

**Temperature effects on respiration and sinking rate**

M. H. Iversen and  
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**Temperature effects on carbon-specific respiration rate and sinking velocity of diatom aggregates – potential implications for deep ocean export processes**

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## Abstract

Most deep ocean carbon flux profiles show low and almost constant fluxes of particulate organic carbon (POC) in the deep ocean. However, the reason for the seemingly non-changing POC fluxes at depths is unknown. This study presents direct measurements of formation, degradation, and sinking velocity of diatom aggregates from laboratory studies performed at 15 °C and 4 °C during a three week experiment. The average carbon-specific respiration rate during the experiment was  $0.12 \pm 0.03$  at 15 °C, and decreased 3.5-fold when the temperature was lowered to 4 °C. No direct influence of temperature on aggregate sinking speed was observed. Using the remineralisation rate measured at 4 °C and an average particle sinking speed of  $150 \text{ m d}^{-1}$ , calculated carbon fluxes were similar to those collected in deep ocean sediment traps from a global data set, indicating that temperature plays a major role for deep ocean fluxes of POC.

## 1 Introduction

Macroscopic aggregates with diameters larger than 0.5 mm are known as marine snow and form from detritus, living organisms, and inorganic matter in both coastal zones and the open ocean (Alldredge and Silver, 1988). Sedimentation of marine snow and fecal pellets drives the export of organic matter from the surface to the deep ocean (Fowler and Knauer, 1986; Asper, 1987) and often occurs at sinking velocities exceeding  $100 \text{ m d}^{-1}$  (e.g. Alldredge and Gotschalk, 1988; Diercks and Asper, 1997; Asper and Smith, 2003). This is termed “the biological pump” (Volk and Hoffert, 1985), which is characterized by continuous consumption and remineralisation of the settling aggregates, resulting in high attenuation of carbon fluxes with increasing depth (e.g. Martin et al., 1987). The efficiency of the biological pump is mainly determined by aggregate sinking velocities and degradation rates of the organic material within settling aggregates, with high export when sinking velocities are high and/or degradation rates are low.

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Remineralisation of particulate organic carbon (POC) by heterotrophic organisms in the ocean is high, and often more than 90 % of the produced POC is respired and solubilized before settling through the euphotic zone (Hedges, 1992). Generally, there is strong attenuation of POC fluxes within the upper hundreds of metres in the open ocean, while the carbon fluxes at greater depths appear low and constant (Suess, 1980; Martin et al., 1987; Iversen et al., 2010). This indicates low remineralisation rates and/or increasing aggregate sinking velocities with depth. However the importance of sinking velocity versus remineralisation for the POC fluxes at depth is still unclear.

Zooplankton concentrations decrease with increasing depth, suggesting microbial degradation is the main degradation mechanism of settling aggregates in the deep ocean (Stemmann et al., 2004). Aggregate-associated microbes are exposed to high pressure and low temperature in the deep ocean compared to the surface ocean. Exposing shallow water adapted bacterial strains to hydrostatic pressure equivalent to 4000 m reduces the abundance, cell size, and activity for some strains while others seem to have physiological pressure adaptations (Grossart and Gust, 2009; Tamburini et al., 2009; Nagata et al., 2010). Such adaptations might explain observations of living, active surface-ocean adapted, particle-associated bacteria at 6000 m depth. (Eloe et al., 2011). Recent studies have observed limited exchange between aggregate-attached and free-living microbes through the water column (Delong et al., 2006; AristeGUI et al., 2009). This supports laboratory observations of bacteria which became permanently attached to aggregates after becoming embedded in the matrix within aggregates (Kjørboe et al., 2002). Therefore, a large fraction of the aggregate-associated microbial community at depth may be made up by surface-ocean adapted microorganisms embedded within the aggregates.

Studies of the influence of elevated temperature on microbial activity showed increased microbial degradation of organic matter when exposing microbes to temperatures higher than their natural range (Hoppe et al., 2008; Piontek et al., 2009). However, data for the influence of low temperature on the activity of particle-attached, surface-ocean adapted microbes sinking to the deep ocean is limited, though this knowledge

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would greatly improve our understanding of deep ocean carbon fluxes. While pressure increases linearly with depth, temperature changes often occur over steep gradients in the upper few hundred meters at low- and mid-latitudes. This results in rapid temperature transitions over short times scales for aggregate-associated microbes sinking with 100 m per day or more, and, thus, transported from, e.g. 15 °C to 4 °C within days. Therefore, direct studies of how a rapid temperature transition from 15 °C to 4 °C affects aggregate dynamics, activity of attached microbial, and aggregate sinking velocity are needed.

In the present study, we directly measured size-specific formation, degradation and sinking velocity of diatom aggregates over three weeks at 15 °C and 4 °C. Size, respiration rate, and sinking velocity of individual aggregates were measured in a vertical flow system in which aggregate sinking velocity was balanced by an upward-directed flow velocity. The fluid motion and solute distribution in the vicinity of the aggregates under these experimental conditions were equivalent to those in the vicinity of an aggregate sinking through the water column at a velocity equal to the water flow velocity (Kjørboe et al., 2001). The oxygen fluxes to such sinking aggregates were calculated from O<sub>2</sub> concentration gradients measured at the aggregate-water interface using an O<sub>2</sub>-microsensor. These methods are non-destructive to the aggregates, which were afterwards collected for dry mass, POC, and PON analysis. We used our obtained laboratory data to calculate potential carbon fluxes in the deep cold ocean and compared them with those obtained from sediment traps in a global data set.

## 2 Material and methods

### 2.1 Algae cultures

Cultures of the diatom *Skeletonema costatum* (North Sea) were grown at 15 °C in 0.2 µm filtered seawater (salinity 32) enriched with nutrients according to f/2 medium (Guillard, 1975) with silicate added at a molar ratio of silicate to nitrate of 1. The cultures

were kept in a 12-h light period at  $150 \mu\text{mol photons m}^{-2} \text{s}^{-1}$ , and allowed a growth period of 13 days, when stationary growth phase was reached.

## 2.2 Aggregate formation

The diatom cultures were diluted with GF/F filtered seawater (salinity 32) to a final concentration of  $3 \times 10^5 \text{ cells mL}^{-1}$  and incubated in 1.15 L Plexiglas roller tanks with diameters of 14 cm and depths of 7.47 cm to form aggregates. In total, 20 roller tank incubations were rotated on rolling tables at 3 rotations per minute (rpm) at  $15^\circ\text{C}$  in darkness. After three days of incubation, the temperature was lowered to  $4^\circ\text{C}$  for half of the roller tanks to imitate a rapid settling to the colder waters of the deep ocean. The aggregate dynamics were followed throughout the study by counting the aggregates within different size classes in each roller tank.

## 2.3 Sinking velocity

Individual aggregates were gently transferred with a wide bore pipette from the roller tanks to a vertical flow system where the sinking velocity of each aggregate was measured (Ploug and Jørgensen, 1999; Ploug et al., 2010). The water in the vertical flow system was similar to the water in the roller tanks (GF/F filtered seawater, salinity 32), and the water temperature was adjusted accordingly to the treatment ( $15$  or  $4^\circ\text{C}$ ). The flow was adjusted with a needle valve until the aggregate remained suspended at a distance of one aggregate diameter above the net, whereby the aggregate sinking velocity was balanced by the upward-directed seawater flow velocity (Ploug et al., 2010). The sinking velocity of an aggregate was calculated from the flow rate divided by the cross-sectional area of the flow chamber. Triplicate measurements of sinking velocity were made for each aggregate. The length of all three aggregate axes ( $x$ ,  $y$ , and  $z$  direction) was measured in the flow system using a horizontal dissection microscope with a calibrated ocular. The aggregate volume was calculated by assuming an ellipsoid shape.

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For comparison with other aggregate shapes we calculated the equivalent spherical diameter (ESD) of each aggregate.

## 2.4 Oxygen measurements

Oxygen gradients at the aggregate-water interface were measured using a Clark-type oxygen microelectrode with a guard cathode (Revsbech, 1989) mounted in a micro-manipulator and calibrated at air-saturation and at anoxic conditions. The electrode current was measured on a picoamperemeter (Unisense, PA2000) and read on a strip chart recorder (Kipp and Zonen) at high resolution ( $2 \mu\text{M O}_2 \text{ cm}^{-1}$ ). The tip diameter of the microsensor was  $2 \mu\text{m}$ . The relative distance between the microelectrode tip and the aggregate surface was measured using a dissection microscope with a calibrated ocular micrometer. The 90 % response time of the electrode was  $< 1 \text{ s}$  and the stirring sensitivity  $< 0.3\%$ . The aggregates were suspended by an upward-directed flow that balanced the aggregate's sinking velocity in the same vertical net-jet flow system as used for estimating sinking velocities (Ploug and Jørgensen, 1999). All measurements were done at steady state of the oxygen gradients. The water in the flow system was similar to the water in the roller tanks ( $0.2 \mu\text{m}$  filtered sea water at  $15$  or  $4^\circ\text{C}$  with a salinity of 32).

## 2.5 Calculations of respiration rates

Oxygen fluxes and respiration rates were calculated from the oxygen gradients measured at the aggregate-water interface under steady-state. The analytical solutions for oxygen distribution and diffusive fluxes at the aggregate-water interface were fitted to measured values by applying the solver routine of the spreadsheet program Excel version 2003 (Microsoft) as previously described (Ploug et al., 1997). We used temperature and salinity corrected oxygen diffusion coefficients of  $1.22 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$  for  $4^\circ\text{C}$  and  $1.72 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$  for  $15^\circ\text{C}$  in the calculations (Broecker and Peng, 1974). The surface area of ellipsoids (Maas, 1994) was used to calculate total oxygen

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consumption. Oxygen consumption rate was converted to carbon respiration assuming a respiratory quotient of 1.2 molO<sub>2</sub> to 1 molCO<sub>2</sub>, as also used in previous studies of O<sub>2</sub> respiration and POC degradation in diatom aggregates (e.g. Ploug and Grossart, 2000; Iversen et al., 2010; Iversen and Ploug, 2010).

## 5 2.6 Aggregate dry weight and particulate organic carbon and nitrogen content

The aggregate dry weight (DW) was determined by filtering single aggregates with known volumes onto pre-weighed 0.4-μm polycarbonate filters. Each filter contained one aggregate, which was gently washed with de-ionized water, to remove salt, and dried at 60 °C for 48 h before weighing on a Mettler Toledo (UMX 2) scale with a sensitivity of 0.1 μg.

The ratio of particulate organic carbon (POC) to DW was determined by filtering ~50 aggregates onto pre-weighed 25 mm GF/F filters. The filters were gently rinsed with de-ionized water, and dried at 40 °C for 48 h before being re-weighed on a Mettler Toledo UMX2 balance (sensitivity: 0.1 μg). POC and PON contents of the aggregates on each filter were measured on an EA mass spectrometer (ANCA-SL 20-20, Sercon Ltd. Crewe, UK) with a precision of ±0.7 μgC or 0.3%. At each time point, when measurements were performed, a POC to DW ratio and a POC to PON ratio were calculated for the measured treatment. This was calculated by dividing the amount of POC by the DW of the material on each filter and used to estimate POC content within measured aggregate by multiplying its DW by the POC:DW ratio for that aggregate treatment and time point.

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## 2.7 Density of aggregates

We used the Navier–Stokes drag equation to calculate the excess density ( $\Delta\rho$ ) of our aggregates (Stokes, 1851):

$$\Delta\rho = \frac{C_D\rho_w w^2}{\frac{4}{3}gESD} \quad (1)$$

5 where  $C_D$  is the dimensionless drag force defined in Eq. (1),  $\rho_w$  is the density of sea water (1.0237 and 1.0254 g cm<sup>-3</sup>, for a salinity of 32 at 15 and 4 °C, respectively),  $w$  is the measured sinking velocity in cm s<sup>-1</sup>,  $g$  is the gravitational acceleration of 981 cm s<sup>-2</sup>, and  $ESD$  is the equivalent spherical diameter in cm. We calculated  $C_D$  using the drag equation for  $Re > 1$  given by White (1974):

$$10 C_D = \left(\frac{24}{Re}\right) + \left(\frac{6}{1 + Re^{0.5}}\right) + 0.4 \quad (2)$$

where Reynolds number ( $Re$ ) was defined as:

$$Re = wESD\frac{\rho_w}{\eta} \quad (3)$$

where  $\eta$  is the dynamic viscosity (1.2158 × 10<sup>-2</sup> and 1.6498 × 10<sup>-2</sup> g cm<sup>-1</sup> s<sup>-1</sup>, for a salinity of 32 at 15 and 4 °C, respectively).

## 15 2.8 Solid hydrated density of aggregate constituents

The solid hydrated density ( $\rho_s$ , g cm<sup>-3</sup>) of the aggregated particles was determined in a density gradient using a modified version of previously reported methods (Schwinghamer, 1991; Feinberg and Dam, 1998). The density gradient consisted of seven dilutions which were made using Ludox TM colloidal silica, sucrose, and distilled water.

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The dilutions had a density range between 1.05 and 1.43 g cm<sup>-3</sup>. The dilutions were buffered to pH 8.1 with 0.0125 M Tris plus 0.0125 M Tris-HCl (final concentration). Thus, the produced gradient was iso-osmotic with seawater of a salinity of 32. Two mL of each dilution were gently transferred to a 20-mL centrifuge tube with the densest dilution below and the least dense dilution on top. The density gradients were refrigerated overnight and allowed to adjust to the treatment temperature before use. One mL of seawater (salinity 32) was gently applied on top of each density gradient, and single aggregates were transferred to individual centrifugation tubes using a wide-tipped pipette letting the aggregates settle into the seawater layer without breaking. After a settling period of 2 to 4 h, the density gradients were centrifuged at 3000 rpm for 30 min to ensure that the aggregate had settled to the density layer equivalent to its solid hydrated density. One mL from the density layer containing aggregated particles was removed from the tube and its weight was measured on a Mettler Toledo fine-balance. Assuming iso-osmotic conditions between the aggregated particles and the density solution, the density of the removed gradient layer represent the solid hydrated density of the particles having neutral buoyancy within it.

## 2.9 Transparent exopolymeric particles (TEP) measurements

TEP concentrations within the aggregates were quantified using the dye-binding assay for spectrophotometric measurements (Passow and Alldredge, 1995). At each measuring point during the incubation period, three nucleopore polycarbonate filters (0.4 μm) were prepared with one aggregate of known volume gently filtered to each. TEP were stained on the filters for 30 s with 500 μL pre-calibrated 0.02 % aqueous solution of al-cian blue (8GX) in 0.06 % acetic acid (pH 2.5). The filters were rinsed once with distilled water to remove excess dye, and were submerged in sulfuric acid to dissolve the dye. The TEP concentration (Xanthan equivalents) within each aggregate was estimated by measuring the one mL of the solvent on a spectrophotometer at 787 nm. The TEP

concentration within each aggregate was determined via triplicate measurements of the solvent.

### 3 Results

#### 3.1 Aggregate formation

Initial cell concentrations of *S. costatum* in all the 20 roller tanks were  $3 \times 10^5 \text{ mL}^{-1}$ , and aggregates were formed within the first 19 h of incubation. A general trend of increasing abundance of larger aggregate sizes concurrent with decreasing abundance of small aggregate sizes over time was observed, indicating that the large aggregates scavenged the small aggregates over time (Fig. 1). However, the aggregates in the  $15^\circ\text{C}$  treatment showed an increase in abundance of small aggregates ( $< 3 \text{ mm}$ ) and a decrease in abundance of large aggregates ( $> 3 \text{ mm}$ ) on day 12, indicating that disaggregation of large aggregates occurred between day 9 and day 12 (Fig. 1a). Thereafter, the small aggregates re-aggregated and/or were scavenged by the larger aggregates which resulted in continuous increasing maximum aggregate size. Lowering the temperature to  $4^\circ\text{C}$  for half of the roller tanks after 3 days of incubation did not have any effect on the aggregate size distribution (Fig. 1b). The aggregates incubated at  $4^\circ\text{C}$  did not show any indication of disaggregation, but had continuously increasing abundance of larger aggregates concurrent with decreasing abundance of small aggregates. This was due to constant scavenging of small aggregates by large aggregates throughout the study. We observed aggregates larger than  $10 \text{ mm}$  in the roller tanks at both temperatures, but those aggregates were very fragile and fell apart during sampling, therefore no measurements were performed on aggregates larger than  $\sim 7 \text{ mm}$ .

#### 3.2 Aggregate TEP content

The content of transparent exopolymer particles (TEP) within the aggregates in both treatments was low but increased with increasing aggregate size from  $\sim 0.3$  to  $\sim 8 \mu\text{g}$

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TEP (Xanthan equivalents) in 1 and 5 mm large aggregates, respectively. The average TEP content to dry weight ratio of the aggregates was low and constant throughout the study (Fig. 4c). No significant differences were observed in the TEP content to aggregate dry weight over time within the 15 or 4 °C treatments or between the two treatments (One-way ANOVA;  $p > 0.2$ , Fig. 4c and Table 1).

### 3.3 Aggregate dry weight

The dry weight (DW) increased with increasing aggregate size for both the aggregates incubated in the 15 and 4 °C treatments (Fig. 2a, e). A tendency of higher variation in size-specific aggregate DW over time was observed for the aggregates incubated at 15 °C compared to those transferred to 4 °C. This was due to a tendency of higher size-specific DW for the 1, 17, and 23 days old aggregates in the 15 °C treatment (Fig. 2b). No changes in size-specific DW over time were observed among the aggregates transferred to 4 °C with the exception of day 15 where aggregates seemed to have higher size-specific DW compared to the other time points in treatment 4 °C (Fig. 2f). However, this was mainly driven by one 3.5 mm aggregate weighing two times more than similar sized aggregates measured on day 15 (Fig. 2e).

### 3.4 Aggregate excess density and hydrated solid density

Due to the fractal nature of aggregates, their excess densities decrease with increasing size, i.e. their porosity increases with increasing aggregate size. The excess densities did not change over time in the 4 °C treatment, but increased in the 15 °C treatments after day 17 and remained high until the last measurement on day 23 (Fig. 2c). The solid hydrated density of the aggregated material ranged between 1.10 and 1.18 g cm<sup>-3</sup> and showed no significant differences within or between the 4 and 15 °C treatments (One Way ANOVA;  $p > 0.38$ ), we have therefore averaged the solid hydrated density of the aggregated material over the entire incubation time for each treatment (Table 1). The constant solid hydrated density during the incubation period shows that the increasing

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size-specific excess density in the 15 °C treatment after day 17 (Fig. 2c) was not due to a density change of the composite particles within the aggregates, but rather due to an increased compactness of the aggregated material. This is also supported by the increase in size-specific DW after day 17 (Fig. 2a).

### 5 3.5 Aggregate sinking velocity

Sinking velocity increased near-linearly with increasing aggregate size in both the 4 and 15 °C treatments (Fig. 2d, h). Lowering the temperature from 15 °C to 4 °C for half of the roller tanks after three days of incubation had no effect on the size-specific sinking speeds, and there was no significant difference in size-specific sinking speed between the 15 °C (day 2 and 5) and the 4 °C (day 4) treatments (one-way ANCOVA,  $p > 0.1$ ). The aggregates in the 4 °C treatment did not show any significant changes in size-specific sinking velocity over time (Fig. 2h; one-way ANCOVA,  $p > 0.3$ ). The 15 °C treatment had similar size-specific sinking speeds between day 2 and day 9, but we measured significantly increased size-specific sinking speeds on day 17 and day 23 (Fig. 2d; one-way ANCOVA,  $p < 0.01$ ). This increase in size-specific sinking speeds coincided with the increase in size-specific excess density (Fig. 2c) and size-specific DW (Fig. 2a) and occurred at the first sampling after the disaggregation event on day 12 (Fig. 1a).

### 3.6 Particulate organic carbon and nitrogen content, and respiration rate

Particulate organic carbon (POC) content in the aggregates increased with increasing aggregate size in both the 4 and 15 °C treatments (Fig. 3a, d). There was no significant difference in the average POC : DW ratio over the entire incubation time between or within the two treatments (Table 1; Student's t-test;  $p > 0.7$ ). The respiration rate per aggregate increased with increasing aggregate size at both 4 and 15 °C, but the size-specific respiration rate was generally higher in the 15 °C treatment compared to that in the 4 °C treatment (data not shown). The respiration rate increased proportional

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to POC content of the aggregates in the two treatments, indicating first-order kinetics of POC degradation at both temperatures (Fig. 3b, e). The carbon-specific respiration rate was calculated by dividing the carbon respiration rate with the total POC content of each aggregate and was size-independent in both treatments at all times (Fig. 3c, f). The overall average carbon-specific respiration rates were  $0.12 \pm 0.03 \text{ d}^{-1}$  and  $0.03 \pm 0.01 \text{ d}^{-1}$  in the  $15^\circ\text{C}$  and  $4^\circ\text{C}$ , respectively. Hence, the average carbon-specific respiration rate was 3.5-fold lower in the  $4^\circ\text{C}$  treatment compared to that in the  $15^\circ\text{C}$  treatment (Table 1; Student's t-test;  $p < 0.01$ ). The slight tendency for increasing average carbon-specific degradation rates over time in the  $4^\circ\text{C}$  treatment and decreasing average carbon-specific degradation rates over time in the  $15^\circ\text{C}$  treatment were not statistically significant (Student's t-test;  $p > 0.1$ ) (Fig. 4a). The tendency of increasing C:N ratio at day 23 in the  $15^\circ\text{C}$  treatment could not be tested statistically since the POC and particulate organic nitrogen only were measured from one filter due to limited amount of material and, therefore, the C:N ratios should be treated with care.

## 4 Discussion

There were no significant changes in size distribution of aggregates transitioned to  $4^\circ\text{C}$  compared to the aggregates kept at  $15^\circ\text{C}$  (Fig. 1). This indicated that the temperature change did not influence the physical structure of the aggregates, which was also evident from the lack of changes in size-specific dry weight, excess density, and sinking velocity between the two temperature treatments between day 4 and 9 (Fig. 2). This shows that temperature changes alone do not influence aggregation and disaggregation processes.

Our measurements of respiration represent community respiration on aggregates, i.e. it includes respiration by diatoms and associated bacteria and protozoa. The average carbon-specific respiration rates measured in aggregates at  $15^\circ\text{C}$  were similar to previous rates measured within marine snow, phytoplankton aggregates, and copepod fecal pellets at surface water conditions (Ploug et al., 1999; Iversen et al., 2010;

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Iversen and Ploug, 2010). The potential fluxes of O<sub>2</sub> due to advection and diffusion to sinking aggregates has earlier been shown to be similar at 4 and 20 °C because the lower diffusivity and higher kinematic viscosity is compensated by higher O<sub>2</sub> solubility at lower temperatures as compared to higher temperatures (Ploug, 2001). The carbon-specific community respiration rates in diatom aggregates measured at 4 °C as compared to those measured at 15 °C were similar to those expected for a Q<sub>10</sub> of 3.3, which has been measured previously with respect to aquatic bacterial growth rates in pelagic habitats (White et al., 1991). Hence, the measured decrease in community respiration rate was presumably due to lower cell-specific activities within the aggregates. Decreased ambient temperatures, therefore, significantly reduce the organic carbon remineralisation by microbiota adapted to higher temperatures, e.g. if surface ocean adapted microbes attached to settling aggregates are transported to the colder deep ocean. Kiørboe et al. (2002) suggested that detachment of bacteria from aggregates is only physically possible soon after attachment because the bacteria may become embedded in the mucus or matrix within the aggregates and, thus, permanently attached. This may explain observations of different prokaryotic communities within aggregates compared to the free water (Moeseneder et al., 2001) and observations of living surface ocean microbes attached to aggregates collected at 6000 m (Eloe et al., 2011).

Our experimental setup excluded changing hydrostatic pressure, thus did not fully reflect true in situ conditions. Hydrostatic pressure has been suggested to be an important environmental parameter influencing microbial dynamics within aggregates (Tamburini et al., 2003, 2006; Grossart and Gust, 2009). Grossart and Gust (2009) showed that increasing hydrostatic pressure at constant temperature reduces bacterial cell size and abundance and can select for species with physiological pressure adaptations. Thus, pressure may also have an effect on microbial turnover of organic matter. This calls for experiments simultaneously investigating the influence from pressure and temperature changes on depth-specific degradation and export processes.

The POC : PON ratio remained relatively stable during our experiment, implying that POC and PON was degraded at similar rates. This has also been observed during

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the first 3 weeks in other degradation studies of diatom aggregates and other detritus where budgets of POC and PON degradation, and C : N ratios were measured (Ploug and Grossart, 2000; Verity et al., 2000; Grossart and Ploug, 2001). We observed high carbon-specific respiration rates at 15 °C but no change in size-specific POC or DW content over time. This suggests that aggregates are primarily degraded outside-in as has also been observed earlier (Ploug and Grossart, 2000). Furthermore, continuous scavenging of POC from the surrounding water, likely as suspended diatom cells, or DOC diffusing from the bulk towards aggregates were presumably additional carbon sources to support respiration in aggregates. Efficient scavenging of suspended particles by settling aggregates has been observed in situ (Brzezinski and Nelson, 1995; Kumar et al., 1998; Passow et al., 2001) and may be common in surface waters with high ambient particles concentrations. Hereby, scavenging of suspended cells may support substrate for rapid turnover of POC by aggregate-associated microbes.

We calculated Reynolds numbers of less than 1 for aggregates smaller than 2 mm and an average of  $10 \pm 6$  for larger aggregates. Hence, the sinking speeds were mainly controlled by inertial forces. Intuitively the higher water viscosity at 4 °C compared to 15 °C should decrease the size-specific sinking speeds, but the temperature difference showed no immediate significant effect on the measured sinking speeds. Using Stokes' Law and Navier–Stokes drag equation, we calculated 27 and 22 % lower sinking speeds, respectively, at 4 °C compared to 15 °C. Often the sinking speed of individual similar sized aggregates varied with more than 50 %, and may have masked any potential temperature effect. Large scatter in size-specific sinking speeds of marine snow is common for both in situ and laboratory produced aggregates due to their highly heterogeneous and porous nature (Aldredge and Gotschalk, 1988; Iversen and Ploug, 2010), complicating predictions of in situ temperature dependent settling.

The 15 °C treatment showed significantly higher size-specific sinking velocities and excess density on day 12 and onwards compared to the measurements before day 12 (Fig. 2c, d) coinciding with a disaggregation event between day 9 and 12 (Fig. 1a). The solid matter density of the composite particles within the aggregates, however, did



not change over time in the two treatments (Table 1), indicating that the increase in size-specific excess density and sinking velocity was due to a more compact packaging of the composite particles within the aggregates after the disaggregation. Ploug et al. (2008) also observed an increase in excess density of *S. costatum* aggregates due to increased compactness over time. Aggregates descending in situ encounter and scavenge small and dense particles (Kepkay, 1994). This may ballast the aggregates and increase their size-specific sinking velocities and excess densities over time (Ploug et al., 2008; Iversen et al., 2010; Iversen and Ploug, 2010)

To test how the carbon-specific respiration rates measured at 4 and 15 °C match the attenuation of carbon fluxes in the deep ocean, we selected deep ocean carbon fluxes from global data sets of sediment trap studies (Table 1 in Lutz et al., 2002, and Table 3 in Honjo et al., 2008). We only included sediment trap studies with two different collection depths from the same study area and time and with an upper trap depth below 900 m (see Table 2). The carbon flux to a lower sediment trap ( $T_L$ ) was calculated using  $L$ -ratios found for 4 °C and 15 °C, the collected carbon flux in an upper trap ( $T_U$ ), and the depth interval between the two traps ( $\Delta z$ ):

$$T_L = T_U - (1 - e^{-L \cdot \Delta z}) \cdot T_U \quad (4)$$

where  $L$  is the fractional remineralisation per meter settled.  $L$  was calculated from the average carbon-specific respiration rate for the 4 and 15 °C treatments (Table 1) divided with an average sinking velocity of 150 m d<sup>-1</sup> for both treatments (Berelson, 2002; Fischer and Karakas, 2009).  $L$  was  $2.20 \times 10^{-4}$  and  $7.64 \times 10^{-4} \text{ m}^{-1}$  for the 4 °C and 15 °C treatment, respectively.

$T_L$  calculated using the 4 °C carbon-specific respiration fitted surprisingly well to the trap collected  $T_L$ , while the 3.5-fold higher carbon-specific respiration rate at 15 °C underestimated the trap collected  $T_L$  (Fig. 5). This indicates that relatively good estimates of deep ocean fluxes can be obtained by inclusions of temperature limitations on respiratory activity alone. Knowledge of particle size spectra at depths would provide better calculations of  $T_L$  since it would allow size-specific sinking speeds instead of average

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sinking speed for all POC to calculate  $L$ . Further, temperature deviations from 4°C would influence the microbial activity and, thus, the microbial degradation rates. However, the relatively good predictability of these simple estimates indicates that temperature plays a major role for deep ocean fluxes of POC, possibly caused by embedding of temperature sensitive microbes from the surface ocean within the aggregates at depths.

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**Table 1.** Average (Av.) measurements for Xanthan equivalent ( $\mu\text{g Xequv}$ ) TEP content to dry weight (DW) ratio, solid hydrated density of the composite particles within the aggregates, POC content to DW ratio, POC content to PON content ratio, and carbon-specific respiration rate (C-spec. deg.) for the 15 and 4 °C treatment over the whole incubation period. Standard deviations are presented together with average values. There were only significant differences in the average values for carbon-specific respiration rate between the two treatments.

Treatment	Av. TEP : DW ( $\mu\text{g Xequv TEP } \mu\text{g Agg}^{-1}$ )	Av. solid hydr. density ( $\text{g cm}^{-3}$ )	Av. POC : DW ( $\mu\text{g POC } \mu\text{g Agg}^{-1}$ )	Av. POC : PON ( $\mu\text{g POC } \mu\text{g PON}^{-1}$ )	Av. C-spec. deg. ( $\text{d}^{-1}$ )
15 °C	0.035 ± 0.008	1.15 ± 0.02	0.25 ± 0.02	5.28 ± 0.47	0.12 ± 0.03*
4 °C	0.036 ± 0.005	1.14 ± 0.02	0.25 ± 0.01	5.02 ± 0.21	0.03 ± 0.01*

\* Significant difference between the 15 and 4 °C treatment (Student's t-test;  $p = 0.01$ ).

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**Table 2.** Sediment trap derived annual flux to depth rates selected from Table 1 in Lutz et al. (2002) and Table 3 in Honjo et al. (2008), the data from the latter is indicated with an asterisk. The fluxes are calculated for the lower sediment traps using Eq. (4) and the carbon-specific degradation rates found from the 4 °C ( $T_L$  4 °C) and the 15 °C ( $T_L$  15 °C) treatment. An average sinking velocity of 150  $\text{m d}^{-1}$  was used in both treatments to find  $L$  from the average carbon-specific respiration rates for each treatment (Table 1).

Region	Trap ID/ Year	Depth (m)	Flux ( $\text{g m}^{-2} \text{yr}^{-1}$ )	References	$T_L$ 15 °C ( $\text{g m}^{-2} \text{yr}^{-1}$ )	$T_L$ 4 °C ( $\text{g m}^{-2} \text{yr}^{-1}$ )
<b>Polar Arctic</b>						
Greenland Sea	88–89	1000	1.2994	Bodungen et al. (1995)		
Greenland Sea		2200	0.3285	Bodungen et al. (1995)	0.52	1.00
Greenland Sea	90–91	1000	0.74825	Bodungen et al. (1995)		
Greenland Sea		2200	0.36135	Bodungen et al. (1995)	0.30	0.58
<b>Atlantic Ocean</b>						
NABE	89–90	1110	1.47825	Honjo and Manganini (1993)		
NABE		2110	1.41255	Honjo and Manganini (1993)	0.69	1.19
NABE		3730	1.0001	Honjo and Manganini (1993)	0.41	0.99
Eq. Atlantic	92–94	1000	2.6864	Usbeck (1999)		
Eq. Atlantic		4500	1.2702	Usbeck (1999)	0.19	1.25
Eq. Atlantic		1833	2.36155	Usbeck (1999)		
Eq. Atlantic		2890	1.4308	Usbeck (1999)	1.05	1.87
*Atlantic	92	2030	1.296	Kuss and Kremling (1999) & Scholten et al. (2001)	0.41	0.93
*Atlantic		3530	0.648			
*Atlantic	89	2018	1.752	Honjo (1992, 1993)		
*Atlantic		3718	0.996	Honjo (1992, 1993)	0.48	1.21
*Atlantic	89	2067	1.128	Honjo (1992, 1993)		
*Atlantic		4563	0.936	Honjo (1992, 1993)	0.17	0.65
*Atlantic	84+	1500	0.876	Deuser et al. (1995) & Conte et al. (2001)	0.24	0.60
*Atlantic	84+	3200	0.624			
*Atlantic	91	1600	0.864	Fischer and Wefer (1996) & Wefer and Fischer (1993)	0.22	0.58
*Atlantic	91	3400	0.588			
Subtrop. Atlantic	77–78	988	1.4381	Honjo (1980)		
Subtrop. Atlantic		3755	0.63145	Honjo (1980)	0.17	0.78
Subtrop. Atlantic		5068	0.6205	Honjo (1980)	0.23	0.47
<b>Pacific Ocean</b>						
Ocean station	83–93	1000	2.7083	Wong et al. (1999)		
Ocean station	82–93	3800	1.1315	Wong et al. (1999)	0.32	1.47
South China Sea	90–95	1200	1.533	Jianfang et al. (1996)		
South China Sea		2240	1.26115	Jianfang et al. (1998)	0.69	1.22
South China Sea		3770	0.9198	Jianfang et al. (1998)	0.40	0.40
South China Sea	87–88	1000	1.4308	Jianfang et al. (1998)		
South China Sea		3350	0.7373	Jianfang et al. (1998)	0.23	0.85
N Eq. Current	88–89	1130	0.6497	Kempe and Knaack (1996)		
N Eq. Current		3130	0.24455	Kempe and Knaack (1996)	0.14	0.42
Eq. Pacific		1600	0.8687	Dymond and Collier (1988)		
Eq. Pacific		3400	0.5913	Dymond and Collier (1988)	0.22	0.59
Eq. Pacific	92–93	2250	0.5548	Honjo et al. (1995)		
Eq. Pacific		4400	0.3504	Honjo et al. (1995)	0.11	0.35
Eq. Pacific	92–93	1191	2.1973	Honjo et al. (1995)		
Eq. Pacific		2091	1.6425	Honjo et al. (1995)	1.11	1.80
Eq. Pacific		3793	1.4016	Honjo et al. (1995)	0.45	1.13
Eq. Pacific	83–84	1895	1.55125	Dymond and Collier (1988)		
Eq. Pacific		3495	1.1899	Dymond and Collier (1988)	0.46	1.09
Eq. Pacific	84–85	1883	2.4747	Dymond and Collier (1988)		
Eq. Pacific		2908	1.8907	Dymond and Collier (1988)	1.13	1.98
Eq. Pacific		2284	1.63885	Honjo et al. (1995)		
Eq. Pacific		3618	1.5987	Honjo et al. (1995)	0.59	1.22
Eq. Pacific	92–93	1292	0.5548	Honjo et al. (1995)		
Eq. Pacific		3594	0.2628	Honjo et al. (1995)	0.10	0.34

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**Table 2.** Continued

Region	Trap ID/ Year	Depth (m)	Flux (g m <sup>-2</sup> yr <sup>-1</sup> )	References	$T_L$ 15 °C (g m <sup>-2</sup> yr <sup>-1</sup> )	$T_L$ 4 °C (g m <sup>-2</sup> yr <sup>-1</sup> )
Indian Ocean						
<i>Arabian Sea</i>		2363	1.387	Honjo et al. (1999)		
<i>Arabian Sea</i>		3915	1.2045	Honjo et al. (1999)	0.42	0.99
<i>Arabian Sea</i>	94-95	858	6.3875	Honjo et al. (1999)		
<i>Arabian Sea</i>		1857	5.9495	Honjo et al. (1999)	2.98	5.13
<i>Arabian Sea</i>		2871	4.672	Honjo et al. (1999)	2.74	4.76
<i>Bay of Benegal</i>	87-88	1040	2.36885	Ittekkot et al. (1991)		
<i>Bay of Benegal</i>		3006	2.04035	Ittekkot et al. (1991)	0.53	1.54
Polar Antarctic						
<i>ACC, Atlantic</i>	92	2453	2.4163	Pudsey and King (1997)		
<i>ACC, Atlantic</i>		3259	1.02565	Pudsey and King (1997)	1.31	2.02
<i>ACC, Atlantic</i>	92	2966	2.38345	Pudsey and King (1997)		
<i>ACC, Atlantic</i>		3766	0.5548	Pudsey and King (1997)	1.29	2.00
<i>SAE Pacific</i>	96-98	982	1.7009	Honjo et al. (2000)		
<i>SAE Pacific</i>		4224	0.62415	Honjo et al. (2000) (JGOFS)	0.14	0.84

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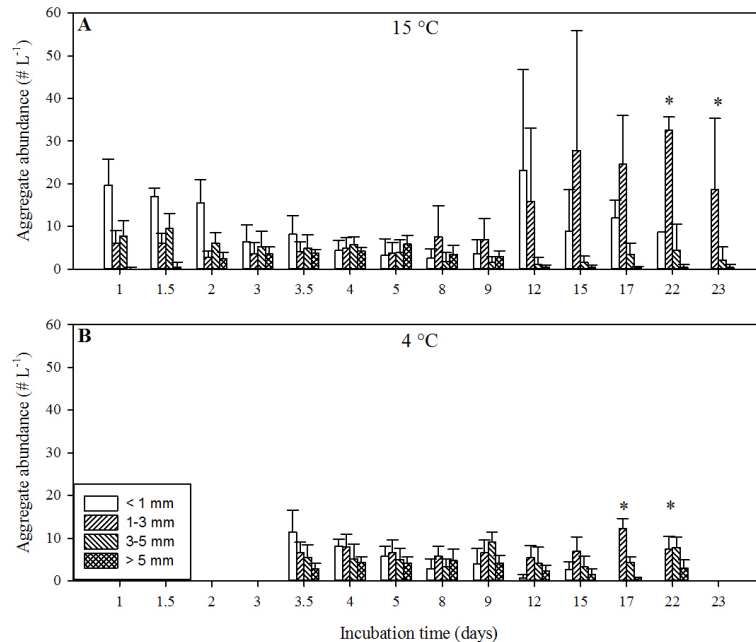
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Interactive Discussion



## Temperature effects on respiration and sinking rate

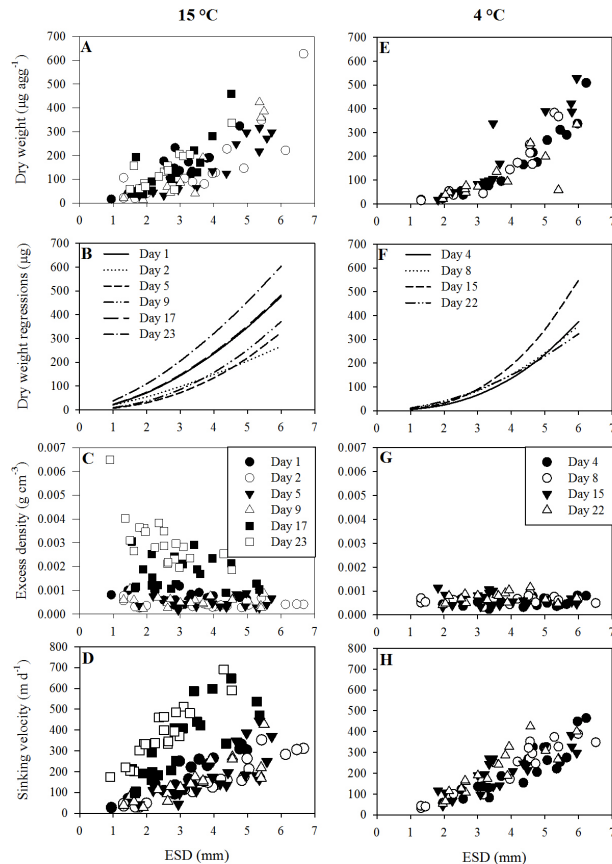
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**Fig. 1.** Aggregate evolution over time for the 15 and 4 °C treatments in the upper and lower panel, respectively. The aggregates in the 4 °C treatment were kept at 15 °C during the first 3 days of incubation. The aggregates were pooled into size classes and counted by eye (MHI) at the different time points during the whole incubation period, and should, thus, be viewed as semi-quantitative measurements. The results give good indications of disaggregation during the incubation period, but the actual aggregate abundances are not absolute values, especially not at high abundances. The asterisks at the last two measured time points in each treatments indicate that only replicate measurements were done, but standard deviations are still plotted to indicate the variation in size distribution in the two roller tanks.

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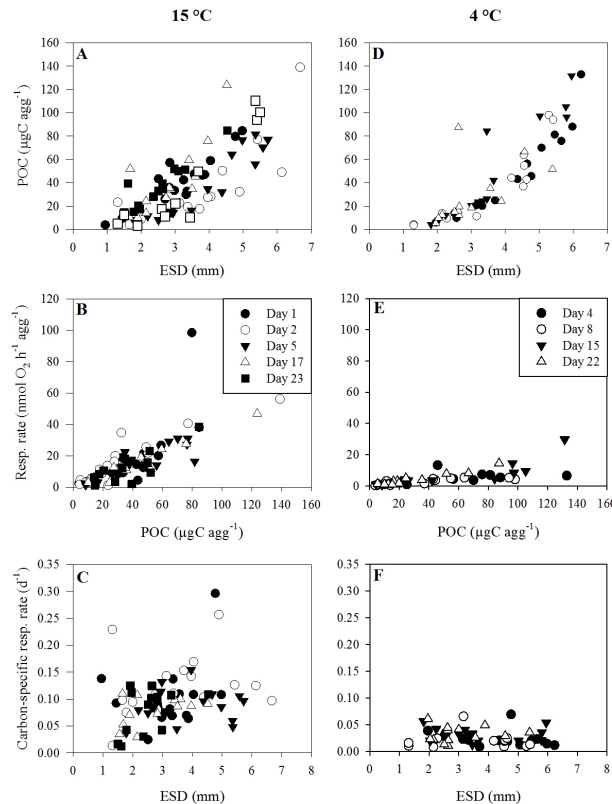


**Fig. 2.** Aggregate dry weight (A, E), dry weight power regressions (B, F), excess density (C, G), and sinking velocity (D, H) plotted against aggregate equivalent spherical diameter (ESD) for the 15 and 4 °C treatments. The symbols for the day of the different measurements are given in the legends. The legends for the 15 °C treatment (A–D) is given in graph (C) and the legends for the 4 °C treatment (D–G) is given in graph (G).

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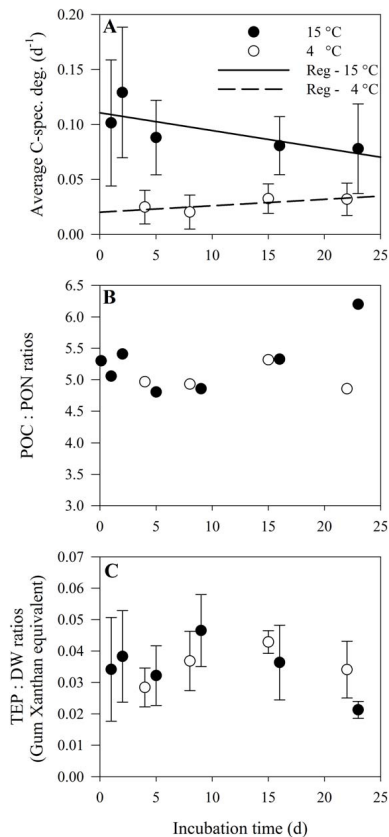
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**Fig. 3.** Aggregate particulate organic carbon (POC) content is plotted against aggregate equivalent spherical diameter (ESD) (A, C), and the respiration rate (Resp. rate) of the microbial community attached to each aggregate is plotted against the POC content of the aggregates (B, D). The symbols for the day of the different measurements are given in the legends. The legends for the 15°C treatment (A, B) is given in graph (B) and the legends for the 4°C treatment (D, E) is given in graph (E).

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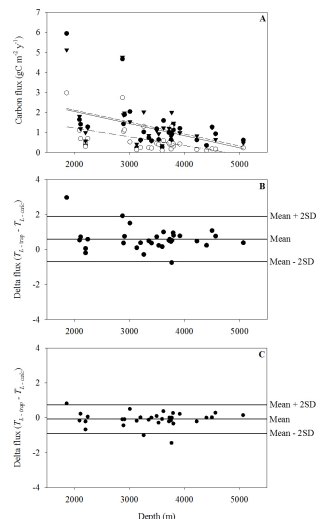


**Fig. 4.** Average carbon-specific respiration rate (Average C-spec. deg.) **(A)**, particulate organic carbon to particulate organic nitrogen ratio (C : N ratios) **(B)**, and transparent exopolymer particles to dry weight ratios (TEP : DW ratios) **(C)** is plotted against the incubation time for both the 15 and 4 °C treatments as solid and open circles, respectively. Standard deviations are indicated in the plot when available.

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**Fig. 5. (A)** Carbon fluxes collected with deep ocean sediment traps (closed circles) and calculated using Eq. (4) for average carbon-specific respiration rates found for the 15 °C treatment (open circles) and the 4 °C treatment (closed triangulars) – see text and Table 2. The fluxes are plotted against the depth of the trap position. Linear regressions are fitted to each data set: Sediment trap collections:  $y = 3.26 - 0.0006x$ ;  $R^2 = 0.16$ , 15 °C treatment:  $y = 2.1 - 0.0004x$ ;  $R^2 = 0.26$ , and 4 °C treatment:  $y = 3.3 - 0.0006x$ ;  $R^2 = 0.19$ . **(B)** Delta flux for the 15 °C treatment calculated as trap carbon flux ( $T_{L-trap}$ ) minus calculated carbon flux ( $T_{L-calc}$ ) and plotted against depth. Delta flux shows the error between the measured and calculated carbon fluxes, if the mean goes through zero the calculated flux return that of the measured flux. Lines for mean and mean  $\pm$  standard deviation are provided in the plot. **(C)** Delta flux for the 4 °C treatment calculated as trap carbon flux ( $T_{L-trap}$ ) minus calculated carbon flux ( $T_{L-calc}$ ) and plotted against depth. Lines for mean and mean  $\pm$  standard deviation are provided in the plot.

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