

# 1     **Aggregates reduce transport distance of soil organic carbon: are** 2                                    **our balances correct?**

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## 8                                    **Abstract**

9     The effect of soil erosion on global carbon cycling, especially as a source or sink for  
10    greenhouse gases, has been the subject of intense debate. The controversy arises mostly  
11    from the lack of information on the fate of eroded soil organic carbon (SOC) whilst in-transit  
12    from the site of erosion to the site of longer-term deposition. Solving this controversy requires  
13    an improved understanding of the transport distance of eroded SOC, which is principally  
14    related to the settling velocity of sediment fractions that carry the eroded SOC. Although  
15    settling velocity has already been included in some erosion models, it is often based on  
16    mineral particle size distribution. For aggregated soils, settling velocities are affected by their  
17    actual aggregate size rather than by mineral particle size distribution. Aggregate stability is,  
18    in turn, strongly influenced by SOC. In order to identify the effect of aggregation of source  
19    soil on the transport distance of eroded SOC, and its susceptibility to mineralization after  
20    transport and temporary deposition, a rainfall simulation was carried out on a silty loam. Both  
21    the eroded sediments and undisturbed soils were fractionated into six different size classes  
22    using a settling tube apparatus according to their settling velocities: > 250, 125 to 250, 63 to  
23    125, 32 to 63, 20 to 32 and < 20  $\mu\text{m}$ . Weight, SOC content and instantaneous respiration  
24    rates were measured for each of the six class fractions. Our results indicate that: 1) 41% of  
25    the eroded SOC was transported with coarse aggregates that would be likely re-deposited  
26    down eroding hillslopes, rather than with fine particles likely transferred to water courses; 2)  
27    erosion was prone to accelerate the mineralization of eroded SOC, and thus might contribute  
28    more  $\text{CO}_2$  to the atmosphere than current estimates which often ignore potential effects of

29 aggregation; 3) preferential deposition of SOC-rich coarse aggregates potentially causes an  
30 increase of SOC remaining in the colluvial system and a reduction of SOC flux to the alluvial  
31 or aquatic system. These findings identify a potential error of overestimating net erosion-  
32 induced carbon sink effects, and thus add an additional factor to consider when improving  
33 our current understanding of SOC erosion and deposition on hillslopes.

34

35 *Key words: eroded organic carbon, instantaneous respiration rate, transport distance, carbon*  
36 *source*

37

## 38 **1. Introduction**

39 The net effect of soil erosion as a source or sink of CO<sub>2</sub> in the global carbon cycle  
40 has been the subject of intense debate (Lal, 2003; van Oost et al., 2007; Quinton et  
41 al., 2010; Dlugoß et al., 2012; Doetterl et al., 2012). On one hand, erosion exposes  
42 the previously incorporated soil organic carbon (SOC), which may accelerate the  
43 mineralization of eroded SOC (Jacinthe et al., 2002, 2004; Kuhn, 2007; Mora et al.,  
44 2007; Lal and Pimentel, 2008). On the other hand, deposition limits the  
45 decomposition of SOC upon burial, while inputs of decomposing plant material on the  
46 surface of eroding sites partially replaces the lost SOC (Harden et al., 1999; van Oost  
47 et al., 2007; Wang et al., 2010). So far, effects of erosion on CO<sub>2</sub> emissions have  
48 mostly been assessed by comparing SOC stocks at the assumed site of erosion and  
49 the site of colluvial deposition (Stallard, 1998; Berhe, 2011; van Hemelryck et al.,  
50 2011; Nadeu et al., 2012; van Oost et al., 2012). One underlying assumption  
51 associated with this approach is that the redistribution of eroded SOC across  
52 landscapes is non-selective. However, several recent publications showed (at least)  
53 temporary enrichment of SOC in sediment, as well as preferential deposition of

54 aggregates with size distribution and SOC content that differ from original soils  
55 (Schiettecatte et al., 2008; Kuhn et al., 2009; Hu et al., 2013a; Kuhn, 2013). As a  
56 consequence, carbon balances drawn only from the SOC stocks on sites of erosion  
57 and colluvial deposition may not adequately consider the potential SOC re-deposition  
58 into the terrestrial system.

59 Regardless of selective or non-selective erosion, sediment fractions are all likely to  
60 experience preferential deposition. Therefore, SOC redistribution, either after  
61 selective or non-selective erosion, is strongly depending on the transport distance of  
62 eroded aggregates. This is thus related to the respective settling velocities of  
63 sediment fractions carrying the eroded SOC (Dietrich, 1982; Kinnell, 2001, 2005).  
64 Although settling velocity has already been included in some erosion models, it is  
65 often based on mineral particle size distribution (Morgan et al., 1998; Beuselinck et  
66 al., 1999; Flanagan and Nearing, 2000; van Oost et al., 2004; Aksoy and Kavvas,  
67 2005). But for aggregated soils, settling velocities are affected by the actual size,  
68 irregular shape, porosity of soil fractions and their incorporation with light-dense SOC  
69 (Kinnell and McLachlan, 1988; Loch, 2001; Hu et al., 2013b). In addition, the upper  
70 limits of the mineral particle size classes used in current erosion models are often  
71 smaller than the actual aggregate sizes. For instance, the largest class in van Oost et  
72 al. (2004) is only 90  $\mu\text{m}$ , whereas up to 250  $\mu\text{m}$  for rill erosion in Morgan et al. (1998).  
73 Such limits may also skew the estimation on settling velocity of eroded sediment.  
74 Hence, the mineral particle size classes, no matter how efficiently applicable in  
75 erosion models, are not the decisive factor that determines the actual settling  
76 behaviour or movement of aggregates. Aggregation of original soil potentially  
77 increases the settling velocities of soil particles, and thereby likely reduces their

78 transport distances after erosion (Hu et al., 2013b). This, in theory, would also reduce  
79 the transport distance of eroded SOC incorporated into soil aggregates.

80 The effect of aggregation of source soil may also affect the movement of SOC down  
81 eroding hillslopes. Aggregation is related to SOC content, and SOC is often  
82 increased in both macro- and micro-aggregates (Tisdall and Oades, 1982;  
83 Cambardella and Elliott, 1994). The quality and stabilizing mechanisms of SOC in the  
84 soil matrix also vary with different aggregate conditions. For instance, physically-  
85 stabilized SOC within macro- and micro-aggregates is protected by forming physical  
86 barriers between microbes and enzymes and their substrates, and thus very  
87 susceptible to mineralization after aggregates break-up (Six et al., 2002). Chemically-  
88 stabilized SOC results from the chemical or physicochemical binding between SOC  
89 and soil minerals (i.e., clay and silt particles). Such stabilization is also likely to be  
90 disturbed by aggregates break-up, as often occurs during erosion and transport  
91 (Starr et al., 2000; Lal and Pimentel, 2008; van Hemelryck et al., 2010).  
92 Biochemically-stabilized SOC is resulted from the inherent or acquired biochemical  
93 resistance to decomposition. Aggregates break-up might also affect the  
94 biodegradability of the SOC or the exposure to hydrolyzation. Therefore, erosion,  
95 either detaching aggregates from the soil matrix or disintegrating larger aggregates,  
96 may have diverse impacts on mineralization of eroded SOC (van Hemelryck et al.,  
97 2010; Fiener et al., 2012).

98 In this study, we aim to conduct an initial test of the theoretical deductions made  
99 above by fractionating eroded loess sediments, generated during a laboratory rainfall  
100 simulation, according to their settling velocities, and then measure their SOC content  
101 and instantaneous respiration rates.

102

## 103 **2. Materials and Methods**

### 104 **2.1. Soil sampling and preparation**

105 A silty loam from the conventionally managed Bäumlhof Farm in Möhlin (47°33' N,  
106 7°50' E), near Basel in northwest Switzerland, was used in this study. The soil  
107 supports a maize-wheat-grass rotation. A-horizon material (top 20 cm) was sampled  
108 from a gentle shoulder slope (< 5%) in March 2012. Previous research on the same  
109 silty loam showed that aggregation increased the settling velocity of original soil  
110 fractions, particularly the medium sized fractions, in comparison with that expected  
111 based on the texture of the original soil (Hu et al., 2013b). The mineral particle  
112 specific SOC distribution, average SOC content (LECO RC 612 at 550°C), and  
113 aggregate stability of original soil (method adapted from Nimmo and Perkins, 2002),  
114 are shown in Table 1. The mineral particle size distribution was fractionated by wet-  
115 sieving, after dispersion by ultrasound using a Sonifier Model 250 from Branson, USA.  
116 The energy dissipated in the water/soil suspension was  $60 \text{ J}\cdot\text{ml}^{-1}$  (i.e. Energy =  
117 output power  $70 \text{ W} \times$  time  $85 \text{ s}$  / suspension volume  $100 \text{ ml}$ ). The SOC mass  
118 proportions across mineral particle size classes were calculated only from average  
119 values of individual weight and SOC content. Although the ultrasound energy used in  
120 Hu et al. (2013b) was not enough to thoroughly disperse the original soil into real  
121 mineral particles (Kaiser et al., 2012), such extent of dispersion was notable enough  
122 to demonstrate the potential under-estimation of applying mineral particle size  
123 distribution to predict the settling velocity of eroded SOC. Hence, it is speculated that  
124 similar increasing effects would also occur to sediment fractions, and thus make the  
125 silty loam suitable to investigate the potential effects of aggregation of original soil on  
126 the transport distances of differently sized sediment fractions. While this study  
127 investigated only one soil, similar loess soils cover about 10% (ca., 14.9 million  $\text{km}^2$ )

128 of the global land area (Sartori, 2000). This study was thus considered relevant as it  
129 generally reflects the erodible nature of similar loess soils under similar management  
130 regimes. In the future, more experiments with soils of different aggregation and  
131 various SOC contents have to be carried out to expand our knowledge on the effects  
132 of aggregation to a wider range of soils.

133 TABLE 1

## 134 **2.2. Experimental set-up**

### 135 *2.2.1. Rainfall simulation*

136 The experiments consisted of three separate components: 1) rainfall simulation to  
137 sufficiently destroy aggregates, so as to ensure that the eroded sediments were less  
138 likely to experience further breakdown during the subsequent settling velocity  
139 measurements; 2) fractionation of the eroded sediments by a settling tube apparatus  
140 into six settling velocity classes; and 3) measurements of the instantaneous  
141 respiration rates of each settling class. The experiments were repeated three times in  
142 order to generate reliable erosion and respiration data.

143 Soils (0 - 5 cm depth) were placed in a 150 × 80 cm flume, which was pitched at a 15%  
144 gradient (Figure 1a). Preliminary tests revealed that a flume of this size could  
145 generate sufficient runoff to initiate non-selective erosion on this particular silt loam.  
146 The soil was sieved into aggregates of a diameter less than 10 mm and over-sized  
147 clods were excluded in order to reduce variations in surface roughness, both within  
148 the flume and between replicates. Levelling the surface also ensured that large  
149 roughness elements, in particular depressions, did not inhibit movement of  
150 aggregates across the flume and thereby prevent selective deposition on the soil  
151 surface. To assist drainage, the base of the flume was perforated and covered with a

152 fine cloth and a layer of sand (c.a., 5 cm). A FullJet nozzle of ¼ HH14WSQ, installed  
153 1.8 m above the soil surface, was used to generate rainfall. Soil of each replicate was  
154 then subjected to simulated rainfall at an intensity of 55 mm·h<sup>-1</sup> for 3 h. The kinetic  
155 energy of the raindrops, detected by a Joss-Waldvogel-Disdrometer, was on average  
156 200 J·m<sup>-2</sup>·h<sup>-1</sup>.

157 Natural precipitation events of 55 mm·h<sup>-1</sup> are unlikely in the Möhlin region, where  
158 precipitation intensity is mostly less than 35 mm·h<sup>-1</sup> (return period of 0.33 years,  
159 MeteoSwiss, 2013). Increased intensity is often considered necessary to compensate  
160 for the deficiency of kinetic energy associated with simulated rainfalls in order to  
161 recreate conditions that were as comparable as possible with natural rainfalls  
162 (Dunkerley, 2008; Iserloh et al., 2012, 2013). A previous study had shown that full  
163 crust formation on the Möhlin silty loam (aggregates < 8 mm) requires a cumulative  
164 kinetic energy of about 340 J·m<sup>-2</sup> (Hu et al., 2013a). This corresponds to natural  
165 precipitation of 35 mm·h<sup>-1</sup> for 30 min (Iserloh et al., 2012). Therefore, a simulated  
166 rainfall of 55 mm·h<sup>-1</sup> lasting for 3 h with a cumulative kinetic energy about 600 J·m<sup>-2</sup>  
167 was chosen in this study to make sure that the aggregates (coarser than those in Hu  
168 et al., 2013a) would experience full crust formation to equilibrium conditions, i.e.  
169 resistance of crust against erosion equals the erosive force of raindrops and runoff.

170 FIGURE 1

171 Tap water, with an electric conductivity of 2220 µs·cm<sup>-1</sup>, which is five times higher  
172 than natural rainwater in Basel, was used during each rainfall simulation. In general,  
173 the increased electric conductivity associated with tap water increases soil dispersion  
174 during tests using simulated rainfall (Borselli et al., 2001). Despite this, however,  
175 comparative aggregate stability tests showed only a 7% difference between rainwater  
176 sampled in Basel and ordinary tap water; thus making it acceptable.

177 *2.2.2. Sediment collection and fractionation by a settling tube apparatus*

178 During each rainfall event, runoff and sediment were continuously collected over 30  
179 min intervals. A 1.8m settling tube (Figure 1b) was used to fractionate the eroded  
180 sediment fractions according to their respective settling velocities. The settling tube  
181 apparatus consists of four components (Figure 1a): the settling tube, through which  
182 the soil sample settles; the injection device, by which the soil sample is introduced  
183 into the tube; the turntable, within which the fractionated subsamples are collected;  
184 and the control panel, which allows an operator to control the rotational speed and  
185 resting/moving intervals of the turntable. Details about the settling tube apparatus  
186 were described in Hu et al. (2013b). The injection device within this particular settling  
187 tube has a volume of 80 cm<sup>3</sup>. As this limits the amount of sediment used during each  
188 test, only sediment collected during the first 10 min of each 30 min interval was used  
189 to determine settling velocities. In total, there were six sediment collection intervals  
190 over the 3 h rainfall events, and a settling fractionation test was carried for each of  
191 the six sediment collection intervals. Prior to being subjected to settling fractionation,  
192 the eroded sediment was allowed to settle for 1 h in collection beakers (height of 20  
193 cm). Measurements confirmed that > 95% of the total mass settled after this pre-  
194 treatment. The supernatant and remaining suspended sediment (corresponding to  
195 EQS < 8 µm) was then decanted off and added to the < 20 µm fraction remaining in  
196 suspension in the settling tube (described as following).

197 Six particle size classes, based on the concept of Equivalent Quartz Size (EQS)  
198 described in Hu et al. (2013b), were selected according to their likely transport  
199 distances after erosion (Table 2). EQS represents the diameter of a nominal  
200 spherical quartz particle that would fall with the same velocity as the aggregated  
201 particle for which fall velocity is measured (Loch, 2001). The six EQS classes were

202 converted to six settling velocities and corresponding settling times using Stokes'  
203 Law (Hu et al., 2013b). The use of Stokes' Law to convert EQS into settling velocity is,  
204 in the strictest sense, limited to particles  $< 70 \mu\text{m}$  (Rubey, 1933). From the  
205 perspective of terrestrial and aquatic systems, however, sediment fractions coarser  
206 than  $63 \mu\text{m}$  are considered as one group that is likely to be re-deposited along  
207 hillslopes. Therefore, the potential error when using Stokes' Law to calculate the  
208 settling velocities of fractions of all sizes is considered acceptable. For soils  
209 dominated by larger mineral grains, different relationships should be used (Ferguson  
210 and Church, 2004; Wu and Wang, 2006). In addition, fine suspended fractions are  
211 considered as one group exported out of the terrestrial system. Hence, with the  
212 current settling tube (length of 1.8 m), any fractions finer than  $20 \mu\text{m}$  (settling time  
213 longer than 1.5 h) were not further fractionated to save time. After fractionation, the  
214 six EQS classes were air-dried for 72 h in a dark environment at ambient temperature  
215 ( $20^{\circ}\text{C}$ ). Despite the possibility of biasing the mineralization SOC potential through the  
216 process of air-drying, as the first step to unwrap the complex effects of aggregation  
217 onto SOC erosion, transport, and deposition, our aim was to produce quasi-natural  
218 sediments, i.e., subjecting to a single rainfall event, successively re-deposited after  
219 increasing transport distances and immediately dried afterwards. Further effects of  
220 multiple rainfall events, other soil moisture conditions (e.g., wet sediments) and long-  
221 term incubation will be investigated in future research, once the role of aggregation  
222 on eroded SOC has been studied.

223 TABLE 2

### 224 *2.2.3. Instantaneous respiration rate measurement*

225 Instantaneous respiration rates were measured, based on the method described in  
226 Robertson et al. (1999) and Zibilske, (1994). In brief, two grams (dry weight) of each

227 EQS size fraction were placed into a 30 ml vial and re-wetted using distilled water in  
228 order to obtain a gravimetric moisture content equivalent to ca. 60%. Preliminary  
229 tests revealed that the gravimetric moisture of 60% represented a proper  
230 intermediate moisture level for sediment fractions of various surface areas, and thus  
231 exerted comparable effects on soil respiration rates (Xu et al., 2004; Bremenfeld et  
232 al., 2013). The re-wetting was done on the previous day before the respiration  
233 measurements. This way, the initial CO<sub>2</sub> pulses of rewetted soils should be largely  
234 excluded (Orchard and Cook, 1983). Even if there were any CO<sub>2</sub> pulses induced by  
235 rewetting, this exactly mimics the natural processes, where dry sediments deposited  
236 from previous rainfall events, experience a second time of erosion and transport  
237 processes. All the re-wetted fractions were then incubated over night at 25°C (vials  
238 open). Two grams of original undisturbed soil were also prepared in the same way  
239 and used to generate reference measurements. Prior to soil respiration  
240 measurements, all vials were sealed using rubber stoppers. Gas from the headspace  
241 of each sealed vial was extracted by a 1 cc syringe at the beginning and end of the 1  
242 h sampling period. Differences in CO<sub>2</sub> concentrations between these two  
243 measurements, as measured on a SRI8610C Gas Chromatograph, were used to  
244 calculate the instantaneous respiration rate.

#### 245 *2.2.4. Laboratory measurements and data analyses*

246 Soil erosion rates for each 30 min interval were estimated by the mass of sediment  
247 samples both from the beginning 10 min (sum of the six EQS classes) and the late 20  
248 min (not fractionated by the settling tube). Runoff samples collected during the late  
249 20 min of each 30 min interval were allowed to settle for more than 48 h. The  
250 supernatant was then decanted off and the sediment was dried at 40°C and weighed.  
251 The SOC content of all the samples was measured by a LECO RC 612 at 550°C.

252 Data analysis was carried out using Microsoft Excel 2010 and R studio software  
253 packages (R version 2.15.1).

254

### 255 **3. Results**

256 Runoff began after 20 min. of rainfall and attained steady state conditions equivalent  
257 to  $18 \text{ mm}\cdot\text{h}^{-1}$  after 120 min. Sediment discharge rates followed a similar pattern and  
258 reached steady state of  $168.7 \text{ g}\cdot\text{m}^{-2}\cdot\text{h}^{-1}$ . Detailed erosional responses are listed in  
259 Table 3. During the simulated rainfall events, the sediments were seen to move  
260 continuously with runoff, and no evident selective deposition was observed on the  
261 soil surface.

262

#### TABLE 3

263 The fraction mass and SOC in the six EQS classes of sediment are presented in  
264 Figures 2 and 3. Preliminary data analysis had shown that while the absolute  
265 sediment mass increased during the simulated rainfall events, the proportional  
266 composition of six EQS classes in each sediment collection interval did not differ  
267 significantly between samples (ANOVA, single factor,  $P > 0.05$ ,  $n = 18$ ). Hence, only  
268 proportional values are presented, and each EQS class could be considered to have  
269 18 replicates (6 sediment collection intervals during each of the 3 rainfall events).  
270 Nevertheless, the distribution of fraction mass and SOC content considerably differed  
271 across six EQS classes: about 61% of the sediment fractions were in EQS of 32 to  
272  $63 \mu\text{m}$  and 63 to  $125 \mu\text{m}$ , containing about 65% of the SOC. This SOC distribution in  
273 six EQS classes of sediment also contrasts against the association of SOC with  
274 mineral particles in the original soil (Table 1).

275

#### FIGURE 2

276

FIGURE 3

277 The instantaneous respiration rates from EQS classes of 32 to 63  $\mu\text{m}$  and 63 to 125  
278  $\mu\text{m}$  were on average lower than that from other fractions (Figure 4a). However, after  
279 multiplying the respiration rate from each class with its fraction mass (Figure 2), EQS  
280 classes of 32 to 63  $\mu\text{m}$  and 63 to 125  $\mu\text{m}$  on average released even more amount of  
281  $\text{CO}_2$  than all other finer or coarser classes did (Figure 4b). The instantaneous  
282 respiration rates per gram of SOC also differ among different EQS classes. In EQS  
283 classes  $< 20 \mu\text{m}$  and 20 to 32  $\mu\text{m}$ , the instantaneous respiration rates per gram of  
284 SOC were lower than that in the original soil (Figure 5). In contrast, all the other four  
285 EQS classes ( $> 32 \mu\text{m}$ ) had higher instantaneous respiration rates per gram of SOC  
286 than the original soil (Figure 5). We attribute the increased respiration rates per gram  
287 of SOC in EQS classes  $> 32 \mu\text{m}$  to the detachment and transport of eroded soils,  
288 during which time the structural aggregates were broken down, thereby exposing the  
289 previously protected SOC to microbial processes (Six et al., 2002; Lal and Pimentel,  
290 2008; van Hemelryck et al., 2010).

291

FIGURE 4

292

FIGURE 5

293

## 294 **4. Discussion**

### 295 **4.1. Likely fate of eroded SOC in the terrestrial and aquatic system**

296 Fractionation of eroded sediment by settling velocity shows that aggregation of  
297 source soil has a clear potential to affect the movement of sediment fractions and  
298 thus the fate of the associated SOC after erosion. According to the conceptual model

299 developed by Starr et al. (2000) (Figure 6), the six EQS classes can be further  
300 grouped into three separate groups, each with a different likely fate: EQS < 20  $\mu\text{m}$   
301 would be likely to remain suspended in runoff and hence, transferred to rivers, and all  
302 EQS > 63  $\mu\text{m}$  would be re-deposited along eroding hillslopes (Table 2). The  
303 intermediate EQS of 20 to 32  $\mu\text{m}$  and 32 to 63  $\mu\text{m}$  can have either fate, depending on  
304 localised flow hydraulics. In accordance with this model, approximately 41% of the  
305 eroded SOC from the silt loam used in this study would be re-deposited along  
306 eroding hillslopes (Figure 7b). This proportion strongly contrasts against the  
307 approximately 11% SOC mass associated with coarse mineral particles > 63  $\mu\text{m}$  in  
308 the original soil (Table 1), and is also contrary to the high SOC content (24.3  $\text{mg}\cdot\text{g}^{-1}$ )  
309 in sediment fraction of EQS < 20  $\mu\text{m}$  (Figure 3a). These results support our  
310 theoretical deduction that aggregation of source soil reduces the likely transport  
311 distance of eroded SOC. This would then decrease the likelihood of eroded SOC  
312 being transferred from eroding hillslopes to aquatic systems, but increase the amount  
313 of eroded SOC being re-deposited into terrestrial systems. These findings are  
314 consistent with those reported by Hu et al. (2013b), in which 79% of the eroded SOC  
315 mass in a silty loam was associated with mineral particles of size < 32  $\mu\text{m}$ , whereas  
316 73% of the SOC mass was actually contained in aggregates of EQS > 63  $\mu\text{m}$ . The  
317 distinct SOC distribution across aggregate size classes also agrees with the field  
318 investigation by Polyakov and Lal (2008), where the coarse aggregates (1 to 0.5 mm)  
319 fractionated by wet-sieving, contained up to 4.5 times more SOC than the finest  
320 fraction (< 0.05 mm). More experiments are required to describe the effects of  
321 different aggregation degrees and SOC contents.

322 FIGURE 6

323 FIGURE 7

## 324 4.2. Erosion as a source of CO<sub>2</sub> flux

325 The effect of aggregation on the likely fate of SOC may also cast new light on  
326 understanding the effect of soil erosion on global carbon cycling. Based on the EQS  
327 specific SOC content (Figure 3), the potential SOC stock of a nominal 25 cm layer of  
328 topsoil on the foot-slope of a colluvial depositional site, assumingly composed of  
329 aggregates EQS > 63 µm, would be 5.1 kg·m<sup>-2</sup> on average (Table 4). The potential  
330 SOC stock from the same 25 cm layer of original soil would be only 4.5 kg·m<sup>-2</sup>, or  
331 15.5% lower than that on the foot-slope of a colluvial depositional site. Such a large  
332 difference implies that a combined model approach (Equation 1), integrating the  
333 effects of aggregation on the likely fate of SOC, is demanded to adequately  
334 distinguish the proportion of SOC likely re-deposited along hillslopes from the portion  
335 potentially transferred to aquatic systems.

$$336 S_d \times C_d = S_e \times C_e - S_a \times C_a - C_{min} \quad (\text{Equation 1})$$

337 Where,  $S_d$ : mass of sediment likely to be re-deposited along hillslopes ;  $C_d$ : carbon  
338 content of sediment likely to be re-deposited along hillslopes ;  $S_e$ : mass of eroded soil;  
339  $C_e$ : carbon content of eroded soil;  $S_a$ : mass of sediment potentially to be transferred  
340 to aquatic systems;  $C_a$ : carbon content of sediment potentially to be transferred to  
341 aquatic systems;  $C_{min}$ : carbon mineralized during transport.

342 TABLE 4

343 In previous reports,  $C_{min}$  was considered to be a minor constituent in the overall  
344 carbon budget, and  $C_d$  was often assumed equivalent to the average of  $C_e$  (Stallard,  
345 1998; Harden et al., 1999; Berhe et al., 2007; van Oost et al., 2007; Quinton et al.,  
346 2010). However, if presuming that  $C_e$  equals  $C_d$  observed in topsoil of colluvial  
347 depositional sites (e.g., in van Oost et al., 2012), then the  $C_d$  would lead to an

348 overestimation of total SOC loss from eroding sites, because  $C_d$  is likely enriched by  
349 SOC-rich aggregates compared to  $C_e$  due to preferential deposition. Conversely,  
350 assuming  $C_d$  corresponds to  $C_e$  observed in topsoil at eroding sites (e.g., in Dlugoß et  
351 al., 2012), would neglect the potential enrichment of SOC in sediment fractions  
352 preferentially deposited on hillslopes. This would thus lead to an underestimation of  
353  $C_{min}$  during transport. In both cases, SOC transferred to aquatic systems would be  
354 overestimated. The observed enrichment of SOC by 15.5% in sediment fractions  
355 composed only of EQS > 63  $\mu\text{m}$ , indicates that the potential error of above-described  
356 estimates could be considerable. A 15.5% SOC enrichment of sediment re-deposited  
357 in the terrestrial system corresponds to the proportion of eroded SOC estimated to be  
358 deposited in permanent sinks (e.g., 0.12 Pg of SOC eroded per year by van Oost et  
359 al. 2007). While the effects of aggregation on SOC redistribution and subsequent fate  
360 cannot be assessed based on one experiment, most sediment is transported in form  
361 of aggregates (Walling, 1988; Walling and Webb, 1990). Ignoring the effect of  
362 aggregation on erosion and redistribution of SOC, therefore, bears the risk of  
363 overestimating the erosion-induced carbon sink effect. As a consequence, the  
364 behavior of aggregated sediment requires a reconsideration of existing approaches  
365 of sediment behavior in erosion models. Further study of different soil types, their  
366 aggregation and aggregate breakdown while moving through landscapes of varying  
367 topography during rainfall events of different intensity, frequency and duration, is  
368 required to assess the relevance of aggregation for SOC movement and fate  
369 identified in this study.

370 The risk of falsely estimating SOC losses during transport is further exacerbated by  
371 the observed instantaneous respiration rates. The instantaneous respiration rates  
372 probably merely represent a spike of SOC mineralization after erosion, and therefore,

373 should not be extrapolated over longer periods of time. However, the 41% proportion  
374 of eroded SOC, which would likely be re-deposited along hillslopes, generated 53%  
375 of the entire instantaneous respiration (Figure 7c). This implies that the immediately  
376 deposited SOC is more susceptible to mineralization than both the mass of coarse  
377 sediment fractions and their SOC content would suggest. These findings are  
378 consistent with those observed by van Hemelryck et al. (2010), who reported that a  
379 significant fraction of SOC eroded from initially dry soil aggregates is mineralized  
380 after deposition. As a consequence, the preferentially deposited SOC could  
381 potentially generate a further error in the carbon source-sink balance. Such error  
382 would be particularly significant, when repeated erosion and deposition processes  
383 along hillslopes cause further disintegration of large aggregates (Kuhn et al., 2003;  
384 van Hemelryck et al., 2010). This would thereby result in additional SOC exposure  
385 and mineralization (Jacinthe et al., 2002; Six et al., 2002). Overall, as a result of  
386 preferential deposition of SOC-enriched sediment fractions and enhanced  
387 mineralization during transport, the carbon losses during transport, so far assumed to  
388 be small (van Oost et al., 2007; Quinton et al., 2010), would actually be  
389 underestimated.

390

## 391 **5. Conclusion**

392 This study aimed to identify the effects of aggregation of source soil on the likely  
393 transport distance of eroded SOC and its susceptibility to mineralization after single-  
394 event transport and deposition. Our data show that 41% of the eroded SOC from a  
395 silty loam was incorporated into aggregates of EQS > 63  $\mu\text{m}$ , and hence would likely  
396 be re-deposited into the terrestrial system rather than being transferred to the aquatic  
397 system. This proportion is much greater than the approximately 11% SOC mass

398 associated with coarse mineral particles > 63  $\mu\text{m}$  in the original soil (Table 1), and the  
399 high SOC content (24.3  $\text{mg}\cdot\text{g}^{-1}$ ) in sediment fraction of EQS < 20  $\mu\text{m}$  would suggest.  
400 Respiration rates from sediment fractions of EQS > 63  $\mu\text{m}$  also increased  
401 immediately after erosion and deposition. Both results indicate that aggregation of  
402 source soil and preferential deposition of SOC-rich coarse sediment fractions may  
403 skew the re-deposition of eroded SOC towards the terrestrial system, rather than  
404 further transfer to the alluvial or aquatic system. Consequently, a risk of  
405 overestimating lateral SOC transfer exists when mineral grain size rather than actual  
406 size of aggregated sediment is applied in erosion models. Our very limited data  
407 indicates that this error could be potentially within the same range as the current  
408 estimate of annual net erosion-induced carbon sink rate.

409 While based on a laboratory experiment and thus with very limited applicability to real  
410 landscapes, the potential effects of aggregation of source soil on reducing the  
411 transport distance of eroded SOC appear to be considerable. This illustrates the  
412 need to integrate the effect of aggregation of source soil on SOC transport distance  
413 into soil erosion models (e.g., as a soil erodibility parameter), in order to adequately  
414 distinguish SOC likely re-deposited in the terrestrial system from the portion  
415 potentially transferred to aquatic systems, and further assess the implications to the  
416 global carbon cycle. Further research should, therefore, focus on the effects of  
417 preferential deposition of eroded aggregates and the fate of SOC in these  
418 aggregates whilst in-transit and during multiple rainfall events. More simulations as  
419 well as field experiments are also needed to examine the effects of various transport  
420 processes (such as slope length, slope gradients, field barriers) onto the mechanism  
421 of aggregate breakdown and aggregate specific SOC distribution. The effects of  
422 varying rainfall characteristics, crust formation, soil management and topography

423 (e.g., Wang et al., 2008; Hu et al., 2013a) onto SOC transport should also be  
424 investigated.

425

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434 much too premature and who is still sorely missed in the department.

435

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600

601 **Table 1** Mineral particle size distribution, soil organic carbon (SOC) distribution  
 602 across mineral particle size, average SOC of bulk soil, and the percentage of stable  
 603 aggregates greater than 250  $\mu\text{m}$  in the silty loam used in this study.

	Mineral particle size ( $\mu\text{m}$ )					SOC of original soil ( $\text{g kg}^{-1}$ )	Aggregates greater than 250 $\mu\text{m}$ (%)
	< 32	32-63	63-125	125-250	> 250		
Weight (%)	62.0 $\pm 0.3$	29.1 $\pm 0.4$	6.6 $\pm 0.3$	1.2 $\pm 0.1$	1.1 $\pm 0.1$		
SOC ( $\text{g kg}^{-1}$ )	13.7 $\pm 0.7$	3.0 $\pm 0.3$	8.9 $\pm 2.6$	21.9 $\pm 0.8^a$	26.4 $\pm 1.3^a$	10.8 $\pm 0.4$	67.2 $\pm 6.9$
SOC mass proportion (%)	80.8	8.3	5.6	2.5	2.8		

604 NOTE: a) might be over-estimated due to the mixture of minute amount of residue or straw, which was previously incorporated  
 605 into the aggregates but then released by dispersion and blended with coarse particles.  
 606 Lower case numbers indicate the range of minimum and maximum values ( $n = 3$ ).  
 607  
 608

609 **Table 2** Six settling velocities based on the Equivalent Quartz Size (EQS) classes,  
 610 and the likely fate of eroded fractions based on the conceptual model developed by  
 611 Starr et al. (2000).

EQS ( $\mu\text{m}$ )	Settling velocity ( $\text{m}\cdot\text{s}^{-1}$ )	Likely fate
< 20	Suspension	Likely transferred to rivers
20 - 32	$3.3 \times 10^{-4} - 1.0 \times 10^{-3}$	Possibly transferred to rivers
32 - 63	$1.0 \times 10^{-3} - 3.0 \times 10^{-3}$	
63 - 125	$3.0 \times 10^{-3} - 1.5 \times 10^{-2}$	Deposited along eroding hillslopes
125 - 250	$1.5 \times 10^{-2} - 4.5 \times 10^{-2}$	
> 250	$> 4.5 \times 10^{-2}$	

612

613

614 **Table 3** Summary of the erosional responses of Möhlin soil over 180 min of rainfall  
 615 time. Subscripted numbers indicate the minimum and maximum range of the  
 616 parameters ( $n = 3$ ).

Steady state (after 120 min)			Total runoff (kg)	Runoff coefficient (%)	Total sediment yield (g)
Runoff rate (mm·h <sup>-1</sup> )	Sediment discharge rate (g·m <sup>-2</sup> ·h <sup>-1</sup> )	Sediment concentration (g·L <sup>-1</sup> )			
18.0 ±0.9	168.7 ±14.4	9.4 ±0.1	40.7 ±3.1	20.6 ±1.6	475.8 ±74.6

617

618 **Table 4** Comparison between soil organic carbon (SOC) stock in top layer of 25 cm  
 619 from a temporary depositional site which is theoretically composed of only three  
 620 Equivalent Quartz Size (EQS) classes, and SOC stock of average original soil in the  
 621 same top layer of 25 cm, as often applied in previous literature.

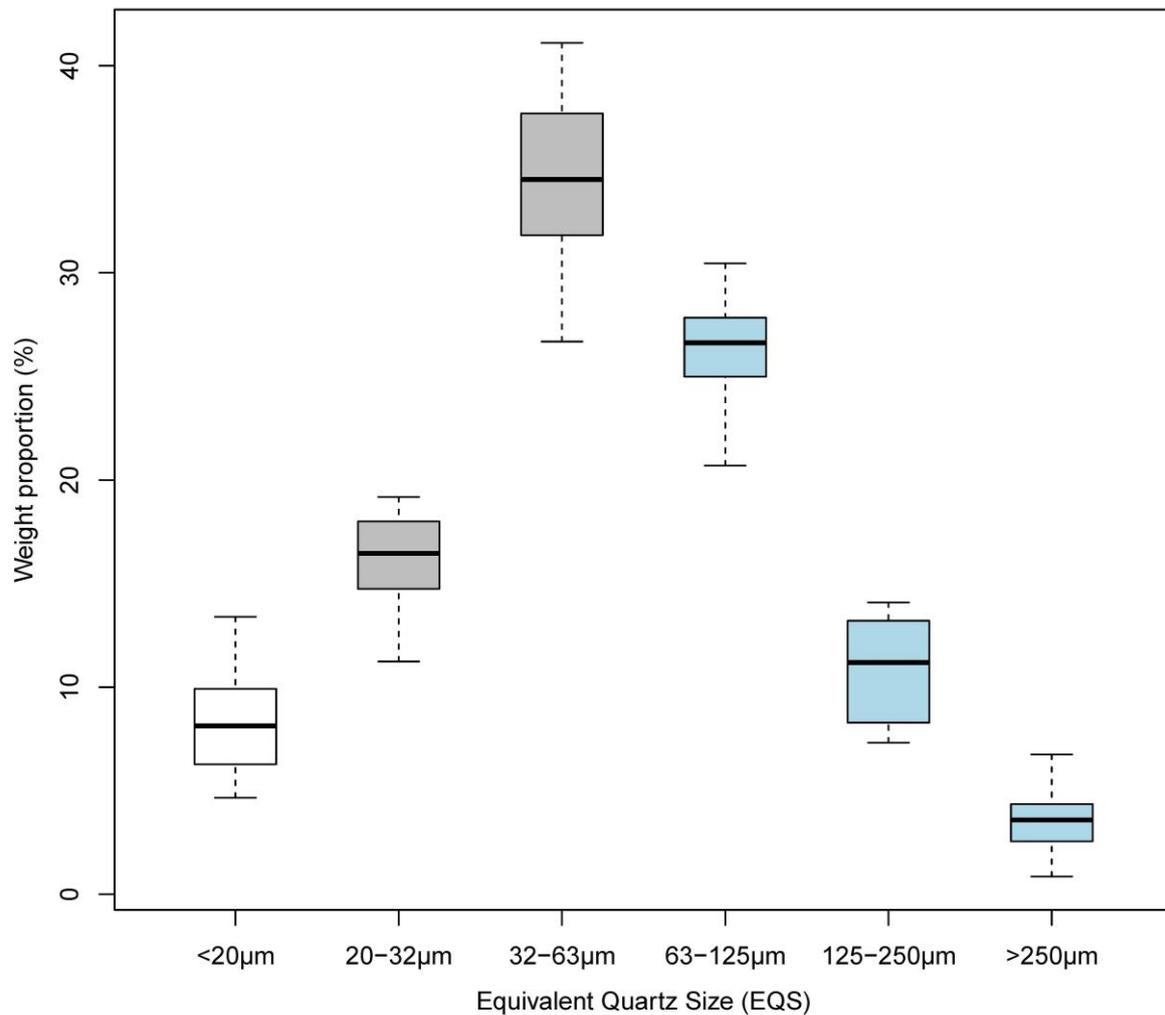
	EQS	SOC content (mg g <sup>-1</sup> )	SOC stock (kg m <sup>-2</sup> ) <sup>a</sup>	Differences (%) <sup>b</sup>	Average SOC stock (kg m <sup>-2</sup> )	Average differences (%) <sup>b</sup>
Re-distributed fractions	> 250	12.2	5.0	-11.1	5.1	-15.5
	125 - 250	15.7	6.5	-44.4		
	63 - 125	9.6	4.0	+11.1		
Original soil	NA	10.8	4.5	NA	4.5	NA

622 NOTE: a. Accurate bulk densities for sediment fractions of different aggregate sizes are not available, so only particle density  
 623 1.65 g cm<sup>-3</sup> is applied here to form a preliminary comparison.

624 b. Minus (-) means underestimation compared to the original soil; Plus (+) means overestimation compared to the  
 625 original soil.  
 626



627  
628 **Figure 1** The rainfall simulation flume (a), and the settling tube apparatus (b). The  
629 settling tube apparatus consists of four components: the settling tube, through which  
630 the soil sample settles; the injection device, by which the soil sample is introduced  
631 into the tube; the turntable, within which the fractionated subsamples are collected;  
632 and the control panel, which allows an operator to control the rotational speed and  
633 rest intervals of the turntable (operations see Hu et al., 2013b)).



635

636

**Figure 2** The weight distribution of different Equivalent Quartz Size (EQS) classes of

637 the sediment. Colors of the boxes correspond to the likely fate of each fraction after

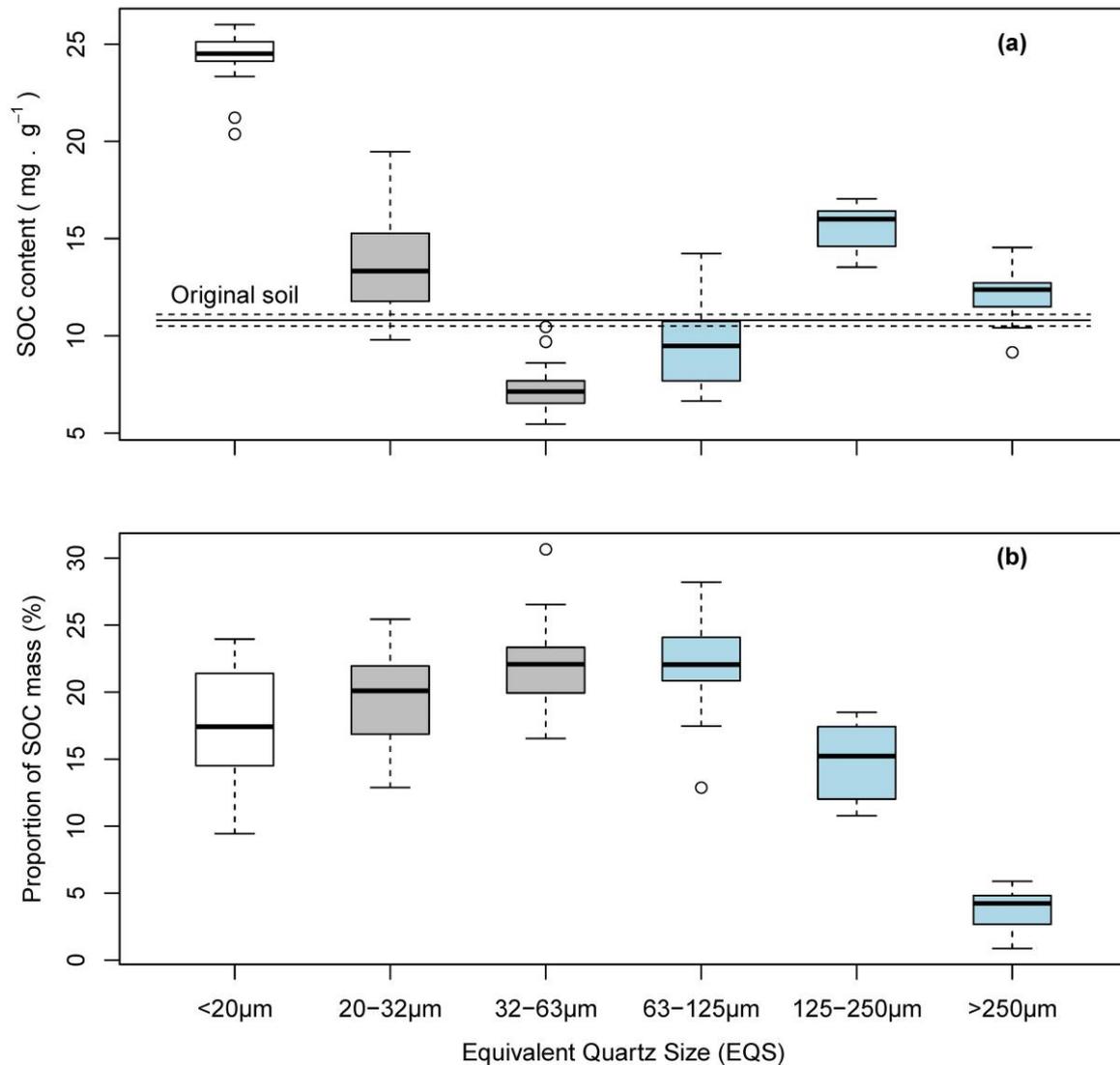
638 erosion. See section 4.1 and Figure 6 for definitions and explanation of the three

639 manners of likely fate. Bars in the boxes represent median values. Whiskers indicate

640 the lowest datum within 1.5 interquartile range of the lower quartile, and the highest

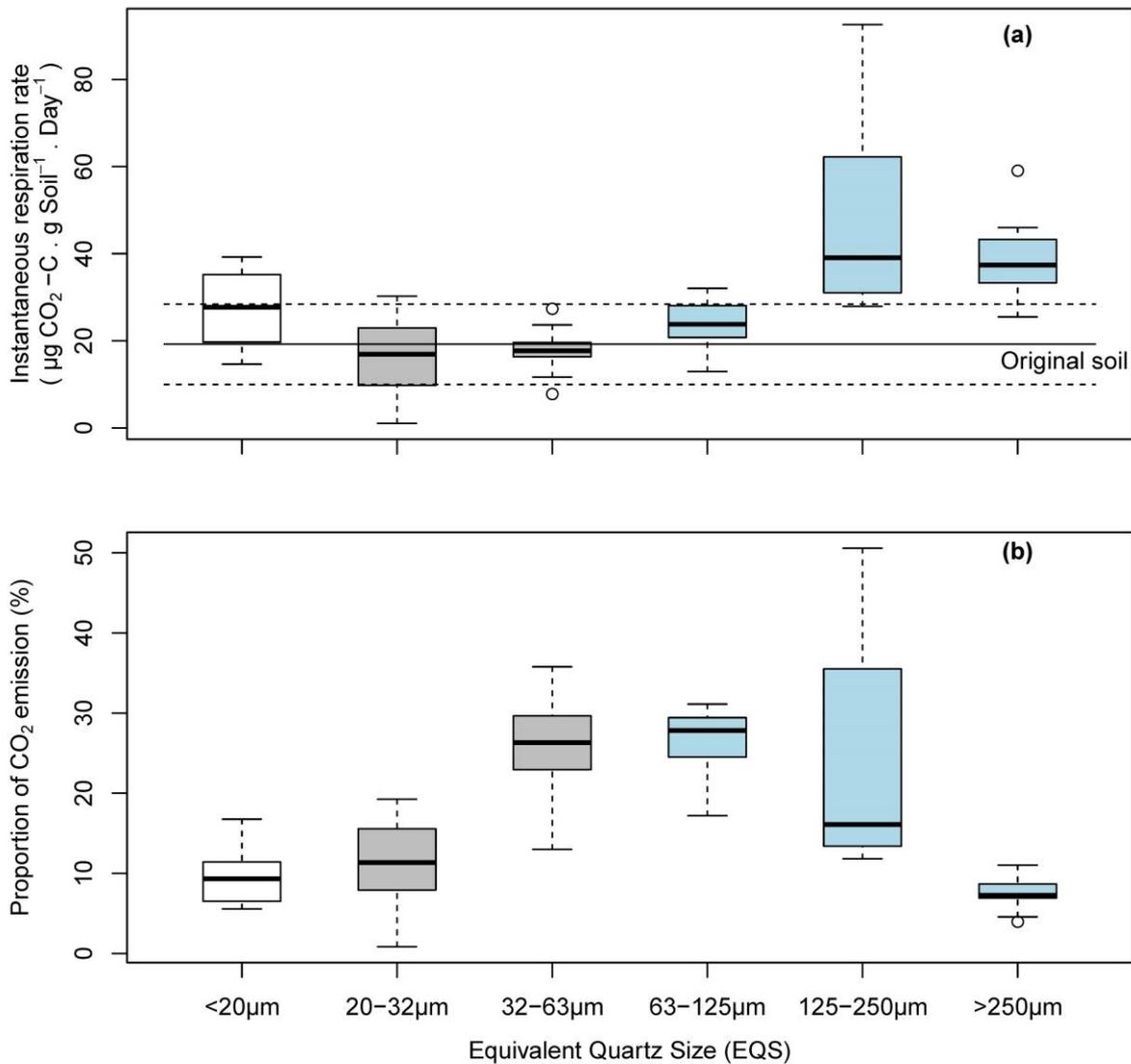
641 datum within 1.5 interquartile range of the upper quartile ( $n = 18$ ).

642



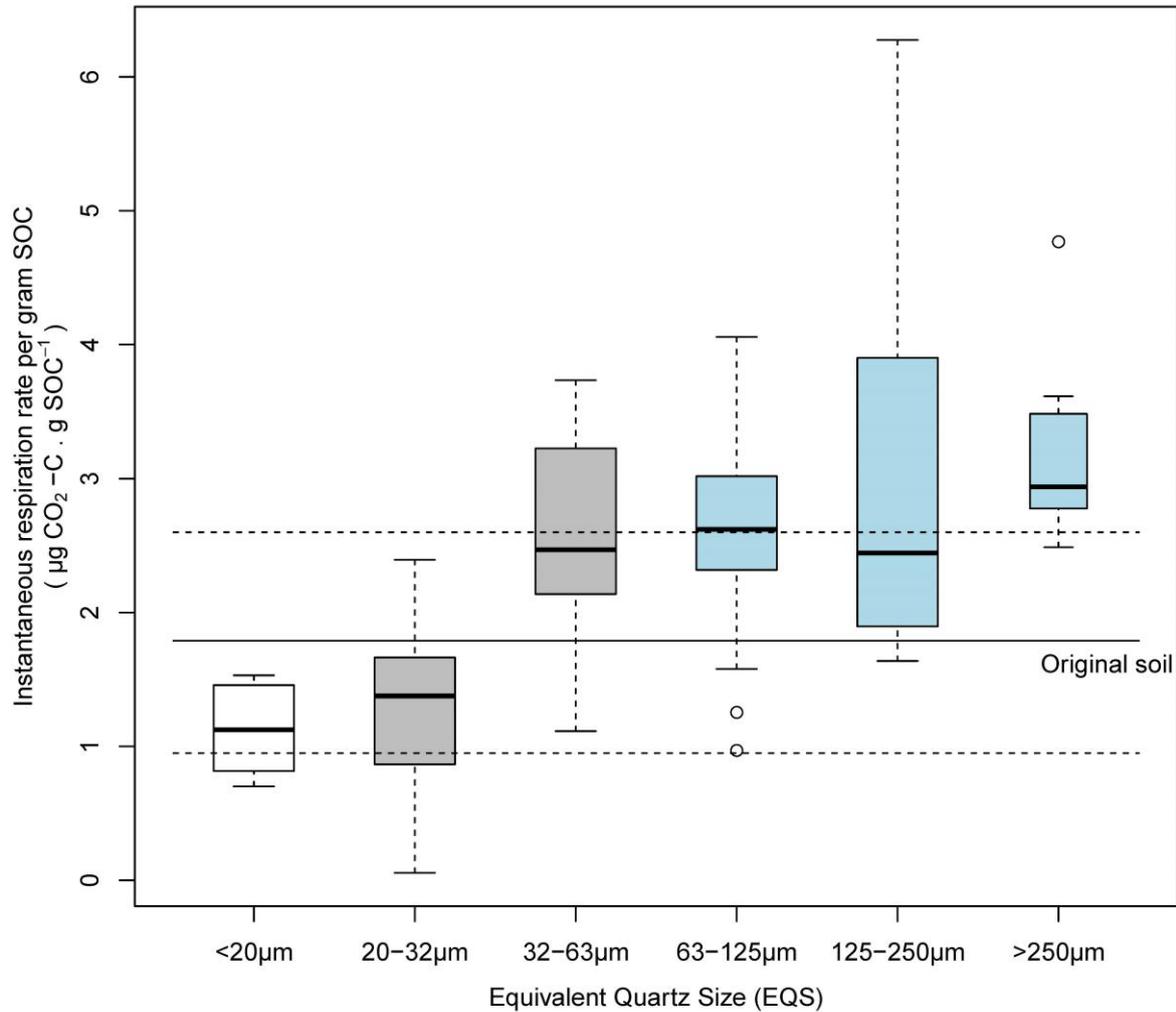
643  
 644 **Figure 3** The distribution of soil organic carbon content (SOC) (a), and soil organic  
 645 carbon (SOC) mass (b) in different Equivalent Quartz Size (EQS) classes of the  
 646 sediment. The bold and dashed lines in (a) denote the average and standard  
 647 deviation of soil organic carbon (SOC) of the original soil. Colors of the boxes  
 648 correspond to the likely fate of each fraction after erosion. See section 4.1 and Figure  
 649 6 for definitions and explanation of the three manners of likely fate. Bars in the boxes  
 650 represent median values. Whiskers indicate the lowest datum within 1.5 interquartile  
 651 range of the lower quartile, and the highest datum within 1.5 interquartile range of the  
 652 upper quartile ( $n = 18$ ).

653



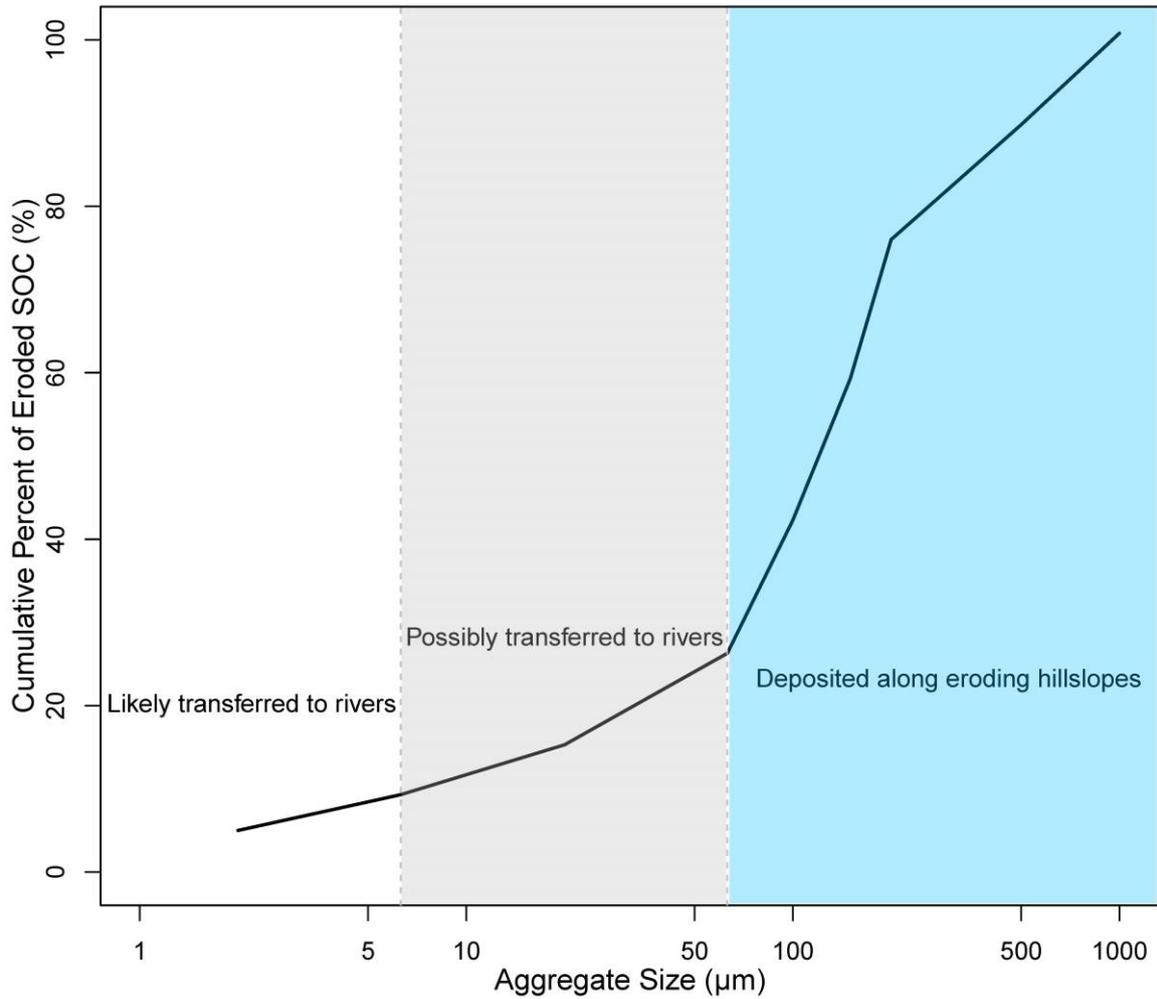
654  
 655 **Figure 4** The distribution of instantaneous respiration rate (a); and potential CO<sub>2</sub>  
 656 emission (b) in different Equivalent Quartz Size (EQS) classes of the sediment. The  
 657 bold and dashed lines in (a) denote the average and standard deviation of  
 658 instantaneous respiration rate of the original soil. Colors of the boxes correspond to  
 659 the likely fate of each fraction after erosion. See section 4.1 and Figure 6 for  
 660 definitions and explanation of the three manners of likely fate. Bars in boxes  
 661 represent median values. Whiskers indicate the lowest datum within 1.5 interquartile  
 662 range of the lower quartile, and the highest datum within 1.5 interquartile range of the  
 663 upper quartile ( $n = 18$ ).

664



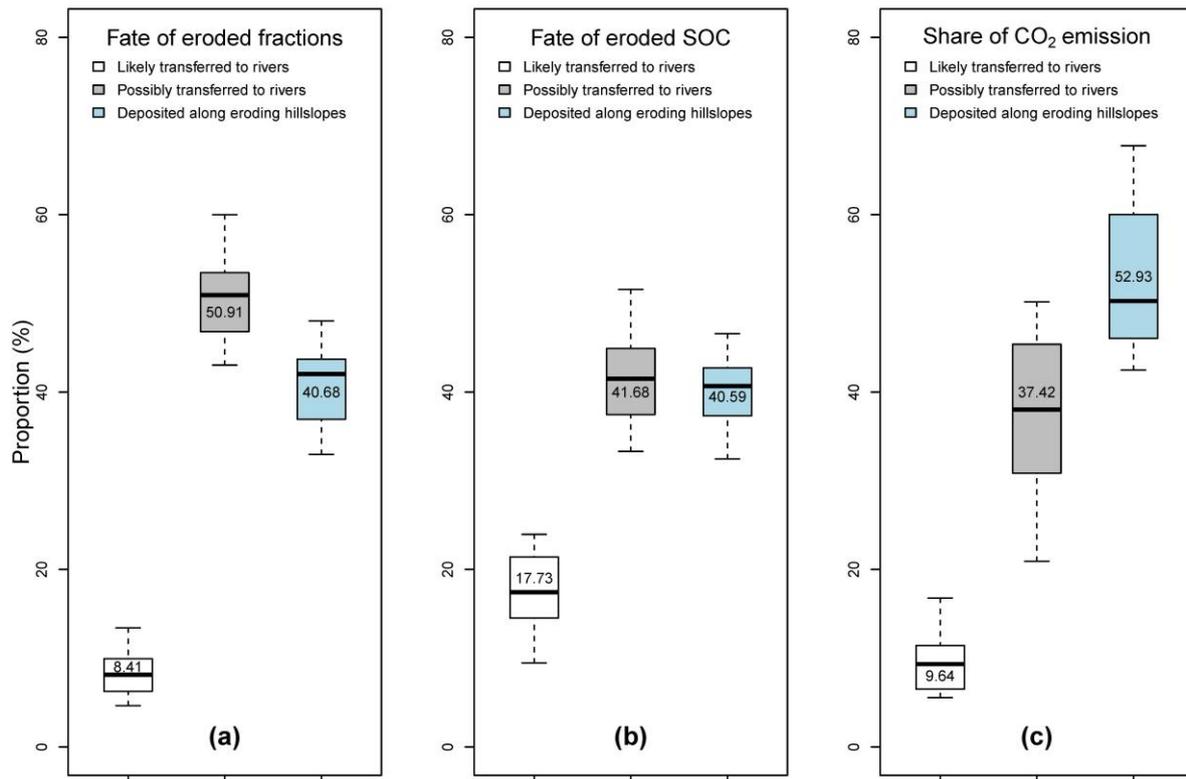
665  
 666 **Figure 5** The distribution of instantaneous respiration rate per gram of soil organic  
 667 carbon (SOC) in different Equivalent Quartz Size (EQS) classes of the sediment. The  
 668 bold and dashed lines denote the average and standard deviation of instantaneous  
 669 respiration rate per gram SOC of the original soil. Colors of the boxes correspond to  
 670 the likely fate of each fraction after erosion. See section 4.1 and Figure 6 for  
 671 definitions and explanation of the three manners of likely fate. Bars in boxes  
 672 represent median values. Whiskers indicate the lowest datum within 1.5 interquartile  
 673 range of the lower quartile, and the highest datum within 1.5 interquartile range of the  
 674 upper quartile ( $n = 18$ ).

675



676  
 677 **Figure 6** Likely fate of eroded soil organic carbon (SOC) as a function of aggregate  
 678 size, re-drawn from the conceptual model developed by Starr et al. (2000). Blocks of  
 679 different colors represent three manners of likely fate of eroded SOC, divided by the  
 680 two convenient cut-off points: aggregate size of 6.3  $\mu\text{m}$  and 63  $\mu\text{m}$ . See section 4.1  
 681 for definitions and explanation of the three manners of likely fate.

682



683

684 **Figure 7** The likely fate of sediment fractions (a), eroded SOC (b), and potential  
 685 share of CO<sub>2</sub> emission (c) by fractions that would have been likely transferred to  
 686 rivers, possibly transferred to rivers, and deposited along eroding hillslopes. The bar  
 687 in box represents the median value, while numbers written in each box denote the  
 688 average value. Whiskers indicate the lowest datum within 1.5 interquartile range of  
 689 the lower quartile, and the highest datum within 1.5 interquartile range of the upper  
 690 quartile ( $n = 18$ ).