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*Supplement of*

## **CO<sub>2</sub> fluxes and ecosystem dynamics at five European treeless peatlands – merging data and process oriented modelling**

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## 1 **Supplemental material**

### 2 ***Calibration procedure***

3 A stepwise approach was used to calibrate model parameter: (I) Parameter ranges of 45  
4 parameters were constrained by applying a Monte Carlo based calibration by multiple runs  
5 with randomized parameter values in a defined range, similar to the Generalized Likelihood  
6 Uncertainty Estimation by Beven and Binley (1992) and Beven (2006). Ranges were selected  
7 according to experiences from previous model runs, in most cases a certain range around the  
8 default values. The list of parameters and their tested ranges are displayed in Table S3. The  
9 output of these runs was compared with several different variables derived from  
10 measurements. A number of performance indicators were considered to define the behavioural  
11 models with an acceptable fit in step I a. Parameter ensembles of accepted behavioural models  
12 were further analysed to identify covariance between parameters and also to understand the  
13 importance and effect of multiple criteria (I b).

14 350'000 runs were executed for each site, except for Hor, for which 700'000 runs were  
15 performed. The higher amount of runs at Hor was motivated by the observed discrepancy in  
16 chamber versus EC derived  $R_{eco}$  values and a wider range for some parameters due to the  
17 relatively high ratio of biomass to GPP.

18 (I a) From these runs, around 75 behavioural models per site were selected according to an  
19 acceptable fit (Tab. S7) to measurement derived  $R_{eco}$  and GPP respectively in case of Hor net  
20 ecosystem exchange (NEE) and plant biomass. Due to their relatively small amplitude, winter  
21 fluxes hardly affect performance indices of the whole year. However they have a high  
22 proportion of soil to plant respiration and are therefore of special interest. Hence, performance  
23 in modelling  $R_{eco}$  and GPP during winter, respectively late autumn in case of Lom (see Tab. 4)  
24 were additionally taken into account. As the ability to constrain parameter values and the  
25 model performance depend on quality and frequency of the available measurement data,  
26 different criteria (Tab. S7) had to be applied for each site.

27 (I b) Performance ( $R^2$ , ME and NSE) of the 75 accepted runs on each variable was plotted  
28 against values for each parameter as well as values for each parameter against values for each  
29 other parameter. These plots were visually analysed to detect covariance between parameters

1 which were further analysed in step III and between parameters and performance which were  
2 further analysed in step I c.

3 (I c) The best fit for one variable does not necessarily lead to the best fit for another variable.  
4 Therefore, a further constraint was achieved by selecting each best 10 out of the 75 runs  
5 independently for each of the variables and each parameter as listed in Table S9. According  
6 the results from I b, different performance indices were used depending on the variable:  $R^2$   
7 was chosen in case of  $R_{\text{eco}}$  and GPP as effect on ME can be compensated by radiation use  
8 efficiency ( $\epsilon_L$ ) in case of GPP and decomposition rate for the fast SOC pool ( $k_I$ ) in case of  
9  $R_{\text{eco}}$ . Mean error was chosen in case of temperature, NSE for all other variables, including  
10 winter  $R_{\text{eco}}$  and winter GPP. This procedure leads to several ranges for each parameter  
11 producing the best performance depending on the variable and the site.

12 (I d) The ranges were merged together to a new range for each parameter, starting with the  
13 highest value of the lower ends of all ranges and lasts to the lowest of the upper ends. These  
14 ranges will be called “overlapping ranges” in the following, even though they did not overlap  
15 in some few cases.

16 (II) Parameters might interact with one or more other parameters and counteract or even  
17 compensate the effect of other parameters. Ranges for such parameters could be same or  
18 overlapping between the sites, but the application of a single set of parameter values might  
19 reveal that only site specific values for one or several of these parameters lead to acceptable  
20 performance. To test this, for each site one of the 75 runs with the highest performance in  $R^2$   
21 of  $R_{\text{eco}}$  selected and  $\epsilon_L$  and  $k_I$  adjusted until ME in GPP and  $R_{\text{eco}}$  was smaller than  $|0.1| \text{ g C m}^{-2}$   
22  $\text{day}^{-1}$ . Afterwards, stepwise each parameter was set to the rounded mean value of the  
23 overlapping range from I d and again  $\epsilon_L$  and  $k_I$  adjusted until ME in GPP and  $R_{\text{eco}}$  was smaller  
24 than  $|0.1| \text{ g C m}^{-2} \text{ day}^{-1}$ . If then the performance in  $R^2$  of  $R_{\text{eco}}$  and GPP was not reduced by  
25 more than 0.05 the modified parameter was kept at this value. Otherwise it was set back to the  
26 previous value and further investigated in III. This procedure was repeated for all parameters  
27 except  $\epsilon_L$  and  $k_I$ .

28 (III) Parameters showing strong interactions or showing different valid ranges for the different  
29 sites or variables were investigated by further multiple calibrations with 2500 to 5000 runs.  
30 For each parameter only this particular parameter and very few other parameters which are  
31 directly related to it were calibrated, while all others were kept constant to the values from  
32 step II. Criteria for accepted runs were a mean error of max  $|0.3| \text{ g C m}^{-2} \text{ day}^{-1}$  in  $R_{\text{eco}}$  and

1 GPP, respectively in GPP and uppermost temperature case of  $p_{ck}$ , to accept 60 to 150 runs.  
2 Such additional multiple calibrations were also performed if the previous results indicated an  
3 optimal range outside the tested range. In this case the calibration range of the parameter was  
4 increased.

5 Then steps I c, d and II were repeated for these additional calibration. If the performance in  $R^2$   
6 of  $R_{eco}$  and GPP was reduced by more than 0.05 the parameter was considered to be site  
7 specific. Again,  $\epsilon_L$  and  $k_l$  were adjusted until ME in GPP and  $R_{eco}$  was smaller than  $|0.1| \text{ g C}$   
8  $\text{m}^{-2} \text{ day}^{-1}$ . This set of parameter values will be called common configuration (C1) in the  
9 following.

10 (IV) Different combination of parameter values might lead to similar good results, which is  
11 called equifinality (Beven, 2006). In those cases were step I to III indicated covariance  
12 between parameters, several different combinations of parameter values leading to similar  
13 good results (ME in GPP and  $R_{eco}$  smaller than  $|0.1| \text{ g C m}^{-2} \text{ day}^{-1}$ ) were tested. Such runs  
14 with a single set of parameter values are called single runs in the following and numbered  
15 with C1 to C7 (Tab. S8).

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19 Beven, K.: A manifesto for the equifinality thesis, *Journal of Hydrology*, 320, 18–36,  
20 doi:10.1016/j.jhydrol.2005.07.007, 2006.

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# 1 **Tables**

## 2 Table S1. Dynamic forcing data

Site	Variable	Period	Resolution of measurement / as used for calibration	number of replicates
Lom	water table	mid 2006-2010	half-hourly/hourly	1
	meteorology (temperature, global radiation, precipitation, wind speed, relative humidity)	mid 2006-2010	half-hourly/hourly	1
Amo	water table	April 2007-2010	half-hourly/hourly	1
	meteorology (temperature, global radiation, precipitation, wind speed, relative humidity)	mid 2006-2010	half-hourly/hourly	1
Hor	water table	2004-2006	half-hourly/hourly	2
	meteorology (temperature, global radiation, precipitation, wind speed, relative humidity)	2004-2011	half-hourly/hourly	1
FsA and FsB	water table	2007-2011	biweekly, since April 2010 half hourly / hourly	1
	meteorology (temperature, global radiation, precipitation, wind speed, relative humidity)	2007-2011	half-hourly/hourly	1

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1 Table S2. Dynamic data for calibrations and comparisons – methods and instruments

Site	Variable	Period	Resolution of measurement / as used for calibration	Method	replicate s	Described in	number of data points
Lom	NEE	mid 2006-10	half-hourly/hourly	EC	1	Aurela et al., 2009)	34895
	R <sub>eco</sub>	2007, 2009, 2010	half-hourly/hourly, summer only	automatic opaque chamber	2	Lohila et al., 2010	27853
	R <sub>eco</sub> , GPP	mid 2006-10	half-hourly/hourly	empirical modelling from EC data	1	Aurela et al., 2009	15236
	winter R <sub>eco</sub>	2006-2010	half-hourly/hourly	empirical modelling from night NEE EC data during Sept.-Nov.	1		6356
	soil temperature at -7 cm	mid 2006-10	half-hourly/hourly	automatic temperature sensors	1		34318
	soil temperature at -60 cm	mid 2006-10	half-hourly/hourly	automatic temperature sensors	1		34318
	LAI	2007-10	4-10 times each summer	optical canopy analyser	9-19		41
	Snow depth	mid 2006-10	hourly	automatic sensor	1		34316
Amo	NEE	mid 2006-10	half-hourly/hourly	EC	1	Drewer et al., 2010	38710
	R <sub>eco</sub>	mid 2006-10	biweekly	manual opaque chamber	9	Dinsmore et al., 2010	57
	R <sub>eco</sub> , GPP	mid 2006-10	half-hourly/hourly	empirical model from EC data	1	Drewer et al., 2010	43475
	winter R <sub>eco</sub>	mid 2006-10	half-hourly/hourly	empirical modelling from night NEE EC data during Nov. -Apr.	1		5348
	soil temperature at -10 cm	mid 2006-10	half-hourly/hourly	automatic temperature sensors	1		35808
	soil temperature at -40 cm	mid 2006-10	half-hourly/hourly	automatic temperature sensors	1		35808
	LAI	2004	11 times	optical canopy analyser	2		11
Hor	NEE	2004-10, except 2007	half-hourly/hourly	EC	1	Hendriks et al., 2007	49611
	R <sub>eco</sub>	2003-06	biweekly	manual opaque chamber	6		53
	R <sub>eco</sub> , GPP	2004-10, except 07,09	half-hourly/hourly	empirical model from EC data	1	Reichstein et al., 2005, Papale et al., 2006	39420

	winter R <sub>eco</sub>	2004-10, except 07,09	half- hourly/hourly	empirical modelling from night NEE EC data during Nov. -Apr.	1		3966
	soil temperat ure at -8 cm	mid 2004- mid 2011	half- hourly/hourly	automatic temperature sensors	1		48881
	soil temperat ure at -11 cm	mid 2004- mid 2011	half- hourly/hourly	automatic temperature sensors	1		48881
	LAI	2006-07	4 times a year	optical canopy analyser, weighted mean from 7 vegetation types	3	Hendriks, 2009	8
	above ground biomass	2005-07	4 times a year	0.16m <sup>2</sup> clipped, dead leaves removed, weighted mean from 7 vegetation types	3	Hendriks, 2009	12
	Root biomass	2006-07	4 times a year	sieved soil cores of 1.15·10 <sup>-4</sup> m <sup>3</sup> , dead roots manually removed, weighted mean from 7 vegetation types	2	Hendriks, 2009	8
FsA and FsB	NEE	2007-2011	3-4 weekly several measurements per day	manual transparent chamber	3	Drösler, 2005; Beetz et al., 2013; Leiber- Sauheitl et al., 2013	1161
	R <sub>eco</sub>	2007-2011	3-4 weekly several measurements per day	manual opaque chamber	3	Drösler, 2005; Beetz et al., 2013; Leiber- Sauheitl et al., 2013	1161
	GPP	2007-2011	3-4 weekly several measurements per day	empirical model from chamber data	3	Drösler, 2005; Beetz et al., 2013; Leiber- Sauheitl et al., 2013	1161
	winter R <sub>eco</sub>	2007-2011	3-4 weekly several measurements per day	manual opaque chamber during Nov.-Apr.	3		357
	soil temperat ure at -2 cm	2007	half- hourly/hourly	automatic temperature sensors	1		36447
	soil temperat ure at -50 cm	2007	half- hourly/hourly	automatic temperature sensors	1		36447
	LAI	summer 2011- summer 2012	~3 weekly	optical canopy analyser	3		26
	Above ground biomass	2007-2011	4 weekly	0.04 m <sup>2</sup> , since 2011 0.16 m <sup>2</sup> , clipped and sorted into living and dead	3		43

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1 Table S3. List of main equations used in this study

Equation	No.	Definition
<b>Plant biotic processes</b>		
$C_{Atm \rightarrow a} = \varepsilon_L \cdot \eta \cdot f(T_l) \cdot f(T_{sum}) \cdot f(CN_l) \cdot f(E_{ta} / E_{tp}) \cdot R_{s,pl}$	(1)	Rate of photosynthesis (g C m <sup>-2</sup> day <sup>-1</sup> )
where $\varepsilon_L$ is the radiation use efficiency and $\eta$ is the conversion factor from biomass to carbon		
$f(T_l) = \begin{cases} 0 & T_l < p_{mn} \\ (T_l - p_{mn}) / (p_{o1} - p_{mn}) & p_{mn} \leq T_l \leq p_{o1} \\ 1 & p_{o1} < T_l < p_{o2} \\ 1 - (T_l - p_{o2}) / (p_{mx} - p_{o2}) & p_{o2} \leq T_l \leq p_{mx} \\ 0 & T_l > p_{mx} \end{cases}$	(2)	Response function for leaf temperature
where $p_{mn}$ , $p_{o1}$ , $p_{o2}$ and $p_{mx}$ are parameters.		
$f(CN_l) = p_{fixedN}$	(3)	Response function for fixed leaf C:N ratio
Where $p_{fixedN}$ is a parameter.		
$f(E_{ta} / E_{tp}) = \frac{E_{ta}}{E_{tp}}$	(4)	Response function for transpiration
$C_{a \rightarrow Leaf} = l_{c1} \cdot C_a$	(5)	Allocation of new assimilates to the leaves
where $l_{c1}$ , is a parameter.		
$C_{a \rightarrow Root} = (1 - l_{c1}) \cdot C_a$	(6)	Allocation of new assimilates to the roots
$C_{respleaf} = k_{mrespleaf} \cdot f(T) \cdot C_{leaf} + k_{gresp} \cdot C_{a \rightarrow Leaf}$	(7)	Plant growth and maintenance respiration from leaves (g C m <sup>-2</sup> day <sup>-1</sup> )
where $k_{mrespleaf}$ is the maintenance respiration coefficient for leaves, $k_{gresp}$ is the growth respiration coefficient, and $f(T_a)$ is the temperature. The equation calculates respiration from stem, roots, and grains by exchanging $k_{mrespleaf}$ to $k_{mrespstem}$ , $k_{mrespoot}$ , $k_{mrespgrain}$ , and using the corresponding storage pools. Respiration from the old carbon pools is estimated with the same maintenance respiration coefficients as for respiration from new carbon pools.		
$f(T) = t_{Q10}^{(T - t_{Q10bas})/10}$	(8)	Temperature response function for maintenance respiration (–)
where $t_{Q10}$ and $t_{Q10bas}$ are parameters.		
$C_{Leaf \rightarrow Stem} = l_{LS} \cdot C_{Leaf}$	(9)	Reallocation of C from leaf pool to stem pool – here used as pool for senescent leaves.
where $l_{LS}$ is a parameter		
$C_{Leaf \rightarrow LitterSurface} = f(T_{Sum}) \cdot f(A_l) \cdot s_{newleaf} \cdot C_{Leaf}$	(10)	Leaf C entering the surface litter pool
where $s_{newleaf}$ is a scaling factor. Stem C is calculated analogously with $s_{newstem}$ .		
$f(T_{Sum}) = l_{Lc1} + (l_{Lc2} - l_{Lc1}) \cdot \min\left(1, \frac{\max(0, T_{Sum} - t_{L1})}{\max(1, t_{L2} - t_{L1})}\right)$	(11)	leaf litter fall dependence of temperature sum
where $tL1$ , $tL2$ , $lLc1$ and $lLc2$ are parameters and $T_{Sum}$ is the so called “dorming” temperature sum, $TDormSum$ . $TDormSum$ is calculated at the end to the growing season when the air temperature is below the		



threshold temperature  $T_{DormTh}$ , as the accumulated difference between  $T_{DormTh}$  and  $T_a$ .  $T_{DormTh}$  is a parameter.

The stem litter rate is calculated analogously with the parameters  $tS1$ ,  $tS2$ ,  $lSc1$  and  $lSc2$ .

$$f(A_l) = e^{l_{LaiEnh} \cdot A_l} \quad (12) \quad \text{Litter fall dependency of LAI}$$

where  $l_{LaiEnh}$  is a parameter and  $A_l$  the leaf area index

$$C_{Root \rightarrow Litter} = f(l_{Rc}) \cdot C_{Root} \cdot S_{newroot} \quad (13) \quad \text{Root C entering the soil litter pool}$$

where  $S_{newroot}$  is a scaling factor. The root litter rate function,  $f(l_{Rc})$ , can be calculated with Eq. (11) by exchanging the parameters  $tL1$ ,  $tL2$ ,  $lLc1$  and  $lLc2$  to  $tR1$ ,  $tR2$ ,  $lRc1$  and  $lRc2$ .

$$C_{OldLeaf \rightarrow LitterSurface} = f(l_{Lc}) \cdot (C_{OldLeaf} - C_{RemainLeaf}) S_{oldleaf} \quad (14) \quad \text{Litter fall from roots, leaves and stems in the "old" biomass in perennial plants are calculated similarly to the "new" biomass but with the important exception that some of the old leaves may be retained}$$

where  $S_{oldleaf}$  is a scaling factor. The litter fall for stems and roots is calculated analogously.

$$C_{RemainLeaf} = C_{OldLeaf} \left(1 - \frac{1}{l_{life} - 1}\right) \quad (15) \quad \text{fraction of the whole } C_{OldLeaf} \text{ pool that will be excluded from the calculation of the litterfall from the old leaves}$$

where  $l_{life}$  is a parameter

$$C_{Leaf \rightarrow Harvest} = f_{leafharvest} \cdot C_{Leaf} \quad (16) \quad \text{amount of harvested carbon, removed from the system}$$

where  $f_{leafharvest}$  is a parameter. Harvest from the stem pool is calculated analogously by exchanging  $f_{leafharvest}$  with  $f_{stemharvest}$ . These parameters are also used to calculate the harvest fractions from the old stem and leaves perennials.

$$C_{Leaf \rightarrow LitterSurface} = f_{leaflittharv} \cdot (C_{Leaf} - C_{Leaf \rightarrow Harvest}) \quad (17) \quad \text{amount of plant parts, which are removed from the plant and enter the surface litter pool at harvest}$$

where  $f_{leaflittharv}$  is a parameter. Similar flows are calculated for stem and roots by exchanging  $f_{leaflittharv}$  to  $f_{stemlittharv}$

$$C_{Mobile} = (C_{Leaf \rightarrow LitterSurface} + C_{OldLeaf \rightarrow LitterSurface}) \cdot m_{retain} \quad (18) \quad \text{Allocation to the mobile C pool for developing new leaves during litter fall}$$

where  $m_{retain}$  is an allocation coefficient.

$$C_{Mobile \rightarrow Leaf} = C_{Mobile} \cdot m_{shoot} \quad (19) \quad \text{Allocation from the mobile C pool at leafing (between GSI 1 and 2) as an additional supply. This process goes on as long as there is carbon left in the mobile pool.}$$

where  $m_{shoot}$  is an allocation coefficient.

$$C_{Roots \rightarrow Leaf} = m_{Root} \cdot (C_{Roots} - C_{Leaf} \cdot r_{rl}) \quad (20) \quad \text{Allocation of C in the roots to leaves, taking place after a harvest event as long as root:leaf ratio is smaller than the value of the parameter } r_{rl} \text{ or until the plant goes to dormancy.}$$

where  $m_{Root}$  and  $r_{rl}$  are parameters

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### Plant abiotic processes

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$$R_{s,pl} = (1 - e^{-\frac{k_{rn} A_l}{f_{cc}}}) \cdot f_{cc} (1 - a_{pl}) R_{is} \quad (21) \quad \text{Plant interception of global radiation (MJ m}^{-2} \text{ day}^{-1})$$

where  $k_{rn}$  is the light use extinction coefficient given as a single parameter common for all plants,  $f_{cc}$  is the surface canopy cover, and  $a_{pl}$  is the plant albedo.

$$f_{cc} = p_{cmax} (1 - e^{-p_{ck} A_l}) \quad (22) \quad \text{Surface canopy cover (m}^2 \text{ m}^{-2})$$

Where  $p_{cmax}$  is a parameter that determines the maximum surface

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cover and  $p_{ck}$  is a parameter that governs the speed at which the maximum surface cover is reached.  $A_l$  is the leaf area index of the plant.

$$A_l = \frac{B_l}{p_{l,sp}} \quad (23) \quad \text{Leaf area index (m}^2 \text{ m}^{-2}\text{)}$$

Where  $p_{l,sp}$  is a parameter and  $B_l$  is the total mass of leaf.

$$L_v E_{tp} = \frac{\Delta R_n + \rho_a c_p \frac{(e_s - e_a)}{r_a}}{\Delta + \gamma \left(1 + \frac{r_s}{r_a}\right)} \quad (24) \quad \text{Potential transpiration (mm day}^{-1}\text{)}$$

where  $R_n$  is net radiation available for transpiration,  $e_s$  is the vapour pressure at saturation,  $e_a$  is the actual vapour pressure,  $\rho_a$  is air density,  $c_p$  is the specific heat of air at constant pressure,  $L_v$  is the latent heat of vaporisation,  $\Delta$  is the slope of saturated vapour pressure versus temperature curve,  $\gamma$  is the psychrometer 'constant',  $r_s$  is 'effective' surface resistance and  $r_a$  is the aerodynamic resistance.

$$r_s = \frac{1}{\max(A_l g_l, 0.001)} \quad (25) \quad \text{Stomatal resistance (s m}^{-1}\text{)}$$

where  $g_l$  is the leaf conductance.

$$g_l = \frac{R_{is}}{R_{is} + g_{ris}} \frac{g_{\max}}{1 + \frac{g_{\max}}{g_{vpd}} \frac{(e_s - e_a)}{g_{vpd}}} \quad (26) \quad \text{Stomatal conductance per leaf area (m s}^{-1}\text{)}$$

where  $g_{ris}$ ,  $g_{\max}$  and  $g_{vpd}$  are parameter values,  $g_{\maxwin}$  corresponds to  $g_{vpd}$  in winter.

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#### Soil carbon and nitrogen processes

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$$C_{DecompL} = k_l \cdot f(T) \cdot f(\theta) \cdot C_{Litter} \quad (27) \quad \text{Decomposition of the fast C pool (g C m}^{-2} \text{ day}^{-1}\text{)}$$

Where  $k_l$  is a parameter.

$$C_{DecompH} = k_h \cdot f(T) \cdot f(\theta) \cdot C_{Humus} \quad (28) \quad \text{Decomposition of the slow C pool (g C m}^{-2} \text{ day}^{-1}\text{)}$$

Where  $k_h$  is a parameter.

$$C_{LitterSurface \rightarrow LitterI} = l_l \cdot C_{LitterSurface} \quad (29) \quad \text{Litter from inactive surface litter pool, entering the fast SOC pool at a continuous rate.}$$

where  $l_l$  is a parameter.

$$f(T) = t_{Q10}^{(T - t_{Q10bas})/10} \quad (30) \quad \text{Response function for soil temperature (-)}$$

Where  $t_{Q10}$  and  $t_{Q10bas}$  are parameters.

Where  $t_{max}$  and  $t_{min}$  are parameters.

$$f(\theta) = \min \left( \begin{array}{l} \frac{p_{\theta satact}}{\left( \frac{\theta_s - \theta}{p_{\theta Upp}} \right)^{p_{\theta p}}} (1 - p_{\theta satact}) + p_{\theta satact}, \\ \frac{p_{\theta Low}}{\left( \frac{\theta - \theta_{wilt}}{p_{\theta Low}} \right)^{p_{\theta p}}} \end{array} \right) \quad \theta_{wilt} \leq \theta \leq \theta_s \quad (31) \quad \text{Response function for soil moisture (-)}$$

$$0 \quad \theta < \theta_{wilt}$$

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where  $p_{\theta_{Upp}}$ ,  $p_{\theta_{Low}}$ ,  $p_{\theta_{Satact}}$ , and  $p_{\theta_p}$  are parameters and the variables,  $\theta_s$ ,  $\theta_{wilt}$ , and  $\theta$ , are the soil moisture content at saturation, the soil moisture content at the wilting point, and the actual soil moisture content, respectively.

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Soil heat processes

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$$q_h(0) = k_{ho} \frac{(T_s - T_1)}{\Delta z / 2} + C_w (T_a - \Delta T_{Pa}) q_{in} + L_v q_{vo} \quad (32) \quad \text{Soil surface heat flow (J m}^{-2} \text{ day}^{-1}\text{)}$$

where  $k_{ho}$  is the conductivity of the organic material at the surface,  $T_s$  is the surface temperature,  $T_1$  is the temperature in the uppermost soil layer,  $\Delta T_{Pa}$  is a parameter that represents the temperature difference between the air and the precipitation,  $q_{in}$  is the water infiltration rate,  $q_{vo}$  is the water vapour flow, and  $L_v$  is the latent heat. The temperature difference,  $T_a - \Delta T_{Pa}$ , can optionally be exchanged to surface temperature,  $T_s$ .

$$k_{ho} = h_1 + h_2 \theta \quad (33) \quad \text{Heat conductivity of the organic material at the surface}$$

where  $h_1$  and  $h_2$  are empirical constants

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1 Table S4. Calibrated parameters

Symbol	Name	unit	Eq.	Definition	Min	Max
$g_{maxwin}$	CondMaxWinter	$m s^{-1}$	(26)	maximal conductance of fully open stomata	0.002	1
$g_{ph}$	GSI Post Harvest(1)	-		growth stage to which plant is set back after harvest	1.3	3
$k_{gresp}$	GrowthCoef(1)	$day^{-1}$	(7)	growth respiration coefficient	0.13	0.25
$k_l$	RateCoefLitter1	$a^{-1}$	(27)	rate coefficient for the decay of C in the fast pool		0.003
$k_{mresleaf}$	MCoefLeaf(1)	$day^{-1}$	(7)	maintenance respiration coefficient for leaves	0.015	0.035
$k_{mresroot}$	MCoefRoot(1)	$day^{-1}$	(7)	maintenance respiration coefficient for root		0.003
$k_{mresstem}$	MCoefStem(1)	$day^{-1}$	(7)	maintenance respiration coefficient for stem		0.013
$k_{rn}$	RntLAI	-	(21)	extinction coefficient in the Beer law used to calculate the partitioning of net radiation between canopy and soil surface	0.52	1
$l_{cl}$	Leaf c1(1)	$g C^{-1}$	(5)	allocation fraction to the leaves	0.52	0.55
$l_{ll}$	RateCoefSurf L1	$day^{-1}$	(29)	fraction of the above ground residues that enter the litter 1 pool of the uppermost soil layer	0.002	0.008
$l_{LaiEnh}$	LAI Enh Coef(1)	-	(12)	scaling factor for enhanced litter fall rates from leaf with higher LAI values	0.0016	0.6
$l_{Lc1}$	LeafRate1(1)	$day^{-1}$	(11)	rate coefficient for the litter fall from leaves before the first threshold temperature sum is reached		0.05
$l_{Lc2}$	LeafRate2(1)	$day^{-1}$	(11)	rate coefficient for the litter fall from leaves after the second threshold temperature sum is reached	0.1	0.3
$l_{LS}$	C Leaf to Stem(1)	-	(9)	scaling factor for reallocation of C from leaf to stem	0.015	0.025
$l_{Rc1}$	RootRate1(1)	$day^{-1}$	(13)	rate coefficient for the litter fall from roots before the first threshold temperature sum is reached		0.015
$l_{Rc2}$	RootRate2(1)	$day^{-1}$	(13)	rate coefficient for the litter fall from roots after the second threshold temperature sum is reached	0.01	0.05
$l_{Sc1}$	StemRate1(1)	$day^{-1}$	(11)	rate coefficient for the litter fall from leaves before the first threshold temperature sum is reached	0.003	0.1
$l_{Sc2}$	StemRate2(1)	$day^{-1}$	(11)	rate coefficient for the litter fall from leaves after the second threshold temperature sum is reached	0.03	0.2
$m_{retain}$	Mobile Allo Coef	-	(18)	coefficient for determining allocation to mobile internal storage pool	0.4 <sup>a</sup> , 0.05 <sup>bc</sup> ,	0.8 <sup>ab</sup> , 0.5 <sup>c</sup> , 0.45 <sup>d</sup>

					0.01 <sup>d</sup>	
$m_{Root}$	RateCoef_fRoot(1)	-	(20)	speed at which reallocation from roots to leaves after harvest take place	0.005	0.04
$m_{shoot}$	Shoot Coef	-	(19)	coefficient for determining allocation from the mobile pool to the leaf at leafing	0.05	0.15
$p_{ck}$	Area kExp(1)	-	(22)	speed at which the maximum surface cover is reached	0.5	1
$p_{L,sp}$	Specific LeafArea	g C m <sup>-2</sup>	(23)	the inverse of specific leaf area, i.e. leaf mass per unit leaf	44	49
$p_{mn}$	T LMin(1)	°C	(2)	minimum mean air temperature for photosynthesis	0.001	0.5
$p_{\theta}$	ThetaPowerCoef	vol %	(31)	coefficient in the soil moisture response function	0.65	4.5
$p_{\theta Satact}$	Saturation activity	vol %	(31)	saturation activity in soil moisture response function	0.001	0.252, 1 <sup>f</sup>
$p_{\theta Upp}$	ThetaUpperRange	vol %	(31)	water content interval in the soil moisture response function for microbial activity, mineralisation-immobilisation, nitrification and denitrification	20, 8 <sup>f</sup>	77
$r_{rl}$	Root Leaf Ratio(1)	-	(20)	threshold value for root:leaf ratio for reallocation of C from roots to leaves after harvest	5	6.5
$s_{newleaf}$	New Leaf(1)	-	(10)	scaling factor for litter fall of new leaf	0.15	0.25
$s_{newroot}$	New Roots(1)	-	(13)	scaling factor for litter fall of new roots	0.1	0.25
$s_{newstem}$	New Stem(1)	-	(10)	scaling factor for litter fall of new stem	0.1	0.15
$T_{amean}$	TempAirMean	°C		assumed value of mean air temperature for the lower boundary condition for heat conduction.	5.5 <sup>a</sup> , 10.5 <sup>b,d</sup> , 13 <sup>c</sup>	6.2 <sup>a</sup> , 15.5 <sup>b,c</sup> , 13 <sup>d</sup>
$T_{DormTh}$	Dormancy Tth	°C	(11)	threshold temperature for plant dormancy	0.1	2.5, 5 <sup>f</sup>
$T_{EmergeSum}$	TempSumStart	°C		air temperature sum that is the threshold for start of plant development	0.5	10
$T_{EmergeTh}$	TempSumCrit	°C		critical air temperature that must be exceeded for temperature sum calculation	0.15	1
$t_{L1}$	LeafTsum1(1)	day°C	(11)	threshold temperature sum for the lower leaf litter rate	10	20
$t_{L2}$	LeafTsum2(1)	day°C	(11)	threshold temperature sum for the higher leaf litter rate	20	50
$T_{MatureSum}$	Mature Tsum	°C		temperature sum beginning from grain filling stage for plant reaching maturity stage	80 <sup>a</sup> , 320 <sup>b</sup> , 750 <sup>c</sup> , 1050 <sup>d</sup>	115 <sup>a</sup> ,450 <sup>b</sup> , 850 <sup>c</sup> , 1350 <sup>d</sup>
$t_{Q10}$	TemQ10	-	(8), (30)	response to a 10 °C soil temperature change on the microbial activity, mineralisation-immobilisation, nitrification and denitrification and plant maintenance respiration	1.95	3.5

$t_{Q10bas}$	TemQ10Bas	°C	(8), (30)	base temperature for the microbial activity, mineralisation-immobilisation, nitrification and denitrification at which the response is 1	15	26
$t_{R1}$	RootTsum1(1)	day°C	(13)	threshold temperature sum for the lower root litter rate	10	20
$t_{R2}$	RootTsum2(1)	day°C	(13)	threshold temperature sum for the higher root litter rate	20	50
$t_{S1}$	StemTsum1(1)	day°C	(11)	threshold temperature sum for the lower stem litter rate	10	20
$t_{S2}$	StemTsum2(1)	day°C	(11)	threshold temperature sum for the higher stem litter rate	20	50
$\epsilon_L$	PhoRadEfficiency	$\frac{gDw}{MJ^{-1}}$	(1)	radiation use efficiency for photosynthesis at optimum temperature, moisture and C-N ratio	1.5 <sup>a</sup> , 2.3 <sup>b</sup> , 1.8 <sup>c</sup> , 2.5 <sup>d</sup>	2.6 <sup>ab</sup> , 3.2 <sup>cd</sup>

1 <sup>a</sup> at Lom

2 <sup>b</sup> at Amo

3 <sup>c</sup> at Hor

4 <sup>d</sup> at FsA and FsB

5 <sup>e</sup> Parameter uses opposite values to the linked parameter

6 <sup>f</sup> range tested in additional multiple runs

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1 Table S5. Most important parameters with constant values

Symbol	Name	unit	Eq.	Definition	Value
$\Delta T_{Pa}$	TempDiffPrec_Air	°C	(32)	difference between air temperature and infiltrating precipitation that will be considered for calculation in convective heat transport by precipitation to the soil	-2
$Z_{humus}$	OrganicLayerThick	m	(33)	thickness of the humus layer as used as a thermal property	3 <sup>abd</sup> , 2.5 <sup>c</sup>
$a_{pl}$	AlbedoLeaf	%	(21)	plant albedo	25
$f_{leafharvest}$	FHarvest Leaf	-	(16)	the fraction of leaves that is harvested	0.85
$f_{leaflittharv}$	FLitter Leaf	-	(17)	fraction of the remaining leaves after harvest that enters the fast SOC pool	0.1
$f_{stemharvest}$	FHarvest Stem	-	(16)	the fraction of stem that is harvested	0.85
$f_{stemlittharv}$	FLitter Stem	-	(17)	fraction of the remaining stem after harvest that enters the fast C pool	0.1
$g_{max}$	CondMax	$m^2 s^{-1}$	(26)	the maximal conductance of fully open stomata	0.02
$g_{ris}$	CondRis	$J m^{-2} day^{-1}$	(26)	the global radiation intensity that represents half-light saturation in the light response	
$g_{vpd}$	CondVPD	Pa	(26)	the vapour pressure deficit that corresponds to a 50 % reduction of stomata conductance	100
$h_1$	OrganicC1	-	(33)	empirical constant in the heat conductivity of the organic material at the surface	0.06
$h_2$	OrganicC2	-	(33)	empirical constant in the heat conductivity of the organic material at the surface	0.005
$k_h$	RateCoefHumus	$day^{-1}$	(28)	rate coefficient for the decay of C in the slow pool	
$l_{ife}$	Max Leaf Lifetime	a	(15)	maximum leaf lifetime	1
$p_{cmax}$	Max Cover	$m^2 m^{-2}$	(22)	maximum surface cover of plant	1
$p_{fixedN}$	FixedN	-	(3)	response for leaf C:N ratio	1
$p_{mx}$	PhoTempResMax	°C	(2)	maximum mean air temperature for photosynthesis	35
$p_{o1}$	PhoTempResOpt1	°C	(2)	lower limit mean air temperature for optimum photosynthesis	15
$p_{o2}$	PhoTempResOpt2	°C	(2)	upper limit mean air temperature for optimum photosynthesis	25
$p_{\theta Low}$	ThetaLowerRange	vol %	(31)	water content interval in the soil moisture response function for microbial activity, mineralisation–immobilisation, nitrification and denitrification.	13
$s_{oldleaf}$	Old Leaf(1)	-	(14)	scaling factor for litter fall of old leaf	1
$s_{oldroot}$	Old Roots(1)	-	(14)	scaling factor for litter fall of old roots	1
$s_{oldstem}$	Old Stem(1)	-	(14)	scaling factor for litter fall of old stem	1
$\eta$	Biomass to carbon	$mol C g^{-1} dw$	(1)	conversion factor from biomass to carbon	0.45

2 <sup>a</sup> at Lom

3 <sup>b</sup> at Amo

4 <sup>c</sup> at Hor

5 <sup>d</sup> at FsA and FsB

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1 Table S6. CoupModel switches - differences to default configuration

Modules	Options	Value
Abiotic driving variables	SoilDrainageInput	Simulated
Abiotic driving variables	SoilInfillInput	Simulated
Abiotic driving variables	SoilTempInput	Simulated
Abiotic driving variables	SoilWaterFlowInput	Simulated
Abiotic driving variables	SoilWaterInput	Simulated
Abiotic driving variables	WaterStressInput	Simulated
Drainage and deep percolation	DriveDrainLevel	Driving File
Drainage and deep percolation	PhysicalDrainEq	Linear Model
External N inputs	N Deposition	on
Gas processes	Methane Model	Detailed
Gas processes	Methane emission by plants	on
Gas processes	Methane oxidation by plants	on
Gas processes	Trace Gas Emissions	Direct Loss
Hidden	AboveTable	No
Hidden	TAirGlobRad	Used
Hidden	TimeResolution	Hourly
Hidden	TypeOfDrivingFile	Standard driving file
Interception	PrecInterception	on
Meteorological Data	CloudInput	Estimated(sunshine)
Meteorological Data	HumRelInput	Read from PG-file (first position)
Meteorological Data	PrecInput	Read from PG-file (first position)
Meteorological Data	TempAirInput	Read from PG-file (first position)
Meteorological Data	VapourAirInput	As relative humidity
Model Structure	Evaporation	Radiation input style
Model Structure	GroundWaterFlow	on
Model Structure	LateralInput	WaterShed approach
Model Structure	Nitrogen and Carbon	Dynamic interaction with abiotics
Model Structure	PlantType	Explicit big leafes
Model Structure	SnowPack	on
Model Structure	WaterEq	On with complete soil profile
Numerical	NitrogenCarbonStep	Independent
Plant	AlbedoVeg	Simulated
Plant	CanopyHeightInput	Simulated
Plant	LaiInput	Simulated
Plant	PlantDevelopment	Start=f(TempSum)
Plant	RootInput	Simulated
Plant Growth	Growth	Radiation use efficiency



Plant Growth	Harvest Day	PG File specified
Plant Growth	Litter fall dynamics	f(DormingTempSum)
Plant Growth	N ReAllocation	On
Plant Growth	N fixed Supply	on
Plant Growth	PlantRespiration	Growth and Maintenance
Plant Growth	ReAllocationToLeaf	On
Plant Growth	Winter regulation	On
Soil evaporation	Evaporation Method	Iterative Energy Balance
Soil evaporation	Surface Temperature	f(E-balance Solution)
Soil frost	FrostSwelling	Off
Soil heat flows	Convection flow	Not accounted for
Soil mineral N processes	Denitrification	Microbial based
Soil mineral N processes	Nitrification	Microbial based
Soil organic processes	Initial Soil Organic	Table

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1 Table S7. Criteria for accepted runs in the basic calibration (I a). Lower and upper limits are  
 2 separated by fore slash. In case of  $R^2$ , the upper limit corresponds to the highest value  
 3 achieved for this site. The criteria were selected to fit for around 75 runs and depend on the  
 4 different performances achieved for the different sites.

Site	Accepted runs	$R_{eco}$ ME	$R_{eco}R^2$	GPP ME	GPP $R^2$	LAI ME	LAI $R^2$	Winter $R_{eco}$ ME	Winter GPP ME	NEE $R^2$	Root biomass ME
Lom	74	-0.15/0.15	0.72/0.79	-0.15/0.15	0.65/0.70	-0.2/0.2		-0.25/0.25	-0.25/0.25		
Amo	64	-0.2/0.2	0.65/0.71	-0.2/0.2	0.65/0.68	-0.5/0.5		-0.4/0.4	-0.4/0.4		
Hor	74	-0.5/0.5		-0.5/0.5					-2/2	0.48/0.53	-150/150
FsA	68	-0.85/0.85	0.5/0.73	-0.85/0.85	0.32	-0.3/0.3	0.58/0.75	-3/3	-1/1		
FsB	67	-0.8/0.8	0.65/0.87	-0.8/0.8	0.35/0.40	-0.25/0.25		-2/2	-1/1		

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1 Table S8. Configurations of the selected single value representations C1-C7. Resulting values  
 2 for  $k_{IJ}$  and  $\varepsilon_L$  can be found in Figure 6.

Identifier	Description	$t_{Q10}$ [-]	$t_{Q10bas}$ [°C]	$p_{\theta Satact}$ [-]	$k_{mrespleaf}$ [day <sup>-1</sup> ]	C:N fast pool [-]	$p_{ck}$ [-]
C1_basic	selected basic common configuration	2.7	18.5	0.05	0.017	27.5	0.42 <sup>a</sup> , 0.2 <sup>b</sup> , 0.9 <sup>c</sup> , 1 <sup>d</sup>
C2_↑plant_resp	higher ratio of plant to soil respiration	2.7	18.5	0.05	0.022	27.5	0.42 <sup>a</sup> , 0.2 <sup>b</sup> , 0.9 <sup>c</sup> , 1 <sup>d</sup>
C3_↑ $p_{\theta Satact}$	higher saturation activity	2.7	18.5	0.40	0.017	27.5	0.42 <sup>a</sup> , 0.2 <sup>b</sup> , 0.9 <sup>c</sup> , 1 <sup>d</sup>
C4_↑temp_response	steeper temperature response function	4.0	12.0	0.05	0.008	27.5	0.42 <sup>a</sup> , 0.2 <sup>b</sup> , 0.9 <sup>c</sup> , 1 <sup>d</sup>
C5_C3&C4	higher saturation activity and steeper temperature response	4.0	12.0	0.40	0.008	27.5	0.42 <sup>a</sup> , 0.2 <sup>b</sup> , 0.9 <sup>c</sup> , 1 <sup>d</sup>
C6_C:N_60	C:N of 60 for the fast decomposition pool	2.7	18.5	0.05	0.017	60	0.42 <sup>a</sup> , 0.2 <sup>b</sup> , 0.9 <sup>c</sup> , 1 <sup>d</sup>
C7_common_ $p_{ck}$	same $p_{ck}$ value for all sites	2.7	18.5	0.05	0.017	27.5	1

3 <sup>a</sup> at Lom

4 <sup>b</sup> at Amo

5 <sup>c</sup> at Hor

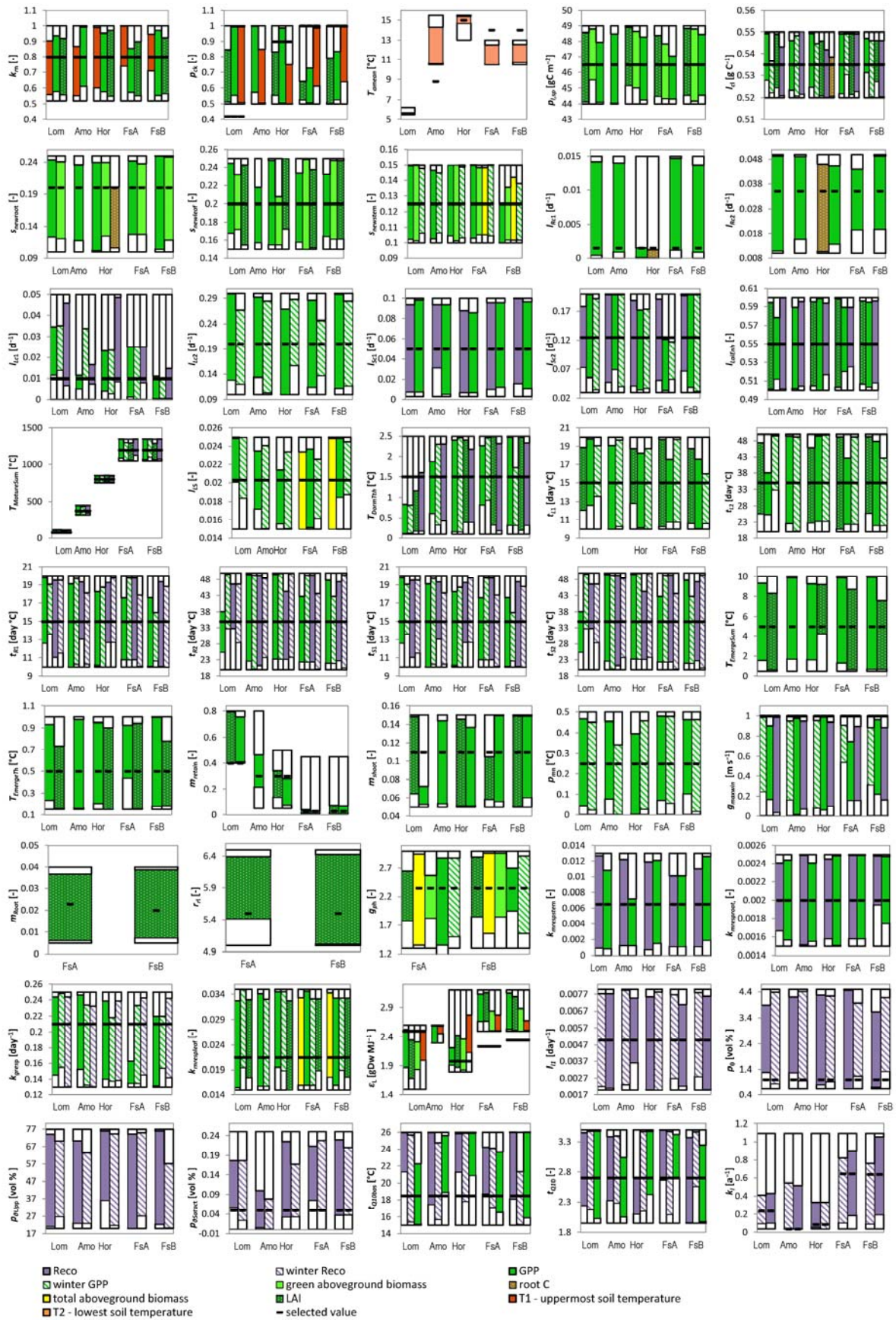
6 <sup>d</sup> at FsA and FsB

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1 Table S9. Variables and related parameter as used for further parameter constraint in step I c  
 2 and III

Variable	Site	Parameter
R <sub>eco</sub>	Lom, Amo, Hor, FsA, FsB	$l_{cl}, l_{Sc1}, l_{Sc2}, l_{Lc1}, l_{Lc2}, l_{LaiEnh}, T_{MatureSum}, T_{DormTh}, t_{R1}, t_{R2}, t_{S1}, t_{S2}, g_{maxwin}, k_{mrespstem}, k_{mresproots}, p_{\theta Satact}, p_{\theta Upp}, l_{l1}, p_{\theta}, k_l, T_{EmergeSum}, t_{Q10}, t_{Q10bas}$
GPP	Lom, Amo, Hor, FsA, FsB	$k_{rn}, p_{ck}, \epsilon_L, p_{l,sp}, l_{cl}, S_{newroot}, S_{newleaf}, S_{newstem}, l_{Rc1}, l_{Rc2}, l_{Sc1}, l_{Sc2}, l_{Lc1}, l_{Lc2}, l_{LaiEnh}, T_{MatureSum}, l_{LS}, T_{DormTh}, t_{L1}, t_{L2}, t_{R1}, t_{R2}, t_{S1}, t_{S2}, m_{shoots}, m_{retain}, T_{EmergeTh}, T_{EmergeSum}, p_{mn}, g_{maxwin}, g_{ph}, k_{mrespstem}, k_{mresproots}, k_{gresp}, k_{mrespleaf}, t_{Q10}, t_{Q10bas}$
winter R <sub>eco</sub>	Lom, Amo, Hor, FsA, FsB	$t_{R1}, t_{R2}, t_{S1}, t_{S2}, k_{gresp}, p_{\theta Satact}, p_{\theta Upp}, l_{l1}, p_{\theta}, k_l, T_{EmergeSum}, t_{Q10}, t_{Q10bas}$
winter GPP	Lom, Amo, Hor, FsA, FsB	$l_{cl}, S_{newstem}, l_{Sc2}, l_{Lc1}, T_{MatureSum}, l_{LS}, T_{DormTh}, t_{L1}, t_{L2}, t_{R1}, t_{R2}, t_{S1}, t_{S2}, p_{mn}, g_{maxwin}, g_{ph}, k_{gresp}, k_{mrespleaf}$
upper most soil temperature	Lom, Amo, Hor, FsA, FsB	$k_{rn}, p_{ck}, \epsilon_L$
lowest soil temperature	Lom, Amo, Hor, FsA, FsB	$T_{amean}$
LAI	Lom, Hor, FsA, FsB	$k_{rn}, p_{ck}, \epsilon_L, p_{l,sp}, l_{cl}, S_{newleaf}, l_{LaiEnh}, T_{MatureSum}, T_{DormTh}, t_{L1}, t_{L2}, m_{shoots}, m_{retain}, T_{EmergeTh}, T_{EmergeSum}, m_{Roots}, k_{mrespleaf}, r_{rl}, g_{ph}$
snow depth	Lom	
green above ground biomass	Hor, FsA, FsB	$\epsilon_L, p_{l,sp}, S_{newroot}, S_{newleaf}, S_{newstem}, g_{ph}$
total above ground biomass	Hor, FsA, FsB	$S_{newstem}, l_{LS}, g_{ph}, k_{mrespleaf}$
root biomass	Hor	$l_{cl}, S_{newroot}, l_{Rc1}, l_{Rc2}$

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1 Figure S1. Tested parameters and ranges of the basic calibration and for configuration C1 selected values. Each  
2 solid bar show the range of the 10 out of 350'000 runs with the best performance index for a validation variable  
3 (x-axis). Only those bars were shown where either a covariance between the performance on this variable and  
4 the parameter were detected or expected due to model equations. Tested ranges are indicated by the grey frame  
5 around the bar.