Author response to comment on "An inversion approach for determining production depth and temperature sensitivity of soil respiration" by R. N. C. Latimer and D. A. Risk

Editor **Authors** 

Thank you very much for your careful replies to the reviews. I enjoyed reading them and I'm sure the reviewers did so, too. I agree with many of your responses....

Thank you kindly. Under the assumption that our suggested textual edits were warranted, we have embedded these changes revised manuscript, along with several other changes that were requested specifically, as described below.

[I] concentrate here only on the **one remaining critical aspect**: the relation of your study to the real world. I'm very happy that Reviewer 1 has raised this (comment on P10140L24). It made me looking at this study in a different manner.

To begin with, I was wondering, why you discuss using your model with real world data in the methods and not the discussion section. I suggest making this a part of the discussion (action 1).

The section called "Incorporating external data" could have been worded better, as it was meant to describe how our synthetic datasets were created, and integrated into the inversion process. We ran the process exactly as we would for field data. We have totally reworded this section, but left it in the same location because the content is methodological in nature, which will now be more obvious. It now reads as:

In this study, we incorporated external data in the same way we would with field studies. We started with real measurements of temperature through depth, and soil volumetric water content, from a local field site. One of the largest challenges in preparing data for inversion is to accurately model soil temperature through depth and time, as temperature is the known determinant of soil lags \citep{phillips}. For each set of temperature measurements through depth, a linear regression (in R) was performed, resulting in a 5th order polynomial for temperature through depth every 1800 s. A linear interpolation through time was performed to obtain temperature values in each layer for every modelled time step. The resultant temperature values replaced our originally sinusoidally varying temperature function in the model. The value of thermal diffusivity was therefore implicitly built into these measurements and is no longer required as a direct model input.

These physical variables were used in a forward instance of the soil model to create  $CO_{2}$  surface flux and  $CO_{2}$  concentration timeseries. Datasets were created using many e-folding depths of production, and  $Q_{2}$  concentration timeseries, so that we had many idealized datasets on hand in which concentration, fluxes and associated temperatures, e-folding depths of production, and  $Q_{2}$  were known. Soil volumetric water content was not formally incorporated as a driver of respiration in these synthetic datasets, so all simulations were performed over periods of constant soil volumetric water content. During inversion we pretended not to know e-folding depths of production, and  $Q_{2}$  of these synthetic datasets, and hoped the inversion process would return the known values. Since the same forward soil model that generated the synthetic datasets was also embedded within the inversion scheme, errors in e-folding depths of production, or  $Q_{2}$  would be due entirely to the inversion process itself.

In general I agree and have not at all any problem with this work being a theoretical study. But inspired by your discussion with reviewer 1 I feel a bit confused about the objectives. There you write "This study seeks to develop a reliable inversion framework for determining the O10 and Zp of different sites given continuous soil measurements." (10140/21). This is clearly related to application with real world data. Consequently, when reading the manuscript the first time, I assumed that the main result from this study for practitioners was, to learn with which additional measurements they could constrain the process's temperature sensitivity estimates better than with surface fluxes only. However, if this model is far from being applicable to real cases (correct me if this is exaggerated), the study is not of good help. If not with inversion, how can practitioners then use their additional soil CO2 concentration data to constrain their empirical temperature sensitivity estimates? Or more precisely: how can they otherwise reliably estimate Zp? If I'm correct, the practical relevance of the study is much weaker (unless you don't know Zp, your Q10 values are biased and this study tells you why, but cannot help you to reduce the bias) and this needs to be clearly understandable expressed in the conclusions (action 2). For example you write that "Depending on the tolerable level of error for a given application, almost every tested combination resulted in reasonably accurate returned Q10 and Zp values."(10154/6). This is correct and sounds good, but you need to make sure that everybody understands that this is only true for the appropriately constrained theoretical case – but most likely not at all for realistic field data! Investing in a CO2 concentration profile measurement will then most probably not pay back. This is an important conclusion, but unfortunately speculative as you didn't test it. Consequently you need to conclude from the discussion on why your model will probably fail in real field cases, to make this a clear consequence from your error analysis (still action 2).

Unfortunately, this is a misunderstanding that has been propagated from the initial review, and which we attempted to clear up in our initial response. It may have helped if we could have uploaded a revised manuscript, where the entire text could be taken together, as it might have made things clearer. But, to clarify once and for all:

The inversion process presented here IS useful in the real world. We do NOT need to know the depth of production a priori, as the reviewer and editor have suggested. This suggestion stems from a simple misunderstanding. Our inversion does in fact determine both the e-fold depth of production ( $Z_p$ ), and temperature sensitivity ( $Q_{10}$ ). These are <u>unknown</u> prior to inversion. But, like for any mathematical model, the <u>shape</u> of these functions must be assumed, or known. For example, it would be clear to any soil researcher that the shape of the  $Q_{10}$  function is different than the numerical value of  $Q_{10}$ , which is simply a solvable numeric parameter within the  $Q_{10}$  equation. In the same way, a production profile equation describes production through depth, and the e-fold parameter (called  $Z_p$  in this manuscript) is needed to solve for production at each depth (but first e-fold is determined by inversion). We believe that the review and editor are generally confusing our need to assume the shape of the production-depth distribution (an equation), with a priori knowledge of production at each depth (a numeric value). These are quite different things, of course.

Our use of e-fold value (or damping depth as it is also sometime called) to describe an exponentially distributed soil  $CO_2$  production profile is a common approach in soil modeling, and goes back over 20 years to at least Suarez and Simunek (1993). It is probably more common than the uniform profile approach, though both are used, and modelers defer to whichever is more suitable for the study in question. To provide some examples of past use in our studies, we have used exponential production profiles (and e-fold parameterization) in modeling studies including Bowling et al. (2015, in Biogeosciences), and Phillips et al. (2010). We have also used exponential production profiles with e-fold parameterization in forward modeling of  $CO_2$  concentrations in

Phillips et al. (2013), and  $\delta^{13}CO_2$  (Nickerson et al. 2014, Nickerson and Risk 2013, Nickerson and Risk 2009). In some other studies we have used instances of uniform production profiles where generic non-specific soils were being simulated, for both  $\delta^{13}CO_2$  (Egan et al. 2014), and  $CO_2$  concentrations (Creelman et al. 2013). However, we would normally pick an exponential representation of production through depth, because the Northern temperate to northern soils with which we work would almost always show exponential production, since waterlogged soils at depth produce  $CO_2$  at a very low rate relative to the surface. Researchers in other parts of the world might want to characterize the production profile differently, and if they have absolutely no idea of the expected pattern, a point-in-time gradient measurement would help establish the pattern. Like any model, there will always be some site-specific modifications required. We have described the need to understand the generalized shape of the production profile (uniform, linear, exponential through depth). Needing to know the generalized shape is, however, far different than knowing the precise e-fold depth value, or the production in each layer ( $P_{(i)}$ ). We solve for the latter.

We have wondered about the root of the misunderstanding, and we recognize several areas.

We first considered whether the inversion text is misleading. But, in the very first sentence of the inversion section, it is clearly stated what parameters are being varied (and we certainly wouldn't iterate over them if they were known):

"The model is run for  $Q_{10}$  values ranging from 1 to 5.5 in steps of 0.1, and  $Z_p$  from 0.02 m to 0.3 m 200 in steps of 0.01 m."

So, that seems generally clear, though we suggest an improvement (which appears below as part of several bullets).

We also conserved whether the definition of Zp was not clearly defined in the methods section, as a parameter within an exponential distribution.

"...Zp is the depth of production (m), defined as the depth below which the total fraction of CO<sub>2</sub> production remaining is 1/e (also called the e-folding depth)." (a related equation is also shown, plus a reference is provided to an earlier manuscript)

It seems generally clear but could perhaps be improved too (see bullets below).

We lastly wondered whether the reviewer and editor might be confused in the results and discussion, where we talk at length about e-fold  $(Z_p)$  solving, and error across the simulations. Though Zp is perhaps not familiar to many readers, it is well defined. But, routinely in the results and discussion we do use the term:

"depth of production"

when we refer to e-fold depth. This usage was defined in the methods section, and was meant to sit as a shortened and more familiar version of the e-fold parameter. But, this terminology might still generate some confusion, as we're not referring to an actual depth of production, but rather a parameter in an exponential equation that can be used to solve for production at each depth, or  $P_{(i)}$ . So, we have changed the methods, results and discussion to simply read e-fold depth.

In summary, we believe that the best way to clear up any misunderstanding is as follows:

- 1. <u>Re-name "depth of production" as "e-fold depth of production" for accuracy and consistency with past papers</u>. We will maintain this usage through the results/discussion. This makes the results and discussion sound more technical, but the accuracy is better.
- 2. State clearly in the first sentence of the inversion methods that  $Q_{10}$  and  $Z_p$  are unknowns: "The model is run <u>for two unknowns</u>, including  $Q_{10}$  values ranging from 1 to 5.5 in steps of 0.1, and  $Z_p$  from 0.02 m to 0.3 m 200 in steps of 0.01 m."
- 3. Clarify that any  $P_{(i)}$  can be solved using the e-fold depth, as follows: " $\mathbb{Z}_p$  is... the depth below which the total fraction of  $CO_2$  production remaining is 1/e, from which the production at any depth P(i) can be calculated based on equation 4.
- 4. We removed this text from the end of the discussion, which was very misleading and would have obviously left a different flavor than reality: Some of the soil parameters across which we tested are obviously unknown a priori. The unknown value of  $Q_{\underline{10}}$  has already been noted, and depth of  $CO_2$  production may also be unknown prior to inversion.

We also noted a significant error in equation 4, which was not previously identified by us, or the previous reviewers. " $Z_p$ " was incorrectly labeled " $d_p$ ", which could have been figured out – but may have misled. Having fixed this, the relationship of  $Z_p$  and  $P_{(i)}$  should now be much clearer!

Lastly, a probable source of uncertainty was present in the last paragraph of the discussion section, which suggested that to better constrain the distribution of production through the soil profile (if it were not assumed exponential) one could consider looking to root depth. Unfortunately, that text was poorly constructed, and suggested that the depth of production was not known. We meant only the form of the equation. So, we have reworked this section, and included it within a "Limitations and opportunities" section, in combination with another 2 paragraphs on the topic which deal with constraining data. This was unfortunate, and conflicted with the math, and all previous definitions – but would have left a strong (and incorrect) flavor at the end of the paper. We apologize.

With this regard using random errors (P10147/06) is not sufficient. The treatment of errors is of course a valuable step towards modelling real world data, but in real world, measured field data tend to have systematic errors (bias in installation, wrong calibration). This, together with soil inhomogeneity at the sensor position is probably the reason, why the model inversion approach will finally fail in real world. Please include the systematic errors in your analysis in addition to the random errors (action 3).

We did not make any changes in this section, because the 10% maximal error we used should generally be in excess of systematic + random errors and is a worst case value. Plus, there would be many possible combinations of systematic + random errors depending on 1) sensors used, 2) e-fold depth and "sharpness" of the difference between surface and depth production, and other factors such as quality of depth measurement during installation. In a sensitivity test like this manuscript, we iterate across all parameters in combination, so when considering the wide variety of available sensors and chambers, there seems a very large number of additional factors that we could include. Given that the study already took between 2 and 3 CPU-years to cover all our error experiments, it seems a very large expansion of the parameter space. Each additional factor would expand the study by a multiple of the factor. So, if we included 10 levels of systematic bias, it would increase the CPU time for our study by a factor of 10. Also, we recently published a random error study on flux measurements (Lavoie et al 2015) and would add that one additionally has to random ecosystem "error", because respiration is not actually always the same every time the ecosystem crosses the same value of T. Our aim was more so to quantify methodological error

associated with the inversion and sensor placement. The error across error types would have been one direction. Another possible direction would have been to investigate alternate forms of the model solving, such as doing depth-specific  $Q_{10}$  solving when there were multiple sensors constraining the production profile and e-fold depth (and where we would not have to solve for it). These are all meritorious directions for research. The error question is an important one, however, and we would suggest that as normal Due Diligence, authors of subsequent studies in which the inversion technique is should be responsible for quantifying the errors specific to their deployment. These are much easier to determine, and authors bear responsibility for communicating error. Unfortunately, it is extremely rare to see even the most basic error analysis, such as a quantified flux error in an autochamber system. Things are changing slowly, but in general most studies have very little discussion of error. What is clear from our inversion error analysis, however, is that the inversion technique leads to far less error than normal regression techniques (see Phillips et al 2011) because it takes gas and thermal diffusion lags into account. We would hope that, in light of these comments, the editor might provide some flexibility on this point.

Per Erik's first remark is another argument that you only partly tackle in the discussion, why an inversion approach in the real world is likely to fail, simply because the Q10 value can vary layer specific in your analysis you take it as a global parameter ("Q10 is the temperature sensitivity of soil respiration" 10142/14). Please review the literature on changes of Q10 with aging of soil organic matter and even with the average temperature level (because it is not the right function) and include in the discussion, what this means for the prospects of deriving accurate Q10 values from in situ field measurements (action 4).

We agree that this is a good topic for discussion, and have added the following text into our discussion, and integrated it with a misleading section that suggested that we do not have adequate constraining information on depth of production, which was not strictly true (we were referring to distribution of production). The entire section of modified text now reads as:

There are both limitations and future opportunities for the inversion approach. In general, the better an inversion is constrained with data, the better it will do in returning the true value for parameters of interest. Some of the soil parameters are distributed in ways that must be assumed. For example, the distribution of CO\$\_2\$ production may be unknown. While most studies in the history of soil modelling have assumed an exponential distribution (and it has been seen in many studies using the gradient technique), some other considerations might help determine whether additional parameterization measurements are needed. For example, knowledge of rooting depth could be one aid. On average, root respiration accounts for 50\% of soil respiration \citep{hanson} and \cite{jackson} provides root distributions for different terrestrial biomes. \cite{jackson} found that tundra, boreal forest and temperate grasslands had upwards of 80-90\% of roots within the top 30 cm of soil whereas deserts and temperate coniferous forests had much deeper rooting profiles, with only 50\% of roots within the top 30 cm. These and other methods may be helpful in providing constraint data when running inversions on real timeseries.

A future opportunity for inversion studies is to determine depth-specific  $Q_{10}$ , which would be of interest to many researchers. Currently there are few field examples where researchers have determined in-situ  $Q_{10}$  as a function of depth, but two examples of such data using include gradient studies include \cite{riskdiochon,tang}. Incubations might seem useful in this regard, but are disputed as a representation of in-situ conditions, especially at depth (Risk et al. 2008). Ideally, an

inversion approach could determine depth-specific  $Q_{10}$ , but the reality is challenging. If an additional 100  $Q_{10}$  values were included as unknowns (one for each layer), it would increase computational demand by 100 times. The inversion results would also be confusing, and extreme values at one depth could potentially cause a spurious match to the measured data. The number of non-unique and implausible solutions would rise significantly as a result. A more reasonable approach might be to define  $Q_{10}$  as we do e-fold, which is as a function of soil depth. This would be computationally compact but whether a function would be realistic is not well known because there are so few examples of  $Q_{10}$  depth profiles against which we could evaluate this approach. The best approach would be to use many profile concentration sensors for constraining data, so that e-fold depth of production could be known, and the inversion could focus instead solely on determining layer-specific  $_{10}$ .

Despite the relatively nascent stage of our soil CO\$\_{2}\$ inversion approach, indications are that it has better theoretical validity than traditional regression approaches, which do not take thermal- and gas-transport lags into account. Our error results here compare very favourably against error analyses generated from detailed examination of regression approaches across thermal- and gas-transport parameter space (Zhang et al. 2015, Phillips et al. 2011, Graf et al. 2008, and others).

As noted above, the inversion approach is not likely to "fail". We were motivated to develop the inversion approach because it is more theoretically valid than regression approaches since it is rooted in thermal and thermal- and gas-transport physics. So, one can argue that it is less likely to fail than the normal regression technique which is plagued with issues. Inversion may however not yet be at the level of maturity where it could determine depth-specific  $Q_{10}$ , but if a suitable dataset presented itself where we could eliminate the need to invert for e-folding depth, we could easily invert for depth-specific  $Q_{10}$ . We have noted this in the text above – that the right datasets would make it possible. Such is the nature of inversion – that the approach depends on what constraining data are available. The better the constraints, the farther the model can be pushed to examine specific parameters in great detail.

In addition to this discussion I have three other comments that I like you to consider in your revision:

1. Figure 1. In the text I immediately understood why there are time lags, but I was and I still am lost with the logic of the figure. Isn't the temperature sensitive gas production missing (link between heat transfer and gas diffusion)? Can you explain what the arrows under 'Time' mean? To shorten this, please consider removing this figure if it has only illustrative character (action 5).

Agreed. We have replaced the word "time" with " $CO_2$ ", reflecting  $CO_2$  production. This helps to represent the temperature sensitive gas production. Presumably the time component is obvious. What is less obvious to many readers is the impact of thermal diffusion, which is one reason to keep the figure. The most important lags are actually of the thermal variety, and not the gas diffusion variety (see Phillips et al 2011).

2. Please do not use colloquial language in the revised version. Avoid, e.g., 'sits in ... as' (action 6)

Thank you. Fixed.

3. 10154/5 Conclusion: why "preliminary"? If the study is preliminary shouldn't we wait until it is finished? Please consider revision. (action 6)

Thank you. Fixed.

I assume that the manuscript will still considerably change. Therefore, we will need it's final version to evaluate it.

Just to be clear, we have also made the revisions we had suggested in the last round of review. They were in general smaller than those recommended here. Also, you had agreed with them and we assume that they were on the mark. Those changes are listed exhaustively in our last communication, and are also shown in our markup.

Overall, we have made considerable changes to the manuscript, and it is more straightforward and cohesive. Thanks kindly for your comments, and consideration of this manuscript.

References used in this response (those appearing as italic and underlined have been added to the manuscript text):

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# An inversion approach for determining distribution of production and temperature sensitivity of soil respiration

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Abstract. Physical soil properties create lags between temperature change and corresponding soil responses, which obscure true  $Q_{10}$  values and other biophysical parameters such as depth of production. This study examines an inversion approach for estimating  $Q_{10}$  and depth of production (Zp) using physically based soil models, constrained by observed high-frequency surface fluxes and/or concentrations. Our inversion strategy uses a 1-D multi-layered soil model that simulates realistic temperature and gas diffusion. We tested inversion scenarios on synthetic data using a range of constraining parameters, time averaging techniques, mechanisms to improve computational efficiency, and various methods of incorporating real data into the model. Overall, we have found that with carefully constrained data, inversion was possible. While inversions using exclusively surface flux measurements could succeed, constraining the inversion using multiple shallow subsurface  $CO_2$  measurements proved to be most successful. Inversions constrained by these shallow measurements returned  $Q_{10}$  and Zp values with average errors of 1.85% and 0.16% respectively. This work is a first step toward building a reliable framework for removing physical effects from high frequency soil  $CO_2$  data. Ultimately, we hope that this process will lead to better estimates of biophysical soil parameters and their variability on short timescales.

#### 1 Introduction

Soil respiration, which includes both root and microbial respiration, represents the largest outward flux of  $CO_2$  from terrestrial ecosystems, with a magnitude far above that of anthropogenic emissions (Raich and Schlesinger, 1992). Small changes in the soil  $CO_2$  flux could therefore have a significant impact on the carbon balance and global atmospheric  $CO_2$  concentrations. In predictions of atmospheric  $CO_2$  over the  $21^{st}$  century, uncertainties surrounding the response of land flux to

climate change are second only to uncertainties surrounding future anthropogenic emissions (Meir et al., 2006). In order to accurately predict future atmospheric CO<sub>2</sub> concentrations, it is crucial to gain a better understanding of how land systems will respond to changing temperature and moisture regimes.

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Soil CO<sub>2</sub> production originates from plant root respiration and microbial decomposition of organic matter. The temperature sensitivity of soil respiration describes how the flux of CO2 from soils will respond to a change in temperature. Normally soil microbial and plant root processes are treated together because they are not readily distinguished from one another. Temperature sensitivity is often quantified by a parameter Q<sub>10</sub>, which describes the factor increase in soil respiration with a temperature increase of  $10^{\circ}\text{C}$ . This  $Q_{10}$  parameter is used in global climate models to quantify soil feedbacks to climate change. It has been found that  $Q_{10}$  values are influenced by a range of environmental factors including soil temperature (Lloyd and Taylor, 1994; Luo et al., 2001), soil volumetric water content (Davidson et al., 1998; Reichstein et al., 2002) and soil organic matter content (Taylor et al., 1989; Wan and Luo, 2003). As these factors exhibit high spatial heterogeneity across ecosystems as well as within a given ecosystem, it has long been expected that  $Q_{10}$  will also exhibit high spatial variability. Despite this, most existing models continue to use a globally constant Q<sub>10</sub> value. This may reduce or enhance predicted release of CO<sub>2</sub> from soils, leading to large over- or under- estimates of the contribution of soil respiration to terrestrial CO2 flux in the face of climate change. There has been considerable debate over the usage and magnitude of  $Q_{10}$  (Davidson et al., 2006; Mahecha et al., 2010), with different studies producing widely variant values. While most studies agree that CO2 flux feedback will be positive, there is no consensus on how best to estimate the magnitude of  $Q_{10}$ .

Historically,  $Q_{10}$  values have been determined through regression analysis of soil temperature and  $CO_2$  surface flux measurements. A known source of error in this approach originates in the physics of soil heat and gas transport, which might separate a change in surface soil temperature (normally a 5 cm or 10 cm temperature is used for deriving  $Q_{10}$ ) from the resultant change in  $CO_2$  flux measured at the surface. The lags depend most heavily on soil heat transport (Phillips et al., 2011), because changes in surface temperature are shifted and dampened significantly as a function of depth, with each successive soil layer experiencing a reduced temperature change in amplitude. Gas diffusion also plays an important role, and even if soil microbes and roots produced  $CO_2$  instantaneously upon receipt of thermal energy at the characteristic production depths, gases still take time to diffuse upward. Soil properties including heat and gas diffusion, and the production depth (Zp), all contribute to these lags (Fig. 1). Phillips et al. (2011) demonstrated that such lags can lead to severe misinterpretation of data when attempting to extract true  $Q_{10}$  values through regression of surface flux and a temperature measurement at a single depth.

These thermal and gas diffusion processes, and the resulting lags, can be captured in a simple 1-D physical heat and gas transport soil model (Nickerson and Risk, 2009; Phillips et al., 2011).

Though not done to date for the soil respiration system, it is possible to use such a model in inverse fashion for estimating the value of parameters like  $Q_{10}$  and Zp by looping the forward model iteratively through possible parameter combinations, with observed measurements as a constraint. Normally, an objective function is used for helping decide which parameter set best minimizes the difference between modelled and measured data. This method has been identified as a promising tool for determining unknown soil parameters (Zhou et al., 2009), with an increasing availability of high frequency data sets allowing for rigorous constraints on known model parameters.

This study seeks to develop a reliable inversion framework for determining the  $Q_{10}$  and Zp of different sites given continuous soil measurements. It also seeks to provide guidance for researchers who would like to build field observational sites suited for inversion analysis. Working exclusively with synthetic soil data that mimics the form of collected field data and of which all parameters are known, we first undertake sensitivity tests to determine optimal sensor placing in the field, and decide whether soil  $CO_2$  surface flux, and/or profile measurements, are more suited for anchoring inversion approaches with the necessary field data for parameter constraint. Using the best sensor combination, we are able to evaluate the accuracy of the inversion approach in returning the original  $Q_{10}$ , and Zp, across many realistic soil type scenarios.

## 75 2 Methods

This study uses a one dimensional CO<sub>2</sub> and heat transport model described by Phillips et al. (2011), originally developed by Nickerson and Risk (2009). This model, with existing versions in Perl and R (R Core Team, 2015), was recoded in C to increase computational efficiency for the parameter solving routine.

#### 30 2.1 Model description

This model (Fig. 2) simulates the movement and production of  $CO_2$  through the soil profile and into the free atmosphere. The model consists of one atmospheric layer and a soil profile 1 m in length, divided into 100 layers of uniform thickness. Each layer can exchange  $CO_2$  with its two nearest neighbouring layers using the 1-D discrete form of Fick's first law:

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$$F_{ij} = -D_{ij} \frac{\Delta C_{ij}}{\Delta z_{ij}} \tag{1}$$

where  $D_{ij}$  is the effective diffusion coefficient between two soil layers,  $\Delta C_{ij}$  is the CO<sub>2</sub> concentration difference ( $\mu$ mol m<sup>-3</sup>) and  $\Delta z_{ij}$  is the difference in depth (m) between the two layers.

For every modelled time step, each soil layer has a defined temperature, biological  $CO_2$  production,  $CO_2$  flux, thermal diffusivity and gas diffusivity. Temperature varies sinusoidally on daily and annual timescales. Changes in surface temperature are shifted and dampened through the soil profile

using:

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$$T[i] = T_{avg} + \Delta T_D e^{\frac{-z_i}{d_{Td}}} sin\left(\omega_D t - \frac{-z_i}{d_{Td}}\right) + \Delta T_Y e^{\frac{-z_i}{d_{Ty}}} sin\left(\omega_Y t - \frac{-z_i}{d_{Ty}}\right)$$
(2)

$$d_{Td} = \sqrt{\frac{2D_T[i]}{\omega_D}}, d_{Ty} = \sqrt{\frac{2D_T[i]}{\omega_Y}}$$
(3)

which simulates the lags related to the rates of thermal diffusion. In this equation,  $T_{avg}$  is the average temperature in the air and soil profile for the duration of the simulation,  $\Delta T_D$  is the amplitude of the daily temperature fluctuation,  $\Delta T_Y$  is the amplitude of the yearly temperature fluctuation,  $\omega_D$  is the radial frequency for daily oscillations ( $\omega_D$ =2 $\pi$ /86400s),  $\omega_Y$  is the radial frequency for annual oscillations,  $z_i$  is the layer depth (m), and  $D_T$  is the thermal diffusivity of the soil (m<sup>2</sup> s<sup>-1</sup>).

Biological CO<sub>2</sub> production in each layer is calculated using an exponentially decreasing function (Nickerson and Risk, 2009):

$$P[i] = \frac{\Gamma_0}{\sum_{i=1}^{N} e^{\frac{-z_i}{Z_p}}} Q_{10}^{\frac{T[i] - T_{avg}}{10}}$$
(4)

where  $\Gamma_0$  is the total basal soil production ( $\mu$ mol m<sup>-3</sup> s<sup>-1</sup>), N is the number of soil layers,  $Q_{10}$  is the temperature sensitivity of soil respiration,  $z_i$  is the depth of the layer (m) and **Zp** is the e-folddepth of production (m), defined as the depth below which the total fraction of  $CO_2$  production remaining is 1/e (also called the damping depth), from which the production at any depth P(i) can be calculated based on equation 4.

Initially, the diffusivity of CO<sub>2</sub> in the soil profile is calculated using the Millington Model (Millingon, 1959), an empirically derived approximation for calculating diffusivity in the field:

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$$D_c = \frac{\theta_w^{\frac{10}{3}} \frac{D_{fw}}{H} + \theta_g^{\frac{10}{3}} D_{fg}}{\theta_T^2}$$
 (5)

 $D_{fw}$  and  $D_{fg}$  are the diffusivity of  $CO_2$  in free water and free air (m<sup>2</sup> s<sup>-1</sup>), H is the dimensionless form of Henry's solubility constant for  $CO_2$  in water, and  $\theta_w$ ,  $\theta_g$  and  $\theta_T$  are the water filled, air filled and total soil porosities, respectively.

At each time step, the diffusivity of each soil layer is calculated using a temperature correction on this Millington diffusivity:

$$D[i] = D_c \left(\frac{T[i]}{T_{avg}}\right)^{1.75} \tag{6}$$

As previously mentioned, the flux from each layer is determined by Fick's first law, written explicitly as:

$$F[i] = D[i] \frac{(C[i] - C[i-1])}{dz} dt \tag{7}$$

where C[i] is the CO<sub>2</sub> concentration of layer i ( $\mu$ mol m<sup>-3</sup>), C[i-1] is the concentration of the layer above, and dt is the time step (s).

Finally, at each time step CO<sub>2</sub> concentration in each layer i is calculated using:

$$C[i] = \frac{C_{t-1}\theta_g dz - F[i] + F[i+1] + P[i]}{\theta_g dz}$$
(8)

where  $C_{t-1}[i]$  is the layer concentration at the previous time step, F[i] is the flux of  $CO_2$  leaving layer i, F[i+1] is the flux of  $CO_2$  entering the layer from the layer below, P[i] is the  $CO_2$  production within layer i.

#### 2.2 Model execution and validation

Before beginning the simulation, the system is initialized using input parameters seen in Table 1. Atmospheric  $CO_2$  concentration remains constant for the duration of the simulation; it is assumed that any flux from the soil will quickly dissipate into the atmosphere. Flux from the bottom soil boundary is set to zero, as production at this depth is negligible according to the exponentially decreasing production function. These system parameters were changed depending on the soil type being simulated.

After initialization, the system undergoes spin-up, during which layer temperatures are held constant at their initial values, and the model is run until the  $CO_2$  concentration in each layer is constant. The duration of the spin up period is dependent on soil diffusivity (and therefore  $\theta_w$ ), and is determined by plotting concentration vs time through the soil profile. This period ranges from 5 to 23 model days within the range of  $\theta_w$  (0.1 to 0.25). The  $CO_2$  concentration in each layer after spin up is the initial layer concentration at the beginning of the actual simulation.

For each modelled time step (dt=1.0 s), temperature, CO<sub>2</sub> diffusivity, CO<sub>2</sub> production and CO<sub>2</sub> flux are calculated in each soil layer. Every soil layer is then revisited, and the new CO<sub>2</sub> layer concentrations are calculated. The progress of the simulation is monitored by outputting the CO<sub>2</sub> concentration and temperature of specified layers.

#### 2.2.1 Validation

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To ensure the model was performing correctly, steady state concentrations through depth (following spin-up) were compared to the steady state solution proposed by Cerling (1984). Daily and yearly temperature fluctuations were removed from the model, and the model was run until CO<sub>2</sub> concentrations in each layer were constant. Deviations of modelled from analytic concentrations were found to be far less than 1%.

In order to model soil conditions, real (or synthetic in the case of this study) measurements must be used to drive the simulation. Measurements of temperature through depth, soil volumetric water content, CO<sub>2</sub> surface flux and CO<sub>2</sub> concentrations take place at 1800 s intervals in the field, and in

our forward synthetic simulations in which we created idealized field data. Soil temperature is an explicit model driver, while CO<sub>2</sub> surface flux and concentration are used as model constraints. Soil volumetric water content is not formally incorporated as a driver of respiration, so simulations are performed over periods of constant soil volumetric water content. Soil volumetric water content is also assumed to be constant through the soil profile.

Accurately modelling soil temperature through depth and time is crucial, as temperature is the known determinant of soil lags (Phillips et al., 2011). For each set of temperature measurements through depth, a linear regression (in R) is performed, resulting in a 5th order polynomial for temperature through depth every 1800 s. A linear interpolation through time is performed to obtain temperature values in each layer for every modelled time step. The resultant temperature values replace our originally sinusoidally varying temperature function in the model. The value of thermal diffusivity is implicitly built into these measurements and is no longer required as a direct model input.

### 2.3 Incorporating constraining data

In this study, we incorporated external data in the same way we would with field studies. We started with real measurements of temperature through depth, and soil volumetric water content, from a local field site. One of the largest challenges in preparing data for inversion is to accurately model soil temperature through depth and time, as temperature is the known determinant of soil lags (Phillips et al., 2011). For each set of temperature measurements through depth, a linear regression (in R) was performed, resulting in a 5th order polynomial for temperature through depth every 1800 s. A linear interpolation through time was performed to obtain temperature values in each layer for every modelled time step. The resultant temperature values replaced our originally sinusoidally varying temperature function in the model. The value of thermal diffusivity was therefore implicitly built into these measurements and is no longer required as a direct model input.

These physical variables were used in a forward instance of the soil model to create  $CO_2$  surface flux and  $CO_2$  concentration timeseries. Datasets were created using many e-folding depths of production, and  $Q_{10}$ s of interest, so that we had many idealized datasets on hand in which concentration, fluxes and associated temperatures, e-folding depths of production, and  $Q_{10}$ s, were known. Soil volumetric water content was not formally incorporated as a driver of respiration in these synthetic datasets, so all simulations were performed over periods of constant soil volumetric water content. During inversion we pretended not to know e-folding depths of production, and  $Q_{10}$ s, of these synthetic datasets, and hoped the inversion process would return the known values. Since the same forward soil model that generated the synthetic datasets was also embedded within the inversion scheme, errors in e-folding depths of production, or  $Q_{10}$ , would be due entirely to the inversion process itself.

# 2.4 Inversion process

The soil profile  $CO_2$  concentrations and soil  $CO_2$  surface flux are outputs of the simulation. Their values are dependent on all of the system input parameters. A method called inverse parameter estimation is employed to determine the values of  $Q_{10}$  and e-fold depth of production that would have given rise to the observed concentrations and fluxes. Through this process, model outputs are compared to measured field data or synthetic data over a range of model input parameters. The field measurements used in this process will be referred to as the model constraints; these constraints consist of  $CO_2$  concentration measurements at various depths in the soil profile, as well as  $CO_2$  surface flux measurements.

## 2.4.1 Inversion steps

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The model is run for two unknowns, including  $Q_{10}$  values ranging from 1 to 5.5 in steps of 0.1, and Zp from 0.02 m to 0.3 m in steps of 0.01 m. This results in a total of 1260 parameter combinations. Inversion seeks to identify the parameter set that minimizes the objective function

$$\sqrt{(S_1 - M_1)^2 + (S_2 - M_2)^2 + (S_3 - M_3)^2 + \dots}$$
(9)

where  $S_i$  and  $M_i$  correspond to modelled and measured  $CO_2$  concentrations at various profile depths. For each parameter set, this objective function is calculated every 1800 timesteps and averaged at the end of the simulation. The pair that minimizes Eq. (9) is output as the inversion result.

## 205 2.5 Validation of the inverse method

Before applying the inversion method to real field data, tests must be done to ensure method accuracy, and this manuscript focuses on such tests. We created synthetic timeseries using the original soil model, that mimic the form of real data sets. The values of  $Q_{10}$  and Zp were known for each synthetic timeseries, as these parameters are required to run the model. This synthetic data included temperature measurements at six depths in the profile, volumetric water content,  $CO_2$  surface flux and  $CO_2$  concentration measurements at various depths in the soil profile.

The inverse method was applied to these synthetic data sets, and the output value of  $Q_{10}$  and  $Z_p$  could then be compared to the actual values of these parameters used to create the timeseries.

## 2.5.1 Constraint, sensitivity, and random error testing

To determine which model constraints resulted in the highest accuracy of the inversion method, the error (Eq. (9)) was calculated using a large range of constraining parameters and combinations thereof. A total of 35 different constraint combinations were tested, representing various combinations of surface CO<sub>2</sub> flux, and subsurface CO<sub>2</sub> concentration measurements up to 0.6 m depth. These combinations are illustrated in Table 2. Testing which constraints consistently returned the most accurate values of Q<sub>10</sub> and Zp aids in determining optimal sensor placing the field.

To ensure model validity across all possible parameter values that may be encountered in the field, extensive sensitivity testing was done using these synthetic timeseries. These timeseries were created across a range of combinations of  $Q_{10}$ , Zp, volumetric water content (diffusivity) and total soil production. Table 3 illustrates the ranges tested for each parameter.

Field-deployable  $CO_2$  sensors typically have 1-5 % error. To see how the model and inversion would perform under these conditions, errors of 1, 5 and 10 % were added into all components of the synthetic data. The effect of these errors on the inverse method were observed.

#### 3 Results and discussion

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Inversions on synthetic timeseries were successful across all tested soil parameters, though some  $CO_2$  concentration measurement depth combinations (surface flux, single or multiple profile measurements) helped to minimize the overall error, as well as the error in  $Q_{10}$  and Zp individually. Errors discussed in this section represent an average from 64 inversions across values of  $Q_{10}$ , efold depth of production, and soil diffusivity as presented in Table 3. In this section, we use either fractional error ( $\frac{|actual-result|}{actual}$ ), or absolute deviation from the actual value (|actual-result|).

# 235 3.1 Best measurement configurations to obtain $Q_{10}$ and Zp via inversion

In Fig. 3 we show the average fractional error in the returned  $Q_{10}$  value for every combination of subsurface CO<sub>2</sub> sensor measurements. Observations of CO<sub>2</sub> concentration shallow in the soil were found to be necessary for highly accurate  $Q_{10}$  estimates. The lowest inversion error for  $Q_{10}$  was 1.85%, in a scenario where subsurface measurements were made at 5, 10 and 15 cm. Single concentration measurements at or above 10 cm also proved successful, with errors < 2.3 %. The least accurate inversions for  $Q_{10}$  occurred when the constraint consisted of (single or multiple)  $CO_2$  concentration measurements deep in the soil profile. We propose that the poor performance of inversion when using deep profile constraints could be related to the low magnitude of thermal and concentration variability at these depths. Deep soil layers are subject to much smaller thermal fluctuations than layers close to the surface. In this less variable environment, CO2 concentrations are less variable and provide less of a signal upon which to anchor inversion. In contrast, CO2 concentrations shallow in the soil exhibited larger variations in temperature and concentration, which presumably allowed  $Q_{10}$  to be extracted more easily. If the primary interest is to obtain  $Q_{10}$  from inversion, multiple CO<sub>2</sub> concentration measurements in the soil were found to be important. It should be noted that, while differences in error rate were noted, errors for all scenarios could be considered tolerably low relative to the normal variance expected from regression-based  $Q_{10}$ , considering the gas transport lags inherent in those data (Phillips et al., 2011).

The average fractional error in Zp for different model sensor combination constraints is also shown in Fig. 3. Out of the 35 combinations tested, only 5 resulted in an average Zp error greater than 2%.

Single concentration measurements shallow or deep in the soil profile caused this larger error, but on average, single concentration measurements at any depth in the soil were less accurate. Inversions constrained by at least one measurement shallow (< 15 cm) and one deep ( $\geq$  30 cm) in the profile returned Zp with 100% accuracy across all sensitivity tests. We did expect that single measurements deep in the profile would perform poorly relative to others, because with the exponentially decreasing production defined in the model,  $CO_2$  production approaches zero at significant depths regardless of the value of Zp and thus cannot perform well as an inversion anchor. The large Zp error of almost 25% associated with soil surface  $CO_2$  flux measurements, was also not surprising. In this situation the inversion scheme must reconstruct Zp mainly via the temporal delay, and damping, between sinusoids of temperature through depth, and soil surface  $CO_2$  flux. Without a concentration measurement in the soil, the gas transport regime is black boxed from the perspective of the inversion scheme, resulting in the large error. Overall, surface  $CO_2$  flux measurements alone are less suited for elucidating information on e-fold depth of production, whereas a combination of shallow and deep measurements is best for reconstructing the distribution of  $CO_2$  production in the soil profile.

In examining inversion accuracy for both parameters  $Q_{10}$  and Zp simultaneously (Fig. 3), we found that multiple concentration measurements shallow in the soil ( $\leq 15$  cm), or combinations shallow in the soil with one deep concentration measurement ( $\geq 30$  cm) were the best constraints. Deep soil measurements and surface flux constraints should therefore be avoided if the aim is the minimize overall error. This overall result is a combination of what was found for  $Q_{10}$  and Zp individually, where shallow measurements were best for  $Q_{10}$  and a combination of shallow and deep measurements resulted in most accurate Zp.

Depending on error tolerance for the final parameter estimates, it is conceivable that the accuracy of all inversions performed here might be sufficient for the community of soil scientists. Out of the 35 combinations tested, 19 resulted in an overall average error less than 5%. The top constraint (measurements at 5,10 and 15 cm) had an average error of 2.01%, and the top 6 combinations all had error less than 3%. These errors are small compared to the degree of random error in  $CO_2$  flux studies (Lavoie et al., 2015). These results are summarized in Table 4, where the top and bottom 5 combinations are listed individually and overall.

This assessment was performed using synthetic data, and even the most ideal field settings will depart from these modelled profiles. For example, we represented  $CO_2$  production through depth using an exponential production function, but a field site may show a linear decrease in production at increasing depths. Clearly users of the inversion process will want to characterize as many site-specific parameters as possible so as to provide proper guideposts and constraints for the inversion, otherwise additional error will be introduced. The sensitivity of the inversion to error is an important question, and will be addressed in a later section.

# 290 3.2 Effect of soil-specific parameters on inversion success

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Having determined the best  $CO_2$  sensor concentration measurement depth to constrain inversions, we can examine how site-specific parameters such as soil diffusivity, depth of  $CO_2$  production and  $Q_{10}$  affect inversion results. For this assessment, we will use the best performing measurement configurations established. Even when not a top choice, we will always include  $CO_2$  surface flux measurements in this section, because of the likelihood that scientists will want to use inversion to analyze these data which are increasing in number rapidly.

Figure 4 a) and b) illustrate how deviation in  $Q_{10}$  and Zp were affected by the diffusivity of site soils. When subsurface sensor combinations were used as a constraint, there was an overall downward trend in  $Q_{10}$  and Zp error with increasing diffusivity. As diffusivity increases (drier soils),  $CO_2$  travels through the soil layers to the surface more quickly which results in decreased lag times, more rapid concentration changes, and more distinct soil responses. Under these conditions of rapid diffusion, inversions were most successful. Sites that are frequently waterlogged with limited air filled pore space tended to be less ideal for inversion, but the optimal instrument configuration still helps ensure reasonably small error throughout the entire range of diffusivities, so there is no strict limitation on the use of the inversion approach in low diffusivity soils.

Figure 4 c) and d) demonstrate the impact of the Zp parameter value on inversion success in terms of deviation in returned  $Q_{10}$  and Zp values. For small Zp values, shallow  $CO_2$  concentration measurements ( $\leq$  15 cm) were the best constraints, presumably because the soil is most active in these top layers. As e-fold depth of production increases, the production of  $CO_2$  is no longer limited to the shallow soil, the exponential production function decreases more slowly. With increasing Zp,  $CO_2$  production in deeper soil layers is higher, and more useful as an inversion constraint. Some matching of deployment depth was also found, where for example shallow concentration measurements were more accurate for returning the correct value of shallow  $CO_2$  production.

Sensitivity tests indicate that increasing the temperature sensitivity of respiration had opposite effects on  $Q_{10}$  and Zp error. Deviation in returned  $Q_{10}$  values increased rather uniformly across the best subsurface measurements, while for most subsurface combinations the Zp error decreased. With increasing  $Q_{10}$ , respiration becomes more sensitive to temperature changes, leading to larger variations in production in the event of a temperature fluctuation. Figure 4 e) and f) illustrate the impact of this parameter on  $Q_{10}$  and Zp error.

With large amounts of existing surface flux data, it is also worth examining the effectiveness of the soil  $CO_2$  surface flux as a constraint, even when it is not the preferred constraint. It is immediately evident from Fig. 4 that inversions constrained by the surface flux resulted in  $Q_{10}$  and Zp deviations that responded much differently to changes in soil diffusivity, e-fold depth of production and  $Q_{10}$ . These deviations were often significantly larger than when subsurface constraints were used. Deviations in  $Q_{10}$  and Zp generally increased as all three parameters increased. This suggests that for low diffusivity, e-fold depth of production and  $Q_{10}$ , surface flux was a reasonable model constraint,

producing errors comparable to the subsurface measurements. This constraint was much less effective for determining depth of  $CO_2$  production. However, Zp was always returned within at least 3.5 cm of its actual value, which for some uses may be an acceptable level of uncertainty. Inversions constrained by surface flux were quite effective in returning  $Q_{10}$ . Returning to Fig. 3, the overall average  $Q_{10}$  error associated with surface flux was less than 5%, which is significantly better than results using deep subsurface measurements. Figure 4 e) suggests that inversions using large  $Q_{10}$  values were responsible for the majority of this error. For  $Q_{10}$  of 1.5, these inversions returned  $Q_{10}$  with 100% accuracy. For the largest  $Q_{10}$ , deviation from the true value climbed as high as 0.6-0.7, which is non-negligible. A shorter model time step could potentially reduce this error, as it may be able to better capture the larger and faster responses associated with high  $Q_{10}$  and diffusivity. As we cannot estimate the  $Q_{10}$  of a site prior to inversion, however, this insight may not be overly useful in site selection. Overall, inversions constrained by the  $CO_2$  surface flux are possible but should be performed with caution, and with reasonable expectations as to the resultant error level.

It is also of interest to examine how the amount of  $CO_2$  production in the soil profile affects inversion. The bulk of our sensitivity tests were performed using a basal  $CO_2$  production of  $10 \mu mol m^{-3} s^{-1}$ , which is a fairly high. In order to test the other extreme, several inversions were performed using a production level of  $1 \mu mol m^{-3} s^{-1}$ . These inversions performed with exactly the same accuracy as those with a production level of 10. From this, we can conclude that the magnitude of production has no effect on inversion success.

## 3.2.1 Random error and inversion

The measurements performed by sensors in the field will always be uncertain to some degree. It is therefore important to examine how these uncertainties in recorded temperature,  $CO_2$  and soil volumetric water content measurements will impact the accuracy of the inversion method. Inversions performed on synthetic data to which random errors of 1, 5 and 10% had been added were indeed less accurate than those performed on idealized data. However the resulting errors in returned  $Q_{10}$  and Zp were not proportional to the amount of error added to the input data, but actually much lower. That is, errors of 5% in the input data did not result in an additional 5% error in output values. An example of this is illustrated in Fig. 5. This plot demonstrates that with random measurement errors in the ranges of 1-5%,  $Q_{10}$  values were still determined with reasonable accuracy. Prior to error addition, deviation in  $Q_{10}$  was around 0.12. This deviation increased to 0.14 for 1% error and 0.17 for 5% error. As sensors in the field are typically uncertain by 1 to 5%, the inversion method remains feasible. We can thus conclude that the inversion process is rather tolerant of error in measurement.

## 3.3 Multi-parameter error landscape

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360 It is worth investigating in detail the error landscape of the inversion process using a multi-parameter sensitivity tests. For this test, we chose the combination of measurements at 5, 10 and 15 cm which had resulted in the most accurate inversions on average.

The results from the sensitivity tests are shown in Fig. 6, panels a) to f). In all combinations, the error in  $\mathbb{Z}p$  was very small, with the maximum error for any single inversion being just over 2%. Despite this small error, it remains evident which soil conditions should be avoided for most accuracy. Sites with low diffusivity, production deep in the soil and low  $Q_{10}$  are the most problematic. This is consistent with the results from Fig. 4 a), c) and e). Trends were not as evident for error in  $Q_{10}$ . In panels a), e) and c) the most notable error was found in panel a) for high e-fold depth of production, low  $Q_{10}$ . There is an error in  $Q_{10}$  here of almost 15%, which equates to a deviation in  $Q_{10}$  of about 0.225 from its actual value. This result is not unreasonable, but it is significantly higher than results from the other inversions. Plot e) demonstrates an interesting result, where there seems to be a valley in the  $Q_{10}$  error, illustrating a tradeoff between e-fold depth of production and diffusivity. This is not evident in the other plots, and does not have an intuitive physical explanation. The effect of  $Q_{10}$  on inversion varies, but success hinges quite clearly on soil diffusivity and depth of  $CO_2$  production. Choosing a site in the appropriate ranges of these two parameters will maximize chances of success.

Some of the soil parameters across which we tested are obviously unknown *a priori*. The unknown value of Q<sub>10</sub> has already been noted, and depth of CO<sub>2</sub> production may also be unknown prior to inversion. Knowledge of root distribution in the soil could be one aid in site selection and instrumental configuration. On average, root respiration accounts for 50 percent of soil respiration (Hanson et al., 2000) and Jackson et al. (1996) provides root distributions for different terrestrial biomes. Jackson et al. (1996) found that tundra, boreal forest and temperate grasslands had upwards of 80-90 percent of roots within the top 30 cm of soil whereas deserts and temperate coniferous forests had much deeper rooting profiles, with only 50 percent of roots within the top 30 cm. These and other methods may help inform the configuration of field experiments, and may be helpful in providing constraint data when running inversions on real timeseries.

## 3.4 Limitations and opportunities

There are both limitations and future opportunities for the inversion approach. In general, the better an inversion is constrained with data, the better it will do in returning the true value for parameters of interest. Some of the soil parameters are distributed in ways that must be assumed. For example, the distribution of CO<sub>2</sub> production may be unknown. While most studies in the history of soil modelling have assumed an exponential distribution (and it has been seen in many studies using the gradient technique), some other considerations might help determine whether additional parameterization

measurements are needed. For example, knowledge of rooting depth could be one aid. On average, root respiration accounts for 50% of soil respiration (Hanson et al., 2000) and Jackson et al. (1996) provides root distributions for different terrestrial biomes. Jackson et al. (1996) found that tundra, boreal forest and temperate grasslands had upwards of 80-90% of roots within the top 30 cm of soil whereas deserts and temperate coniferous forests had much deeper rooting profiles, with only 50% of roots within the top 30 cm. These and other methods may be helpful in providing constraint data when running inversions on real timeseries.

A future opportunity for inversion studies is to determine depth-specific  $Q_{10}$ , which would be of interest to many researchers. Currently there are few field examples where researchers have determined in-situ  $Q_{10}$  as a function of depth, but two examples of such data using include gradient studies include Risk et al. (2008); Tang et al. (2003). Incubations might seem useful in this regard, but are disputed as a representation of in-situ conditions, especially at depth (Risk et al. 2008). Ideally, an inversion approach could determine depth-specific  $Q_{10}$ , but the reality is challenging. If an additional 100  $Q_{10}$  values were included as unknowns (one for each layer), it would increase computational demand by 100 times. The inversion results would also be confusing, and extreme values at one depth could potentially cause a spurious match to the measured data. The number of non-unique and implausible solutions would rise significantly as a result. A more reasonable approach might be to define  $Q_{10}$  as we do e-fold, which is as a function of soil depth. This would be computationally compact but whether a function would be realistic is not well known because there are so few examples of  $Q_{10}$ -depth profiles against which we could evaluate this approach. The best approach would be to use many profile concentration sensors for constraining data, so that e-fold depth of production could be known, and the inversion could focus instead solely on determining layer-specific  $Q_{10}$ .

Despite the relatively nascent stage of our soil CO<sub>2</sub> inversion approach, indications are that it has better theoretical validity than traditional regression approaches, which do not take thermal-and gas-transport lags into account. Our error results here compare very favourably against error analyses generated from detailed examination of regression approaches across thermal- and gas-transport parameter space (Zhang et al., 2015; Phillips et al., 2011; Graf et al., 2008).

### 4 Conclusion

Overall, this inversion method proved successful in preliminary testing on synthetic data. Depending on the tolerable level of error for a given application, almost every tested combination resulted in reasonably accurate returned  $Q_{10}$  and Zp values. The subsurface concentration measurements that yielded the highest error were typically those that would be of least convenience to install and maintain deep in the soil profile. The other constraint associated with high overall error was  $CO_2$  surface flux, which would likely be the data with highest availability. Most of the error from this constraint arises in estimating the Zp parameter. The  $CO_2$  surface flux is still a reasonable means

of estimating  $Q_{10}$  values via inversion. While in most cases the error was lower for high diffusivity, shallow production soils, the application of this method is certainly not limited to such regions.

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This method is computationally intensive as it performs a sweep through all possible combinations in parameter space. This study used roughly 2.5 core-years of time despite the fact that synthetic timeseries were short. This full sweep ensures that the global minimum in the objective function is located every time, and when solving inversely for two unknown parameters (as we are), this is not an unreasonable approach. However, if it was of interest in the future to examine longer timeseries, or additional parameters such as the depth dependence of  $Q_{10}$ , resulting in additional unknown parameters, it may be beneficial to explore other search algorithms to increase efficiency, such as Simulated Annealing.

The next step for this work would be to perform inversions on real timeseries with appropriate measurement constraints, to obtain temperature sensitivity and CO<sub>2</sub> production depth estimates for various sites. With the increasing availability of high frequency soil data, there would be no shortage in data to analyze. Applying this method for periods of varying constant moisture levels could also help build an understanding of moisture effects on temperature sensitivity of respiration.

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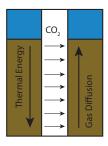
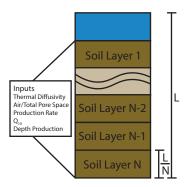


Figure 1. Thermal and gas diffusion lags through a soil profile.



**Figure 2.** Conceptual representation of the 1-D layered soil model. Overall profile length is denoted with L, and N represents the number of individual layers in the model soil profile.

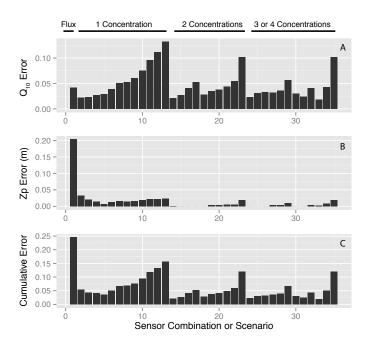
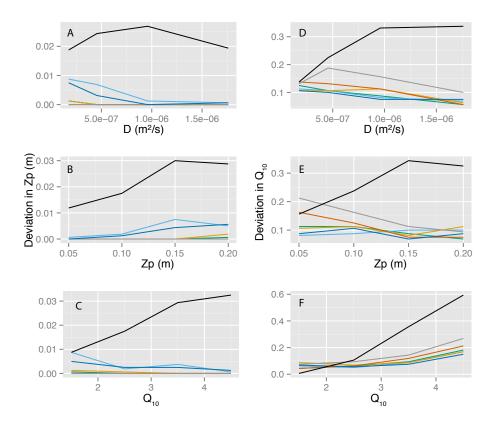


Figure 3. Fractional Error in  $Q_{10}$  and Zp individually for different sensor combination scenarios, plus cumulative fractional error in  $Q_{10}$  and Zp for the same scenarios.



**Figure 4.** Error in  $Q_{10}$  and Zp as a function of  $Q_{10}$  (Panels C,F), Zp (Panels B,E) and D (Panels A,D), for a grouping of the best sensor measurement depth combinations. Individual 5 cm and 10 cm observational scenarios are shown in light blue and dark blue, respectively. The 5+15 cm measurement scenario is shown in green. Orange and red illustrate sensitivity of the 5+10+15 cm and 5+10+30 cm scenarios, respectively. Finally, the 4-point 5+15+30+60 cm measurement sensitivity is represented in grey while the surface flux scenario is shown in black. For these sensitivity tests, the known  $Q_{10}$  was 2.0, and a Zp of 0.2 m was used.

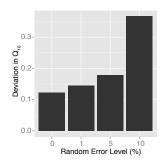
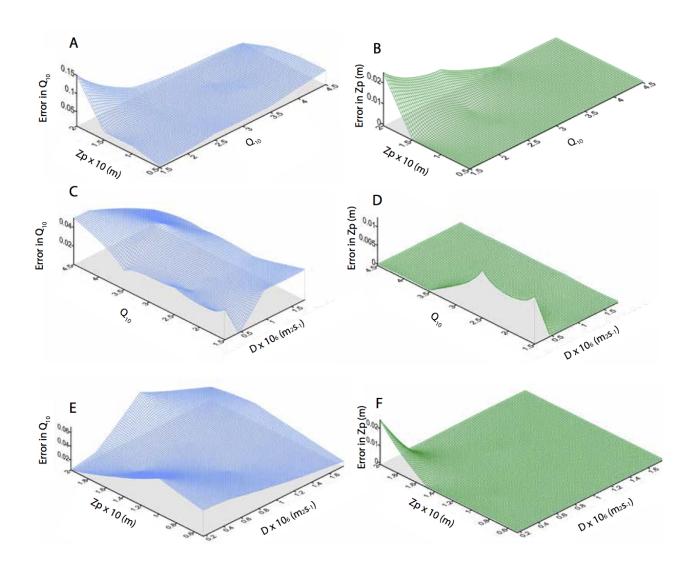


Figure 5. Sample of random error effects on inversion, constrained by one concentration measurement at 5 cm. For this sensitivity test, the known  $Q_{10}$  was 2.0.



**Figure 6.** Error in  $Q_{10}$  and  $Z_p$  as a function of  $Q_{10}$ ,  $Z_p$  and Diffusivity for the constraint 5+10+15 cm. For these sensitivity tests, the known  $Q_{10}$  was 2.0, and a  $Z_p$  of 0.2 m was used.

**Table 1.** Default parameter values for simulations

| Parameter  | Value/Range                                    |
|--|--|
| Soil porosity $(\theta_T)$                       | 0.40 (v/v)                                     |
| Thermal diffusivity $(D_T)$                      | $5 \times 10-7  (\text{m}^2  \text{s}^{-1})$   |
| Average air and soil temperature $(T_{avg})$     | 15°C   |
| Daily air temperature amplitude ( $\Delta T_D$ ) | $5^{o}\mathrm{C}$                              |
| Yearly air temperature amplitude $(\Delta T_Y)$  | 12°C   |
| Atmospheric CO <sub>2</sub>                      | 380 ppm  |
| Total basal $CO_2$ production $(\Gamma_0)$       | $1  10 \ \mu\text{mol m}^{-2} \ \text{s}^{-1}$ |
| Production exponential folding depth (Zp)        | 0.05-0.20 m                                    |
| $Q_{10}$   | 1.5-4.5  |
| Volumetric water content $(\theta_w)$            | 0.10-0.25 (v/v)                                |

**Table 2.** Measurement combinations used for the simulations. The combination number is listed at the beginning of each row. The columns represent the type of measurement (e.g.  $CO_2$  surface flux), or the depth of concentration measurement in centimetres. The "X" values denote whether the type or depth of measurement was included in the combination.

| Combination | Flux | 5 | 10 | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 |
|-------------|------|---|----|----|----|----|----|----|----|----|----|----|----|
| 1           | X    |   |    |    |    |    |    |    |    |    |    |    |    |
| 2           |      | X |    |    |    |    |    |    |    |    |    |    |    |
| 3           |      |   | X  |    |    |    |    |    |    |    |    |    |    |
| 4           |      |   |    | X  |    |    |    |    |    |    |    |    |    |
| 5           |      |   |    |    | X  |    |    |    |    |    |    |    |    |
| 6           |      |   |    |    |    | X  |    |    |    |    |    |    |    |
| 7           |      |   |    |    |    |    | X  |    |    |    |    |    |    |
| 8           |      |   |    |    |    |    |    | X  |    |    |    |    |    |
| 9           |      |   |    |    |    |    |    |    | X  |    |    |    |    |
| 10          |      |   |    |    |    |    |    |    |    | X  |    |    |    |
| 11          |      |   |    |    |    |    |    |    |    |    | X  |    |    |
| 12          |      |   |    |    |    |    |    |    |    |    |    | X  |    |
| 13          |      |   |    |    |    |    |    |    |    |    |    |    | X  |
| 14          |      | X |    | X  |    |    |    |    |    |    |    |    |    |
| 15          |      | X |    |    |    |    | X  |    |    |    |    |    |    |
| 16          |      | X |    |    |    |    |    |    |    |    | X  |    |    |
| 17          |      | X |    |    |    |    |    |    |    |    |    |    | X  |
| 18          |      |   |    | X  |    |    | X  |    |    |    |    |    |    |
| 19          |      |   |    | X  |    |    |    |    |    |    | X  |    |    |
| 20          |      |   |    | X  |    |    |    |    |    |    |    |    | X  |
| 21          |      |   |    |    |    |    | X  |    |    |    | X  |    |    |
| 22          |      |   |    |    |    |    | X  |    |    |    |    |    | X  |
| 23          |      |   |    |    |    |    |    |    |    |    | X  |    | X  |
| 24          |      | X |    | X  |    |    | X  |    |    |    |    |    |    |
| 25          |      | X |    | X  |    |    |    |    |    |    | X  |    |    |
| 26          |      | X |    | X  |    |    |    |    |    |    |    |    | X  |
| 27          |      |   |    | X  |    |    | X  |    |    |    | X  |    |    |
| 28          |      |   |    | X  |    |    | X  |    |    |    |    |    | X  |
| 29          |      |   |    |    |    |    | X  |    |    |    | X  |    | X  |
| 30          |      | X |    | X  |    |    | X  |    |    |    | X  |    |    |
| 31          |      | X |    | X  |    |    | X  |    |    |    |    |    | X  |
| 32          |      |   |    | X  |    |    | X  |    |    |    | X  |    | X  |
| 33          |      | X | X  | X  |    |    |    |    |    |    |    |    |    |
| 34          |      |   |    |    |    | X  | X  | X  |    |    |    |    |    |
| 35          |      |   |    |    |    |    |    |    |    |    | X  | X  | X  |

 Table 3. Default parameter values for sensitivity testing.

| Parameter   | Abbr.      | Minimum | Maximum | Increment |
|---|------------|---------|---------|-----------|
| Total basal $CO_2$ production ( $\mu$ mol m <sup>-2</sup> s <sup>-1</sup> ) | $\Gamma_0$ | 1       | 10      | 10        |
| Production exponential folding depth (m)                                    | Zp         | 0.05    | 0.2     | 0.05      |
| $Q_{10}$  |            | 1.5     | 4.5     | 1         |
| Volumetric water content (v/v)  | $\theta_w$ | 0.1     | 0.25    | 0.05      |

 $\textbf{Table 4.} \ \ \text{Best and worst sensor combinations for determining } \ Q_{10}, \\ \textbf{Zp} \ \ \text{and overall through inversion}.$ 

|      |                   | Combination  |                   |  |  |
|------|-------------------|--------------|-------------------|--|--|
| Rank | $Q_{10}$          | Zp           | Overall           |  |  |
| 1    | 5+10+15 cm        | n/a          | 5+10+15 cm        |  |  |
| 2    | 5+15 cm           | n/a          | 5+15 cm           |  |  |
| 3    | 5 cm              | n/a          | 5+15+30 cm        |  |  |
| 4    | 10 cm             | n/a          | 5+15+30+60 cm     |  |  |
| 5    | 5+15+30 cm        | n/a          | 5+30 cm           |  |  |
| 31   | 45 cm             | 55 cm        | 50 cm             |  |  |
| 32   | 50 cm             | 50 cm        | 50+60/50+55+60 cm |  |  |
| 33   | 50+60/50+55+60 cm | 60 cm        | 55 cm             |  |  |
| 34   | 55 cm             | 5 cm         | 60 cm             |  |  |
| 35   | 60 cm             | Surface Flux | Surface flux      |  |  |