± 0.005 P < 0.01 intercept = 0.7 ± 0.2 P < 0.01 R <sup>2</sup> = 0.029	n/a	slope = 0.003 ± 0.001 P = 0.01 intercept = -0.23 ± 0.09 P = 0.01 R <sup>2</sup> <sub>tot</sub> = 0.008	slope = 0.009 ± 0.004 P = 0.02 intercept = -0.05 ± 0.03 P = 0.14 R <sup>2</sup> <sub>tot</sub> = 0.002	P = 0.11	quad = -0.71 ± 0.06 P < 0.01 lin = 5.6 ± 0.4 P < 0.01 intercept = -10.8 ± 0.8 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.099
	S (n = 946)	quad = -0.16 ± 0.02 P < 0.01 lin = 0.19 ± 0.09 P = 0.03 intercept = 0.5 ± 0.1 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.145	slope = 0.29 ± 0.06 P < 0.01 intercept = -1.5 ± 0.3 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.012	slope = -0.082 ± 0.007 P < 0.01 intercept = 2.0 ± 0.2 P < 0.01 R <sup>2</sup> = 0.112	n/a	slope = 0.003 ± 0.001 P = 0.01 intercept = 0.00 ± 0.08 P = 0.98 R <sup>2</sup> <sub>tot</sub> = 0.008	slope = 0.009 ± 0.004 P = 0.02 intercept = -0.05 ± 0.03 P = 0.14 R <sup>2</sup> <sub>tot</sub> = 0.002	P = 0.11	quad = -0.71 ± 0.06 P < 0.01 lin = 5.9 ± 0.4 P < 0.01 intercept = -11.5 ± 0.8 P < 0.01 R <sup>2</sup> <sub>tot</sub> = 0.099
Actual / attainable MAI (method 2)	All of Sweden (n = 955)	quad = -2.6 ± 0.4 P < 0.01 lin = 11 ± 2 P < 0.01 intercept = 32 ± 2 P < 0.01 R <sup>2</sup> = 0.048	slope = 10.7 ± 0.8 P < 0.01 intercept = -18 ± 5 P < 0.01 R <sup>2</sup> = 0.146	n/a	slope = -19 ± 5 P < 0.01 intercept = 100 ± 5 P < 0.01 R <sup>2</sup> = 0.131	slope = -0.04 ± 0.02 P = 0.01 intercept = 42 ± 1 P < 0.01 R <sup>2</sup> = 0.005	slope = 0.18 ± 0.06 P < 0.01 intercept = 39.2 ± 0.6 P < 0.01 R <sup>2</sup> = 0.008	slope = 2.0 ± 0.5 P < 0.01 intercept = 32 ± 2 P < 0.01 R <sup>2</sup> = 0.014	slope = 3 ± 1 P < 0.01 intercept = 29 ± 4 P < 0.01 R <sup>2</sup> = 0.009