

# Modification of the RothC model to simulate soil C mineralization of exogenous organic matter

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**Abstract.** The development of soil organic C (SOC) models capable to produce accurate predictions of the long term decomposition of exogenous organic matter (EOM) in soils is important for an effective management of organic amendments. However, reliable C modelling in amended soils requires specific optimization of current C models to take into account the high variability of EOM origin and properties. The aim of this work was to improve the prediction of C mineralization rates in amended soils by modifying the RothC model to encompass a better description of EOM quality.

15 The standard RothC model, involving C input to the soil only as decomposable (DPM) or resistant (RPM) organic material, was modified by introducing additional pools of decomposable (DEOM), resistant (REOM) and humified (HEOM) EOM.

The partitioning factors and decomposition rates of the additional EOM pools were estimated by model fitting to respiratory curves of amended soils. For this task, 30 EOMs from 8 contrasting groups (compost, anaerobic digestates, sewage sludges, 20 agro-industrial wastes, crop residues, bioenergy by-products, animal residues, meat and bone meals), were added to 10 soils and incubated under different conditions.

The modified Roth C model was fitted to C mineralization curves in amended soils with great accuracy (mean correlation coefficient: 0.995). Differently to the standard model, the EOM-optimized RothC was able to better accommodate the large variability in EOM source and composition, as indicated by the decrease in the root mean squared error of the simulations 25 for different EOMs (from 29.9% to 3.7% and from 20.0% to 2.5% for bioethanol residue and household waste compost amended soils, respectively). Average decomposition rates for DEOM and REOM pools were  $89 \text{ y}^{-1}$  and  $0.4 \text{ y}^{-1}$ , higher than the standard model coefficients for DPM ( $10 \text{ y}^{-1}$ ) and RPM ( $0.3 \text{ y}^{-1}$ ).

Results indicate that explicit treatment of EOM heterogeneity enhances the model ability to describe amendment 30 decomposition under laboratory conditions and provides useful information to improve C modelling on the effects of different EOM on C dynamics in agricultural soils.

Future researches involve the validation of the modified model with field data and its application to long term simulation of SOC patterns in amended soil at regional scale under climate change.

## 1 Introduction

Exogenous organic matter (EOM) is all organic material of biological origin that is applied to cultivated fields for the purpose of growing crops, improving soil quality and restoring or reclaiming land for future use (Marmo et al., 2004). Agricultural utilization of EOM is considered to be an effective way of restoring losses of soil organic matter (SOM) and offsetting soil degradation and climate change (Lal, 2004; Smith, 2004a; Smith, 2004b). A reliable management of amendment requires a thorough knowledge of EOM mineralization patterns, as the rate of EOM decomposition is critical to determine its effects on soil properties, nutrient cycling and C accumulation.

However, prediction of EOM transformation in soil is a very difficult task as EOM mineralization is an extremely complex process depending on several factors such as EOM biochemical composition, EOM stabilization treatment, size and activity of soil microorganisms and pedoclimatic conditions (Franzluebbers, 2004). In particular, EOM composition is extremely variable, since organic residues may have plant or animal origin and may have undergone different stabilization treatments.

Process-oriented soil organic C (SOC) modelling represents a reliable solution for an efficient management of EOM amendment as it offers in principle a unique mean of addressing the high variability in the properties of EOM and pedoclimatic conditions and the complexity of mechanisms and factors affecting C mineralization in the field. The effectiveness of models in predicting long term C changes in amended soils has been recently supported by findings of Karhu et al. (2012), Noirot-Cosson et al. (2016), Peltre et al. (2012), and Plaza et al. (2012), who found good correlations between modelled and measured C stocks for different types and amounts of EOM. Some examples of C models that have been utilized to simulate SOC trends in amended soils at field scale are reported in Table 1.

As the composition and properties of amendments is the most important factor controlling their decomposition (Cavalli et al., 2014; Do Nascimento et al., 2012; Karhu et al., 2012), several authors have highlighted the importance of a proper characterization of EOM to decrease the uncertainty in model predictions of SOC trends in amended soils. Regarding the relevance of organic matter (OM) quality in SOC modelling, most models are based on the concept that decomposition can be adequately simulated by assuming different conceptual or functional pools of OM that decay according to first order kinetics with specific decomposition rate constants (Borgen et al., 2011). Exogenous organic matter is composed by substances with different properties and distinct levels of accessibility to microorganisms. The rate of EOM mineralization is mainly determined by the combination between quality and accessibility and the intensity of response to environmental factors of substrates with diverse characteristics. Therefore, an accurate partitioning of EOM into a number of discrete pools and estimation of their functional characteristics (i.e. initial C and N contents, decomposition rate) is of great importance to improve model predictions (Sierra et al., 2011; Thuries et al., 2001). Generally C models identify two or three pools of EOM, while their decomposition rates can be fixed or variable according to the specific EOM. However, rigorous methods for establishing entry pools that account for the diversity of EOM have not been developed to date (Peltre et al., 2012). This represents one of the major problems for a reliable C modelling of amended soil, as this separation is challenging and no

65 universally recognized methodology exists to perform this task. According to Petersen et al. (2005b), the uncertainty related to the fractionation of EOM into pools is one of the major weaknesses associated to the C modelling of amended soils. Several approaches have been proposed in order to determine EOM pools partitioning factors and decomposition rates, but, to date, no satisfactory method for such characterization have been found. The main approaches that have been devised so far are based on chemical or kinetic subdivision of EOM. Partitioning based on the chemical properties of EOM is generally  
70 performed by stepwise chemical digestion (SCD) and near infrared reflectance spectroscopy (NIRS)(Borgen et al., 2011; Peltre et al., 2011). Such methods are relatively rapid and simple, but presents the main disadvantage that these operationally defined fractions do not precisely correspond to the model pools. An alternative to chemical analysis is to characterize EOM pools by direct fitting of simulated CO<sub>2</sub> emissions to measured respiration curves from incubation experiments (Barak et al., 1990). Fitting pool parameters in this way provides kinetically defined parameters that reflect the rate of C mineralization  
75 observed for each residue (Borgen et al., 2011; Trinoustrot et al., 2000) and is appealing because it allows for simultaneous estimation of both pool size and decomposition rate (Scharnagl et al., 2008) that can be directly used in process-oriented models (Batlle-Aguilar et al., 2011). EOM pools characterization by fitting CO<sub>2</sub> respiration from incubations was successfully achieved for NCSOIL (Corbeels et al., 1999; Gabrielle et al., 2004; Noirot-Cosson et al., 2016), CANTIS (Garnier et al., 2003; Parnaudeau, 2005) and TAO (Pansu and Thuries, 2003) models and was also performed by several  
80 other researchers (Antil et al., 2011; Borgen et al., 2011; Cavalli and Bechini, 2011). In general, results of previous works on EOM characterization for soil C model calibration showed that kinetically defined partitioning enhances the predictions of mechanistic models compared to operationally defined fractions (Borgen et al., 2011; Gabrielle et al., 2005) and that the wider applicability of EOM characterization by SCD and NIRS is obtained at the expense of a lower accuracy.

To date, there are no soil C models specifically developed to evaluate the C accumulation potential of amended soils, with the only exception of the TAO (transformation of added organic matter) model (Pansu and Thuries, 2003). Furthermore, C models have not been extensively calibrated in amended soils and the quality of organic inputs is an aspect that has not been adequately considered and needs further investigation (Parshotam et al., 2001). An example of this inadequacy is represented by the Rothamsted Carbon model (RothC), one of the most well-known and widely used models simulating SOC trends (Jenkinson et al., 1991; McGill, 1996), because it requires relatively few and easily available parameters and input data.  
85 Although it has also been used in a few occasions to make predictions following application of EOM (Yokozawa et al., 2010), its actual structure suggests that the model is not particularly suited for C simulation in amended soils. Carbon inputs to the model are divided in the decomposable plant material (DPM) and resistant plant material (RPM) pools, each one characterized by a specific decay rate. This implies that the model does not allow C inputs deriving from crop residues to be differentiated from EOM. Secondly, the quality of the OM entering in the soil is only defined by the partitioning between  
90 decomposable and resistant organic materials, as the decomposition rate are fixed and constant for each pool. The insensitivity of the actual model to the variation in the quality of inputs was showed by Falloon (2001). In fact, RothC allows only a specific EOM, namely farmyard manure, to be treated separately from crop residues, but its partition coefficients and decomposition rates are fixed. This model behaviour contrasts with the large variability in the decomposition rate of different  
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EOMs and the evidence that model predictions can be improved by identification of EOM specific decomposition rate, as demonstrated by Mueller et al. (2003) with the DAISY model. Similarly to RothC, the original DAISY model involves two pools of added EOM with decomposition rates that are constant for a wide range of added organic materials. Mueller et al. (2003) showed that adjusting the decomposition rates for each EOM significantly increased the model capacity to predict C mineralization in amended soils.

The aim of this study was to devise an easy and effective procedure for the optimization of the RothC model to improve the prediction of EOM-C mineralization, as a first step of model development for reliable SOC simulation in amended soils. Such procedure is based on two steps:

- modification of RothC involving the introduction of additional entry pools of EOM
- utilization of information derived from laboratory incubation experiments to define the size and decomposition rate of the additional EOM pools.

## 110 **2 Materials and Methods**

### **2.1 Incubation experiments**

#### **2.1.1 Soils used for incubations**

The soils used for the incubation experiments were sampled from agricultural areas in the Mediterranean area and specifically in Northern Italy and Southern Spain. The soils were sampled at 5-20 cm depth with an auger and several subsamples were pooled together to obtain a representative sample. Location and main physico-chemical characteristics of the soils are reported in Table 2.

The soil were sieved moist through a 2 mm aperture grid and stored (5 °C) until the beginning of the experiments. Before the starting of the trials, the soils were pre-conditioned by incubation under aerobic conditions for 7 days at the same temperature and water content adopted for the experiments.

120 The range of soils showed a widely different texture and pH. Apart from Gorizia, Bueriis and Lodi, the samples were characterized by low contents of organic C and N and a small pool of soil microbial biomass.

#### **2.1.2 EOMs used for incubations**

As a whole 30 different EOMs were utilized for the incubation experiments. They were considerably distinct in terms of origin, chemical composition, and stabilization/transformation processes to which they were subjected. According to the above properties they were classified in 9 different EOM groups (Table 3) and their main features and properties are reported on Table 4. Most of them presented an alkaline pH, while the organic wastes with a pH < 5.2 were bioethanol residue, hydrolyzed leather and two-phase olive mill waste. The total organic C (TOC) concentration ranged between 28.2% and 53.0%, except for green waste biochar, which had a TOC content of 86.0%. Total N varied between 0.3% and 17%, mainly

depending to the EOM origin. Generally, vegetal derived EOM as vine shoots compost, household waste compost, green waste compost, crop residues, two-phase olive mill waste and green waste biochar showed low levels of total N (0.3-2.3%). On the other side, EOM of animal origin (meat and bone meals, blood meal, horn and hoof meal) showed high values of N (8.2-17.0%). As a consequence of the variability in C and N content, the C/N ratio ranged between 3 (horn and hoof meal) to almost 200 (wheat straw) and 345 (green waste biochar). The differences among EOMs were also highlighted by the content of easily available C (WSC) and N (WSN), varying from 0.1 to 203 g kg<sup>-1</sup> and from 0 to 37.9 g kg<sup>-1</sup> for WSC and WSN, respectively. The EOMs showing the highest contents of easily degradable C and N were bioethanol residue and blood meal. In general high concentrations of mineral N (NO<sub>3</sub><sup>-</sup> and NH<sub>4</sub><sup>+</sup>) were found for liquid digestates. Conversely, bioenergy by-products two-phase olive mill waste, and biochar were characterized by very low amounts of NO<sub>3</sub><sup>-</sup>.

### **2.1.3 Amended soils incubation experiments**

The solid residues were ground and sieved (< 0.5 mm) to homogenize their particle size before application. The residues were thoroughly mixed with pre-conditioned moist soil samples (50 g dry weight basis) at the beginning of the incubation and kept under aerobic conditions in the dark in 130 ml plastic jars in a thermostatic chamber. In the case of liquid residues soil were pre-incubated at such humidity that after EOM addition they were brought to the moisture content required for incubation. Unamended soils were also included as a control. Each treatment was replicated at least twice. The moisture levels in the jars were checked weekly by measuring weight loss, and deionised water was added when necessary to maintain constant moisture. Incubations were performed for a range of temperature (10-30 °C), soil moisture (20-40% water holding capacity (WHC)) EOM rate (0.1-0.75 %) and time (7-37 d) conditions. Details on incubation conditions (soil type, rate of residue, soil water content, temperature and incubation time) are reported on Tables S1-S6 of Supplement. As a whole, more than 30 incubations (each involving 7 treatments) were performed, utilizing 30 different residues and 10 soils with contrasting properties for a total of 224 treatments.

### **2.1.4 Soil CO<sub>2</sub> measurement**

CO<sub>2</sub> evolution was measured every 6 h on aliquots of moist soils by means of an automated system for gas sampling and measurement (Mondini et al., 2010). (Fig. 1). The ‘apparent’ net C mineralisation (C derived from the residues) was calculated as the difference between the CO<sub>2</sub>-C emitted by the EOM amended soil and that produced over the same period by the unamended control soil.

## **2.2 RothC model modification and optimization**

### **2.2.1 Description of the RothC model**

The Rothamsted Carbon model (RothC) was one of the first multi-compartmental models to be developed (Coleman and Jenkinson, 1996; Jenkinson and Rayner, 1977) and has been evaluated and optimized for a variety of ecosystems including

croplands, grasslands and forests (Coleman et al., 1997; Falloon and Smith, 2002; Smith et al., 1997) and in various climate regions, including Mediterranean and semi-arid environments (Farina et al., 2013; Francaviglia et al., 2012; Skjemstad et al., 2004).

RothC describes the dynamics of SOM by splitting it into five compartments with different decomposition (or kinetic) rate constant (K), namely decomposable plant material (DPM,  $K = 10 \text{ y}^{-1}$ ), resistant plant material (RPM,  $K = 0.30 \text{ y}^{-1}$ ), soil microbial biomass (BIO,  $K = 0.66 \text{ y}^{-1}$ ), humified organic matter (HUM,  $K = 0.02 \text{ y}^{-1}$ ) and inert organic matter (IOM). Each compartment, except IOM, follows first-order decay kinetics, i.e. each pool is considered well-mixed and chemically homogeneous and the decomposition rate is assumed to be controlled by the available substrate. The proportion of organic matter decomposed per unit time is therefore constant and equal to K.

The model considers two main type of C inputs to the soil: crop residues and farmyard manure. Crop residues are divided into compartments of DPM and RPM with partitioning factors (f) depending on the nature of the inputs. The partitioning of FYM into pools is fixed and corresponds to DPM 49%, RPM 49% and HUM 2%. At each monthly time step, part of each C input pool is decomposed according to its specific decomposition rate. Part is mineralized as  $\text{CO}_2$  and the rest is transferred to the compartments BIO and HUM. The proportion of the decomposed pool converted to  $\text{CO}_2$  and (BIO + HUM) is determined by the clay content of the soil. The rate constants are modified at each period by three multipliers, depending on the temperature, the moisture deficit of soil and the presence/absence of vegetation. Due to extensive previous evaluations of model performance (e.g. Smith et al., 1997), no further validation of the current model is presented here.

## 2.2.2 Modification of the RothC model

The standard model considers C input to the system by EOM only as farmyard manure with fixed partitioning factors. Since in the present study a wide range of EOMs with different characteristics was added to the soil, and in agreement with the procedure adopted by Peltre et al. (2012) and Falloon (2001) for RothC simulation in amended soils, in a first stage of the study fitting of the RothC model to the respiratory curves was assessed by varying the partitioning factors of EOM pools. To enable model fitting of respiration data from the incubation trials, an Excel version of the RothC model (26.3 version) was utilized. The Excel version of the model was tested for correctness under several RothC standard scenarios.

A total of 86 simulations were performed considering soil amended with residues from different EOM groups. All the simulations were run as difference with the control treatment (i.e. only the  $\text{CO}_2$  derived from EOM was simulated) utilizing a time step of  $0.25 \text{ d}^{-1}$ . Thus the initial size of the soil organic pools was virtually set to zero, including the size of the inert OM pool (IOM). This was possible because in the RothC model the C trend of each pool is described with first order kinetics. Hence, the fate of total soil C is the sum of the fate of the C of the different pools. Consequently, the difference in  $\text{CO}_2$  evolution between soils with and without EOM application corresponds to the  $\text{CO}_2$  derived from the additional input of OM in the soil. It was therefore assumed that the decomposition of humified SOM was unaffected by the decomposition of added residues (i.e. no priming effect was caused by EOM application to the soil).

Model fitting to measured values was conducted by changing individual partition coefficients ( $f_{DPM}$ ,  $f_{RPM}$ ,  $f_{HUM}$ ) of the EOM pools by stepwise iteration using Excel-Solver with the Newton method until maximum agreement between measured and simulated amounts of CO<sub>2</sub> was achieved assuming as a criteria the smallest sum of squared residuals (SSR). An humified pool was attributed only to residues characterized by the presence of stable OM, such as compost, anaerobic digestates and olive mill waste. For each EOM and incubation conditions, an 'individual' fitting procedure was used to minimise the difference between observed and simulated values. The 3 parameters were optimized simultaneously, considering the following constraints in order to avoid biologically unrealistic parameter estimates:

$$f_{DPM} + f_{RPM} + f_{HUM} = 1$$

$$f_{HUM} < 0.3 \text{ for anaerobic digestates and agro-industrial wastes}$$

The partitioning factor for HUM was set to a maximum of 0.3 in the case of digestate and agro-industrial wastes according to the values found by Cavalli and Bechini (2011; 2012) after model calibration for soil amended with pig slurries stored under anaerobic conditions before use.

The capacity of the standard model to fit C mineralization curves of amended soils was assessed by calculating the root mean squared error (RMSE), i.e. the total difference between measured and simulated values, expressed as percentage of the mean observed values.

As results of the fitting procedure were not acceptable due to the high values of RMSE (see below section 3.2), a modification to the model source code was performed to improve the model ability to describe respiratory curves of amended soil. The proposed modification involves the inclusion of two additional pools of EOM (decomposable EOM (DEOM) and resistant EOM (REOM)), each one characterized by specific and variable rate of decomposability.

Furthermore, for organic residues characterized by the presence of stable OM (i.e. compost, anaerobic digestate and agro-industrial wastes), a third EOM pool is introduced (humified EOM (HEOM)) which is directly incorporated into the soil HUM pool. EOM added to the soil is split into the DEOM, REOM and HEOM pools according to the partitioning factors  $f_{DEOM}$ ,  $f_{REOM}$  and  $f_{HEOM} = 1 - f_{DEOM} - f_{REOM}$ . DEOM and REOM pools decompose with specific decomposition rates ( $K_{DEOM}$  and  $K_{REOM}$ ), that may be different from those of plant residues, while HEOM, being directly incorporated into the HUM pool, decomposes with the same decomposition rate ( $K = 0.02 \text{ y}^{-1}$ ). Decomposed DEOM and REOM are split in CO<sub>2</sub>, BIO and HUM. The proportion of decomposed DEOM and REOM that goes to CO<sub>2</sub>, BIO and HUM is regulated in the same way as for the entry pools of plant residue. Below is reported a mathematical representation of the modified model as a set of differential equations:

$$\frac{dDPM}{dt} = f_{DPM}P - K_{DPM}DPM \quad (1)$$

$$\frac{dRPM}{dt} = (1 - f_{DPM})P - K_{RPM}RPM \quad (2)$$

$$\frac{dDEOM}{dt} = f_{DEOM}E - K_{DEOM}DEOM \quad (3)$$

$$\frac{dREOM}{dt} = f_{REOM}E - K_{REOM}REOM \quad (4)$$

225             $\frac{d\text{BIO}}{dt} = \alpha K_{\text{DPM}} \text{DPM} + K_{\text{RPM}} \text{RPM} + K_{\text{DEOM}} \text{DEOM} + K_{\text{REOM}} \text{REOM} + K_{\text{HUM}} (\text{HUM} + (1 - f_{\text{DEOM}} - f_{\text{REOM}}) E) - (1 - \alpha) K_{\text{BIO}} \text{BIO}$             (5)

$\frac{d\text{HUM}}{dt} = \beta (K_{\text{DPM}} \text{DPM} + K_{\text{RPM}} \text{RPM} + K_{\text{DEOM}} \text{DEOM} + K_{\text{REOM}} \text{REOM} + K_{\text{BIO}} \text{BIO}) - (1 - \beta) K_{\text{HUM}} (\text{HUM} + (1 - f_{\text{DEOM}} - f_{\text{REOM}}) E)$             (6)

$\frac{d\text{IOM}}{dt} = 0$             (7)

230 where:

DPM = decomposable plant material; RPM = resistant plant material; HUM = humified organic matter; BIO = soil microbial biomass; DEOM = decomposable EOM; REOM = resistant EOM; IOM = inert organic matter.

$f_{\text{DPM}}$  = partitioning factor for DPM;  $f_{\text{DEOM}}$  = partitioning factor for DEOM;  $f_{\text{REOM}}$  = partitioning factor for REOM.

$K_{\text{DPM}}$  = decomposition rate for DPM;  $K_{\text{RPM}}$  = decomposition rate for RPM;  $K_{\text{BIO}}$  = decomposition rate for BIO;  $K_{\text{HUM}}$  = decomposition rate for HUM;  $K_{\text{DEOM}}$  = decomposition rate for DEOM;  $K_{\text{REOM}}$  = decomposition rate for REOM.

P = plant (crop residue) input; E = EOM input;  $\alpha$  = transfer coefficient to BIO pool;  $\beta$  = transfer coefficient to HUM pool.

The C flow of the standard and modified model is reported in Fig. 2.

An Excel version of the modified model was then utilized to perform model fitting of the same 86 respiratory curves previously simulated with the standard model. The procedure utilized was the same with the exception that model fitting was conducted by simultaneously changing partitioning factors ( $f_{\text{DEOM}}$ ,  $f_{\text{REOM}}$ ,  $f_{\text{HEOM}}$ ) and decomposition rate constants ( $K_{\text{DEOM}}$ ,  $K_{\text{REOM}}$ ) of the different pools of EOM, considering the following constraints in order to avoid biologically unrealistic parameter estimates:

$$f_{\text{DEOM}} + f_{\text{REOM}} + f_{\text{HEOM}} = 1$$

$$f_{\text{HEOM}} < 0.3 \text{ for anaerobic digestates and agro-industrial wastes}$$

$$K_{\text{REOM}} > 0.15 \text{ y}^{-1}$$

$$K_{\text{DEOM}} < 230 \text{ y}^{-1}$$

The criteria for setting the partitioning factor for HEOM ( $f_{\text{HEOM}}$ ) to a maximum of 0.3 in the case of digestate and agro-industrial wastes was the same reported in the case of the standard model. The minimum  $K_{\text{REOM}}$  value was set at  $0.15 \text{ y}^{-1}$  according to the RothC modification proposed by Skjemstad et al. (2004).  $K_{\text{DEOM}}$  was set to a maximum of  $230 \text{ y}^{-1}$  in agreement to maximum values found by Thuries et al. (2001) utilizing a 3 EOM pools model for 14 different plant residues, compost and manures. This constraint was not considered in the case of blood meal as the respiration curves presented a very steep initial phase, an indication of a decomposable pool characterized by high degree of decomposability. This is supported by results of Thuries et al. (2001) who found a decomposition rate constant of  $243 \text{ y}^{-1}$  for the labile pool of animal residues. Generally increasing the number of variable parameters increases the precision of the model at the expense of its accuracy and generality (Snipes and Taylor, 2014). The Aikake information criterion (AIC) was developed as an aid to compare and select among different models (Symonds and Moussalli, 2011). It takes into account how well the model fits the data, but

penalizes models with greater numbers of fitted parameters. Therefore it selects the model that has a minimum number of parameters while fitting well the data. In order to select between the two model structure AIC was calculated according to Symonds and Moussalli (2011) as:

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$$AIC = n \left[ \ln \left( \frac{RSS}{n} \right) \right] + 2k \quad (8)$$

Where n = number of cases, RSS: residual sum of squares, k: number of variable parameters + 1.

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According to Symonds and Moussalli (2011) a modified version of the index (corrected AIC: AICC) was calculated because of the small sample size in the case of the present work ( $n/k < 40$ , were n is the number of cases and k is the number of fitted parameters in the most complex model):

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$$AICC = AIC + \frac{2k(k+1)}{n-k-1} \quad (9)$$

Further associated statistics to assess the relative strengths of each candidate model were calculated as suggested by Snipes and Taylor (2014):

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$$\Delta AICC: AICC_{(i)} - AICC_{best} \quad (10)$$

Were  $AICC_{(i)}$  is AICC of method (i) and  $AICC_{best}$  is the lowest AIC value.

$\Delta AICC$  is a measure of each model with respect to the best model (model with lowest AICC). Mazerolle (2006) indicates the following interpretation of this index:  $\Delta AICC < 2$  suggests substantial evidence for the model, values between 3 and 7 indicate that the model has considerably less support, whereas a value  $> 10$  indicates that the model is very unlikely.

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$$ER_{(i)}: Evidence\ Ratio: \exp(-0.5 * \Delta AICC_{best}) / \exp(-0.5 * \Delta AICC_{(i)}) \quad (11)$$

$$LER_{(i)}: \text{Log}_{10}(ER_{(i)}) \quad (12)$$

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LER provides an indication of how much better the best model, i.e. the model with the lowest AICC, is in approximating the true data compared to another model. Snipes and Taylor (2014) set a level of evidence for selecting the model with the lowest AICC of ‘substantial’, ‘strong’, and ‘decisive’ corresponding to LERs between model probabilities greater than 0.5, 1 and 2, respectively.

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### 2.2.3 Optimization of the modified RothC model

In the following stage of the study the modified model was applied to the whole data set, consisting in 224 cumulative respiration curves from amended soils incubated under different conditions. Biochar amended soils ( $n = 4$ ) were excluded from the procedure of parameter estimation due to very low values of CO<sub>2</sub>-C emissions resulting in not statistically robust

respiration curves. Optimization was performed as described in the previous sections by finding the best combination of  
295 variable parameters that results in the best fitting of the respiratory curve.

The accuracy of the model to simulate C mineralization were assessed according to the criteria proposed by Smith et al.  
296 (1996), utilizing the worksheet MODEVAL 2.0 for Windows (Smith and Smith, 2007). The total difference between  
measured and simulated values, expressed as percentage of the mean observed values, was considered by calculating the root  
300 mean squared error (RMSE). The lower limit for RMSE is 0, which denotes no difference between measured and simulated  
values. The association between simulated and measured values (i.e. the percentage of total variance in the observed data  
that is explained by the predicted data) was evaluated by the sample correlation coefficient (R). The error in the simulation  
as a proportion of the measurement was evaluated by the relative error (E), expressed as the mean error percentage over all  
the measurements. The consistent errors or bias in the model was evaluated by the mean difference between measured and  
305 simulated data (M). Because M does not include a square term, simulated values above and below the measurements cancel  
out and so any inconsistent errors are ignored.

### 3 Results

#### 3.1 EOM soil mineralization

As an example of the rate of CO<sub>2</sub> mineralization from soil amended with different EOMs, Fig. 3a shows the dynamics of  
310 CO<sub>2</sub> evolution from the Llano de la Perdiz soil. Range and mean values of net C mineralization for the different EOM  
groups, as defined in the materials and methods section, are reported in Table 5 which summarizes results from all the  
incubations performed utilizing different conditions and incubations carried out under standard laboratory conditions (20 °C,  
40% WHC, 0.5% application rate and 30 days incubation period).

Considering all the incubations performed, the extra CO<sub>2</sub>-C varied in the range 0.01-38.6% of the added EOM-C (Table 5).  
315 According to mean values of net C mineralization obtained under standard laboratory conditions, the different EOM groups  
can be ranked as follows (values in parenthesis are the percentage of added C emitted as CO<sub>2</sub>-C): biochars (0.02%) <  
composts (3.0%) < anaerobic digestates (4.0%) < sewage sludges (4.8%) < agro-industrial wastes (6.3%) < crop residues  
(10.4%) < bioenergy by-products (12.8%) < animal residues (16.8%) < meat and bone meals (21.3%).

In the case of compost, EOM mineralization ranged from 0.9 to 11.1%, with a mean value of 3.7% (Table 5). The total extra  
320 CO<sub>2</sub>-C evolved from the soils amended with meat and bone meals ranged between 7.8 and 38.6%, while in the case of  
bioenergy by-products net CO<sub>2</sub>-C production was in the range 6.9-16.8%. Extremely low values of C mineralization (0.01-  
0.04%) were recorded for biochar amended soil (Table 5). Significant relationship between cumulative net CO<sub>2</sub>-C of  
different EOM group and chemical properties were found only for water soluble N ( $r^2 = 0.70$ ; P<0.01).

#### 3.2 Modification of the model and optimization by incubation data

325 Results of the preliminary phase of the study, in which the possibility to fit soil respiratory curves using the standard model  
and varying the partition coefficients of EOM was investigated, are shown in table 6 reporting mean RMSE values for  
different EOM groups. In general the fitting obtained with the standard model was not satisfactory with an average RMSE  
(i.e. the percentage of error between measured and simulated values) of 21.6% for the 86 examined incubations and a  
maximum of 27% in the case of bioenergy by products. According to Smith and Smith (2007) a value of RMSE lower of  
330 10% could represent a threshold for an acceptable simulation for a particular purpose. Consequently, the model was  
modified as described in section 2.2.2 and the fitting procedure was performed by simultaneously varying the partitioning  
factors and decomposition rates of EOM. Results showed a dramatic increase in the precision of the model, being the  
average RMSE of 2.9% (Table 6). Calculation of AIC and related statistics (Delta AICc -  $\Delta\text{AICc}$ ; logarithm of evidence ratio  
- LER) was performed to evaluate if the increase in the complexity of the model due to the introduction of new parameters  
335 was justified by the increased model goodness of fit. In particular,  $\Delta\text{AICc}$  is a measure of each model relative to the best  
model (i.e. the model with the lower AICc value). Results clearly shows that the modified model was always the best model  
( $\Delta\text{AICc} = 0$ ) and that the standard model was unlikely to give an effective description of respiratory curves as its  $\Delta\text{AICc}$  mean  
value by far exceeds the value of 10 indicated by Mazerolle (2006) as threshold to support model validity.  
Similarly, the evidence ratio compares the AICc of the best model with the AICc of another model and provides a measure  
340 of how much more better is the best model in approximating the real data. In the case of the present study the average LER  
value clearly shows that the modified model was by far better (i.e. 132 times) than the standard one, considering that a  
threshold LER of 2 is considered as a decisive level to select the best model (Snipes and Taylor, 2014).  
The fitting procedure with the modified model was hence applied to all the dataset of incubations and mean, minimum and  
maximum values of statistical indicators utilized to evaluate the model goodness of fit between measured and simulated data  
345 are reported on Table 7. On Tables S1-S6 of Supplement, the pool parameters, the incubation conditions and the statistical  
indicators of model goodness of fit are detailed. Biochar amended soils were omitted from the optimization procedure due to  
very low CO<sub>2</sub> emissions values resulting in not statistically robust respiratory curves.  
As a whole, the modified model was able to fit very well the respiratory response of the amended soils, as indicated by the  
statistical indicators (Table 7; Tables S1-S6 of Supplement). The only exceptions were represented by some soil amended  
350 with a low dose of anaerobic digestate (100 kg N ha<sup>-1</sup>). The mean correlation coefficient (R) for all incubations was 0.995  
and was higher than 0.945 for all but one EOM. The root mean squared error (RMSE) for vine shoots compost, household  
waste compost and bioethanol residue was 4.3%, 2.5% and 3.7%, respectively, while considering all the cases it was 4.5%.  
The relative error (E) ranged between -16.4 and 3.5% (Tables S1-S6 of Supplement). The goodness of fit was also  
underlined by the very low values of M (on average -1.2 µg CO<sub>2</sub>-C g<sup>-1</sup>) (Table 7). As an example of curve fitting, Fig. 3b  
355 depicts measured and simulated net cumulative CO<sub>2</sub>-C evolution for EOMs reported in Fig. 3a.  
Average decomposition rate for EOM and REOM pools were 89 y<sup>-1</sup> and 0.4 y<sup>-1</sup>. Evaluation of pool parameters showed a  
large variability in the composition and decomposition rates of the studied EOMs. Range of different parameters were: 0-  
0.63; 0.21-0.98; 0.06-0.78 for f<sub>EOM</sub>, f<sub>REOM</sub>, f<sub>HEOM</sub> and 11-330; 0.15-2.51 for K<sub>EOM</sub>, K<sub>REOM</sub>, respectively (Tables S1-S6 of

Supplement). Coefficients of variation of the parameters considering all the treatments were 83, 24, 53, 69 and 95% for f<sub>DEOM</sub>, f<sub>REOM</sub>, f<sub>HEOM</sub>, K<sub>DEOM</sub> and K<sub>REOM</sub>, respectively. Pool sizes and decomposition rates were not significantly correlated. No statistically significant relationships were found between pool parameters and chemical properties of different EOM groups. Partition coefficients for DEOM were significantly correlated with cumulative net CO<sub>2</sub>-C ( $r^2 = 0.92$ ; P < 0.01). Calculation of mean pool parameters and associated percent of variation of standard error of all incubations performed with the same EOM type (Table 8) or with the same EOM group (Table 9) showed always a relative standard error smaller than 50%, a threshold value proposed by Robinson (1985) for a statistically acceptable estimation of model parameter, with a single exception in the case of stable compost CMC VII (Table S1 of Supplement).

## 4 Discussion

### 4.1 EOM soil mineralization

The ranking of the different EOM groups according to mean values of net C mineralization was in agreement with results of similar studies on the decomposability of EOMs of different origin and nature (Lashermes et al., 2009; Thuries et al., 2001). Values of net C mineralization (expressed as percentage of added C) for compost amended soil were similar to the ones recorded by De Neve et al. (2003), who measured CO<sub>2</sub>-C values in the range 1.8 - 8.8% of added C for different composts. Values of mean CO<sub>2</sub>-C respiration of meat and bone meals (16.8%) are in agreement with other previous C mineralization studies of residues characterized by low values of C/N ratio, as, for example, 16% and 19% obtained from poultry manure and pig slurry after a 20-day incubation at 22 °C (Levi-Minzi et al., 1990). Regarding by-products from bioenergy production, values of C mineralization in the present study were significantly lower to the ones measured by Cayuela et al. (2010). This dissimilarity can be attributed to the different conditions utilized for the incubation. Nevertheless, the organic residues showed the same relative differences in CO<sub>2</sub> production. The significant correlation between EOM water soluble N and mineralized added C is in agreement with previous studies showing that N availability is an important factor regulating EOM decomposition (Trinsoutrot et al., 2000).

### 4.2 Model modification

The development and optimization of SOC models capable to produce accurate and reliable predictions of EOM decomposition in soils (Karhu et al., 2012) represents an essential prerequisite for their utilization as a tool for an effective management of EOM amendment. RothC considers C input into the soil in the form of EOM only as farmyard manure with fixed partitioning factors of C pools. Fallon (2001) showed that such model structure was not adequate to simulate C dynamics in sludge amended soils. To enhance the ability of RothC to accommodate a wider range of EOMs some authors have proposed to vary the partition coefficients attributed by RothC to EOM pools and this change resulted in a much closer agreement between modeled and measured SOC trends (Falloon, 2001; Peltre et al., 2012). Therefore, in the first stage of the study we investigated the possibility to describe the respiratory curves of amended soil utilizing the same approach.

However, results of the fitting procedure clearly showed that it was not feasible to achieve a satisfactory fitting by only varying the proportion of the EOM pools (mean RSME: 21.6%; n = 86; Table 6). Consequently a modification of the model was proposed based on the hypothesis that its performance would be enhanced by setting specific EOM decomposition rates different from those of plant residues. This corresponds to the introduction of two new pools of organic C entering in to the soil as decomposable and resistant EOM are considered to have different properties in terms of degradability with respect to the correspondent plant residues pools. Results of the fitting procedure performed with the modified model demonstrated a remarkable improvement in the goodness of fit of respiratory curves (average RMSE 2.9%, n = 86; Table 6). The introduction of new parameters (such as the decomposition rate of decomposable and resistant EOM in the case of the present study) generally decreases the bias between simulated and measured values, but this is obtained at the expense of an increase in the complexity of the model. Too many parameters could result in a greater variance in the output of the model due to the uncertainty associated to parameters estimation. Moreover a model with too many parameters hold the risk of over-fitting, i.e. of modelling the random noise in the data rather than the true values. This cause a decrease in the predictive performance or generality of the model when applied to different data set as an over-fitted model is too dependent to the data utilized for its calibration. An ideal model would Calculation of  $\Delta AICc$  and the evidence ratio (Table 6), statistics derived from AIC, clearly showed that the modified model was a far better model in comparison to the standard one in terms of simulation of respiration curves from amended soil. According to AIC derived indexes the benefit obtained by the modified model in terms of decreased bias between measured and simulated data overcompensates the increase in model complexity due to the introduction of new parameters.

In addition to the results of RMSE and AIC, the reliability of the model modification was supported by findings of previous works indicating the limitation of actual RothC in amended soil and the increase in model performance obtained by setting specific decomposition rates for EOM. The standard RothC model has been shown to be insensitive to the variation in the quality of EOM inputs and therefore is not adequate for the simulation of soils amended with EOMs characterized by a huge variability in chemical structure and degradability (Tits et al., 2014). This limitation has been attributed to the fact that it does not distinguish between crop residues and EOM, notwithstanding their widely different nature, and is highlighted by the results of Tits et al. (2014). The authors simulated 30 years of compost addition and the quality of EOM in their work was addressed by calibrating the DPM/RPM ratio with the SOC content, however this ratio encompassed not only EOM quality, but also the quality of input materials (crop residues). Consequently, the calibrated DPM/RPM ratio was site specific, as this ratio depended not only from compost properties, but also by the crop type and management of the site utilized for calibration. The fact that the same pool structure is used to represent organic materials that widely differ in composition and decomposition pattern (e.g. crop residues vs. compost) simplifies model structure, but is likely to generate less accurate results (Cavalli and Bechini, 2011).

Results of previous works also suggest that for a reliable simulation of C mineralization in amended soils there is not only the need to partition EOM into a number of discrete pools, but also to differentiate the quality of EOM from that of crop residues. In particular, Cavalli et al. (2014) underline the relevance to assess different decomposition rates for crop residues

425 and EOM pools, as in the modified RothC, since they found that EOM degradable and resistant pools always decomposed more rapidly than the analogue crop residues pools. Similarly, Borgen et al. (2011) clearly showed that model predictions can be improved by identification of EOM specific decomposition rate. Mueller et al. (2003) demonstrated the inadequacy of the original assumption in the DAISY model of two EOM-pools with predefined constant turnover. Henriksen and Breland (1999a) and Henriksen et al. (2007) presented a model partitioning plant residues in 3 distinct pools (decomposable, 430 structural, resistant) which have distinct, but fixed (i.e. equal for all plant materials) decomposition rates. The only exception is represented by the structural pool which decomposition rate varies as a function of N availability for microbial growth. The need for individual adjustment of the decomposition rate invalidates the fundamental assumption that the specific decay rate constant of each defined pool maybe set a priori because it is uniform across litter qualities and support the fact that residue-specific EOM pool decomposition rate enhances the performances of the model. Further support to the effectiveness 435 of the proposed modification to the model structure presented in this study derives from the work of Incerti et al. (2011) who found that a model with 3 EOM pools satisfactorily described the pattern of litter decomposition. In addition, the authors found an enhancement of the predictive ability of the 3 pools model by varying the decomposition rate of the pool with intermediate degradability as a function of the lignin content. Accordingly, Cavalli and Bechini (2012) and Petersen et al. (2005b) have demonstrated that C simulation in amended soils is increased by a specific EOM parameterization. Finally, it 440 has to be noted that models with a similar complex structure as in the proposed modified RothC (5 different pools of C input to the soil and specific decomposition rates for decomposable and resistant EOM) have been already proposed and successfully validated for amended soils (NC-SOIL: Noirot-Cosson et al., 2016 - CN-SIM: Petersen et al., 2005a; Cavalli and Bechini, 2012).

#### 4.3 Model optimization

445 The results of the respiration curve fitting on the whole data set show that the modified model was able to adequately fit the respiratory response of amended soil, as demonstrated by the average value of RMSE for vine shoots compost (4.3%), household waste compost (2.5%), bioethanol residue (3.7%) and for all the 224 respiratory curve examined in this study (4.5%). As a comparison, Cavalli and Bechini (2011) calibrated the 3-EOM pools of CNSIM model for a reduced range of 450 incubation conditions (3 soils and 5 liquid dairy manures) and obtained an average RMSE of 8.7%. Results suggest that for a reliable simulation of C mineralization in amended soils under laboratory conditions there is not only the need to partition EOM into a number of discrete pools, but also to find specific decomposition rates for such pools.

The calibration of EOM parameters was soil and incubation condition-specific to enable the model to find the best fit of measured data. Consequently, failures to simulate C trends can be attributed exclusively to the inadequacy of the model structure to accurately describe soil respiration. The results of the optimization procedure indicated that the modified model, 455 encompassing additional EOM pools with specific parameters, is able to accommodate the large variability of the tested EOMs in terms of composition and properties. Such variability in EOM quality is indicated by the extended range of values characterizing each pool parameter. These findings support the hypothesis that explicit treatment of EOM heterogeneity

would improve the performances of the RothC model. The lack of correlation between chemical properties of residues and pool parameters is in agreement to the evidence that operationally defined fractions do not precisely match kinetically defined pools. This is mainly due to the fact that the distinct components of organic residues interact with soil components and this modifies their decomposability along the incubation period (Trinsoutrot et al., 2000). Kinetically defined pools take into account such interactions and this represents an advantage in terms of simulation accuracy with respect to the operationally defined pools. The significant relationship between cumulative CO<sub>2</sub> and f<sub>DMP</sub> could be explained on the basis that most of the mineralized EOM-C emitted during the incubation derives from the degradable pool.

Calculation of mean pool parameters for EOM type and EOM group (Tables 7 and 8) indicated that the uncertainty associated to the parameters was always lower than the suggested threshold for statistically acceptable estimation of parameter (standard error of the mean < 50%; Robinson, 1985). These results indicate that the parameter values mainly reflects the EOM properties and that the model is capable to keep the effects of incubation conditions (i.e. type of soil, temperature, soil water content, rate of EOM application) to a minimum. This is in agreement with previous works suggesting that EOM quality is the most important factor affecting organic residue decomposition in soil (Cavalli et al., 2014; Do Nascimento et al., 2012; Karhu et al., 2012;). A low variability associated to mean parameters for EOM group is an indication that this common set of parameters could be utilized to simulate SOC patterns in soil amended with the different EOMs belonging to a specific group with an acceptable error.

#### **4.4 Potential limitations of the proposed model modification and optimization**

Soil organic C modelling is subject to several potential drawbacks and limitations. Due to the aim of this work, only aspects specifically related to the proposed procedure for model modification and optimization will be discussed, namely the suitability of short term incubation to asses EOM pool parameters, issues of model validation for long term scale in field conditions and problems associated with simultaneous fitting of multiples parameters.

##### **4.4.1 Suitability of short term incubations to asses EOM pool parameters and model validation under field conditions**

One of the major concerns about the proposed optimization method is the suitability of short term incubation to adequately characterize EOM in terms of pools of different decomposability, as it was suggested that short term incubation are appropriate only to estimate the mineralization of the more decomposable pools. On the other hand, long term incubations, while providing a more accurate characterization of EOM, are highly demanding in terms of laboratory work, time and space. To date, an agreed minimum incubation period to obtain reliable evaluations of EOM pools has not been established.

Sleutel et al. (2005) underlined that such period depends on the EOM type and the kind of model used to fit the data. They found that for a specific EOM a reliable estimation was obtained with only 16 days at 16 °C and that a second order model required a minimum incubation time of about 50 days at 16 °C for the estimation of EOM stable organic C within less than 3% of the true value for all organic materials. In the case of a parallel first order model, a minimum incubation period of 42 days at 16 °C was necessary to obtain a reliable estimation of pig slurry and compost pools. Such EOMs represent well

490 stabilized materials for which the incubation time is likely to be more important for a reliable parameter estimation with  
respect to more degradable EOMs. Such minimum incubation periods are consistent with the incubation time utilized for  
most of the experiments in this study, when considering the different incubation temperature. It is important to note that one  
possible shortcut to reduce the incubation time needed for a satisfactory fitting is the use of higher temperatures, as the  
mineralization rates significantly increase. As a matter of fact, according to the rate modifying factor for temperature utilized  
495 in RothC, an incubation period of 30 days at 20 °C corresponds to a period of 42 days at 16 °C to mineralize an equal  
amount of CO<sub>2</sub>.

To verify the suitability of the incubation period utilized in this work (30 days) for a satisfactory curve fitting and test the  
dependence of EOM pool parameters from the incubation time, we have utilized an independent data set from a laboratory  
incubation performed at 15 and 25 °C for 300 days with a corn and soybean residues amended soil. We calibrated the EOM  
500 pool parameters considering the whole incubation period (300 days) and a shorter incubation time (30 days for incubations at  
25 °C and 50 days for incubations at 15° C). Results showed that the standard error associated to parameters obtained at  
different incubation time was acceptable (smaller than 50% of parameter value; Robinson, 1985). To estimate the error in  
SOC prediction associated with set of parameters calibrated at different incubation time, we performed long term RothC  
simulations (100 years), involving annual addition of 1 t ha<sup>-1</sup> of EOM-C and utilizing such different set of parameters.  
505 Results showed that the difference in the yearly rate of SOC sequestration was always lower than 7%. We obtained similar  
results utilizing another set of independent data from a 60 days incubation of soil amended with cow manure, pig slurry and  
anaerobic digestates. In this case the difference in C sequestration potential utilizing set of parameters obtained after 30 and  
60 days of incubation was lower than 5%.

The ability to estimate reliable SOM pools utilizing short term incubation data also depends on the accuracy in tracking the  
510 cumulative respiratory curve. The high measurement frequency of the automatic system used in this study (1 measurement  
every 6 hours) improves the precision of the cumulative curve in comparison to standard methodologies (i.e. alkali trapping)  
characterized by a limited number of sampling points. High number of measurements allows outliers to be more easily  
identified and eliminated. A further source of uncertainty is related to the fact that cumulative curves accumulate errors  
515 associated with each sampling point. The system used in this study is characterized by a high precision, as percent relative  
standard deviation of the mean for CO<sub>2</sub> measurement is typically less than 0.5% (Mondini et al., 2010). This minimizes the  
weight that each sampling point has on the total cumulative respiratory response in comparison to traditional measurements  
with alkali trapping, usually taken at large sampling intervals. We consider that the accuracy of measurement system utilized  
in this work compensate the possible limitations associated with short incubation time in comparison incubation performed  
for longer periods, but with less accurate and frequent measurements.

520 The reliability of short incubations in performing acceptable characterization of EOMs pool parameters is also supported by  
several researches. Mueller et al. (2003) used an incubation time of 52 days at 9 °C to calibrate EOM pools of DAISY  
model. It is important to note that an incubation period of 30 days at 20 °C, as the one carried out in our work, would  
correspond to an incubation period of 86 days at 9 °C to mineralize the same amount of CO<sub>2</sub>. De Neve et al. (2003)

incubated several wastes for 39 days at 21 °C to estimate the amount of stable C, a parameter that can be used directly as an input in some C sequestration simulations models. Gale et al. (2006) showed that an incubation period of 28 days at 22 °C was sufficient for determining rate decomposition constants to represent EOM decomposition kinetics to be used in C models. Peltre et al. (2013) calibrated EOM pool parameter of the DAISY model utilizing respiration curves from amended soil incubated at 15 °C for 56 days. Saviozzi et al. (2014) performed an incubation of 25 days at 25 °C to infer the labile and recalcitrant EOM-C pool parameters. Similar conclusions concerning the suitability of short term incubation to obtain reliable EOM characterization were drawn by Beloso et al. (1993), Pedra et al., (2007) and Garcia et al., (1992), utilizing incubation periods of 21, 28 and 42 days, respectively.

As a whole, an incubation time of 30 days and measurements performed with an accurate system could be considered as a reasonable trade off between the accuracy of the information obtained in terms of C mineralization and the demand for saving costs, time and space in the laboratory.

The suitability of short term incubation to estimate reliable EOM pools does not implies that parameters derived from short-term laboratory incubations can be automatically transposed to field condition to simulate long term C dynamics of amended soils. In fact, laboratory incubations are usually performed with sieved soil under optimal constant conditions for microbial activity that could result in quite different EOM mineralization rate with respect to that of a structured soil in a variable field environment. Therefore assimilation of laboratory data in existing models need to be carefully evaluated against field data (Schimel et al., 2006). Nevertheless, several authors have demonstrated that model parameterization obtained in laboratory incubations can be utilized to provide reliable simulation of EOM mineralization under field conditions (Gabrielle et al., 2005; Kaborè et al., 2011; Noirot-Cosson et al., 2016; Vidal-Beaudet et al., 2012). This could be explained on the basis that EOMs composition and properties are the main factors regulating their mineralization in the soil (Cavalli et al., 2014; Do Nascimento et al., 2012; Karhu et al., 2012).

Furthermore, data requirements for model validation under field conditions makes at present this task not feasible to a large degree. As the main objective of the proposed model modification is to increase the ability to capture the large variability in EOM quality, validation at real scale would require data from long term field experiments dealing with a large range of EOM with contrasting properties. This is problematic to date due to the limited amount of suitable data available. While there are several ongoing long term experiments dealing with manure, straw and sludge amendment, there are relatively few experiments reporting C data of soils amended with compost from source separate collection and anaerobic digestates. Furthermore, field experiments with EOM only recently utilized in agriculture (meat meals) or new EOMs from bioenergy by-products are lacking. Moreover, there are no long term field experiments dealing with EOMs characterized by different degree of stability (i.e. compost at different stages of the composting process) that would allow an improved validation of important model parameters such as pool partitioning factors ( $f_{DEOM}$ ,  $f_{REOM}$ ,  $f_{HEOM}$ ) and  $K_{REOM}$ .

Another opportunity for enhanced validation would be the assessment of model ability to discriminate the effect of soil texture on EOM mineralization. Cavalli et al. (2014), in an incubation study, reported no significant differences in EOM decomposition among soils with contrasting texture and attributed this to the soil structure disturbance caused by sample

preparation in incubation experiments that can reduce the physical protection of the applied EOM and decrease a textural effect that might be more explicit under field conditions. Unfortunately experiments concerning EOM application to soils with contrasting texture are very few.

Establishment of field experiments dealing with EOM characterized by contrasting properties and degree of transformation under different environmental and management options would allow for a proper evaluation of model performances in simulating long term SOC dynamics.

#### 4.4.2 Simultaneous fitting of multiple parameters

In RothC, as in many other SOM models, the amount of C associated with each pool decomposes following an exponential decay. In theory these pools are of defined size that should not change with environmental conditions or with the procedure used to fit the model with the data. Cabrera et al. (1995) underlined that pools and rate constants in the exponential models are inversely related which suggests that the same fit to available data could be obtained by increasing one parameter while decreasing the other, a situation formally called equifinality or non identifiability. Research has also shown that increasing the incubation time can increase or decrease the size of a pool while having the opposite effect on rate constants. The possibility to obtain a non identifiable set of parameters also increases with decreasing number of incubation data. These problems with exponential models suggest that they need to be used judiciously when trying to identify pools of defined and fixed size as different combinations of pool size and decomposition rate giving a good fit to respiratory curve may result in significant differences in SOC when the model is run over a long term period.

A possible solution to avoid this pitfall is to have independent controls to constrain parameters estimates (Ahrens et al., 2014). Unfortunately, we did not have such controls for all the incubation data. Nevertheless, we are confident that the optimized parameters represent a univocal set of values. First of all, unique identification of the optimized parameters was sought by maintaining constant HEOM decomposition rate and by imposing constraints to partition coefficients and decomposition rates according to scientific data in order to obtain pool parameters biologically meaningful. As for the influence of incubation time on pool estimates, we have found consistent set of parameters between calibrations performed after 30 and 300 days of incubation. Regarding the impact of few measurements points, this does not apply to our curves characterized by a high frequency measurement. Moreover, even if from a theoretical point of view there is the possibility to obtain different set of parameters leading to accurate simulation, this is limited by the shape of the cumulative curve, as for example the first part of the curve, describing the fast release of CO<sub>2</sub> from the most degradable C, can be adequately described only by a specific combination of k<sub>DEOM</sub> and f<sub>DPEOM</sub> values. Finally, a significant correlation between pool size and decomposition is an indication of model overparameterization and the likelihood to obtain accurate simulations by different combination of the parameters. In the case of the present work such relationships were always not significant and this suggests that the optimized parameters are likely to reflect a unique solution. Simultaneous fitting of several parameters is not unusual in model calibration. As an example, Mueller et al. (2003) and Cavalli and Bechini (2012) simultaneously fitted 5 and 6 parameters, respectively.

## 5 Conclusions

An effective management of organic amendment requires the development of C models able to take into account the quality of added EOM. The main innovative aspects of this work consist in the modification of the RothC model to include additional EOM pools and in their parameterization by model fitting to respiratory curves of amended soils. Results of the study show that the modified and optimized model was able to adequately describe EOM mineralization curves obtained under laboratory conditions and support the hypothesis that defining EOM-specific partitioning factors and decomposition rates improves the simulation ability of the model in amended soils.

Due to the effect of different environmental conditions between laboratory and field conditions, the validation of the modified model with field data represents a necessary step in the model development as a tool to evaluate SOC storage in EOM amended soils in the long term. However, the conceptual changes to the model structure and the potential usefulness of the model are justified through its ability to simulate detailed experimental data. We consider that the capacity of the model to adequately describe mineralization curves of EOM under laboratory conditions represents an essential prerequisite for a reliable C modelling of amended soils, as it demonstrates the ability of the model to resolve the large variability in EOM composition and properties. Furthermore, information derived from the fitting procedure could be useful to identify knowledge gaps on environmental factors and soil processes that regulate EOM decomposition in the soil, suggesting further ways to improve the model.

The findings of the present research indicate that laboratory experiments on EOM decomposition could be useful to improve the simulation of C dynamics in amended soils.

## Authors contribution

Claudio Mondini conceived and designed the experiments, analyzed the data, wrote the paper, prepared figures and/or tables and reviewed drafts of the paper.

Maria Luz Cayuela conceived, designed and performed the experiments, analyzed the data, and reviewed drafts of the paper.

Tania Sinicco performed the experiments and reviewed drafts of the paper.

Flavio Fornasier conceived and designed the experiments, performed the experiments and reviewed drafts of the paper.

Antonia Galvez performed the experiments and reviewed drafts of the paper.

Miguel Angel Sánchez-Monedero conceived, designed and performed the experiments and reviewed drafts of the paper.

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807 **Table 1.** Soil C models utilized for C simulation in amended soils.

Model	EOMs	Yearly application rate	Simulation period (y)	Reference
RothC	Chicken and dairy manure	170-670 kg N ha <sup>-1</sup>	2	Abbas and Fares, 2009
RothC	Cattle and pig FYM and slurry, broiler litter	0.6-7.0 t C ha <sup>-1</sup>	14	Bhogal et al., 2010
RothC	FYM, WS, SS, sawdust, compost	6.5-30 t ha <sup>-1</sup>	11-52	Peltre et al., 2012
RothC	User defined	User defined	User defined	Carbo-PRO web tool, 2012
RothC	FYM	10-15 t fw ha <sup>-1</sup>	25	Yokozawa et al., 2010
RothC	Waste garden compost	5-45 t ha <sup>-1</sup>	15	Tits et al., 2014
C-simulator	Waste garden and household waste compost	30 t ha <sup>-1</sup>	13	Tits et al., 2010
CN-SIM	FYM	2 t C ha <sup>-1</sup>	52	Petersen et al., 2005a
DAISY	Compost	5-10 t dm ha <sup>-1</sup>	50	Stoppler-Zimmer et al., 1999
DAISY	Oilseed rape straw	8 t ha <sup>-1</sup>	2	Mueller et al., 1997
DAISY	WS, maize, blue grass	6 t fw ha <sup>-1</sup>	1	Mueller et al., 1998
DAISY	FYM, WS, sawdust	6.5 t dm ha <sup>-1</sup>	35	Bruun et al., 2003
DAISY	MSW compost, SS, FYM, cattle slurry	200 kg N ha <sup>-1</sup>	50	Peltre et al., 2013
DAISY	Compost	20 t ha <sup>-1</sup>	4.5	Gerke et al., 1999
NCSOIL	MSW compost	10-25 t dm ha <sup>-1</sup>	4	Gabrielle et al., 2005
NCSOIL	FYM, Urban waste compost	2 t C ha <sup>-1</sup>	13	Noirot-Cosson et al., 2016
Cantis	WS	8 t dm ha <sup>-1</sup> (1.2 g C kg <sup>-1</sup> )	1	Garnier et al., 2003
Yasso07	WS, FYM, green manure	2 t C ha <sup>-1</sup>	35	Karhu et al., 2012
DNDC	WS, FYM, compost	0.03-0.5 t C ha <sup>-1</sup>	6	Sleutel et al., 2006
CENTURY	WS, FYM, sawdust, green manure	2 t C ha <sup>-1</sup>	30	Paustian et al., 1992
CQESTR	WS, FYM, corn stalks	6.0-7.5 t dm ha <sup>-1</sup>	34	Plaza et al., 2012
3 pools model	Organic compost	20-40% w:w	5	Vidal-Beaudet et al., 2012

808 EOM: exogenous organic matter; FYM: farmyard manure; WS: wheat straw; SS: sewage sludge; MSW: municipal solid wastes; fw: fresh weight;

809 dm: dry matter; w: weight.

810 **Table 2.** Main physico-chemical characteristics of soils used for incubations.

<b>Location</b>	<b>Country</b>	<b>Soil</b>	<b>Soil use</b>	<b>Sand</b>	<b>Silt</b>	<b>Clay</b>	<b>pH</b>	<b>CaCO<sub>3</sub></b>	<b>SOC</b>	<b>N<sub>TOT</sub></b>	<b>SOC/</b>	<b>C<sub>mic</sub></b>
				<b>code</b>	<b>(%)</b>	<b>(%)</b>	<b>(%)</b>	<b>(g kg<sup>-1</sup>)</b>	<b>(g kg<sup>-1</sup>)</b>	<b>(g kg<sup>-1</sup>)</b>	<b>N<sub>TOT</sub></b>	<b>(μg g<sup>-1</sup>)</b>
S. Martino	Italy	SM	Arable	69	28	3	8.3	740	10.5	1.2	8.8	114
Gorizia	Italy	GO	Meadow	37	48	15	7.8	46	25.4	2.4	10.6	795
Bueris	Italy	BU	Arable	6.0	48	46	7.0	-	32.0	4.5	7.1	269
Lodi	Italy	LO	Meadow	67	21	12	6.7	-	22.0	2.1	10.5	205
Reana	Italy	PE	Arable	55	28	17	6.5	-	15.9	1.2	13.3	118
Ribis	Italy	RI	Arable	54	32	14	4.6	-	8.1	1.3	6.2	65
Codroipo	Italy	CO	Arable	27	58	15	7.1	-	19.0	2.0	9.5	350
Jumilla	Spain	JU	Olive orchard	52	21	27	8.0	415	10.4	1.0	10.4	119
Alquife	Spain	AL	Disused mine	53	30	17	8.5	1.3	2.5	0.9	2.8	10
Llano de la Perdiz	Spain	LL	Arable	32	17	51	7.0	0.5	9.2	1.1	8.4	146

811 SOC: soil organic C; N<sub>TOT</sub>: total N; C<sub>mic</sub>: soil microbial biomass C.

**Table 3.** Description of exogenous organic matter (EOM) used for incubations.

EOM group	EOM group code	EOM type	EOM type description	EOM type code
Compost	CO	Vine shoots compost	compost from vine tree prunings	VSC
		Household waste compost	compost from the separate collection of household organic wastes	HWC
		Green waste compost	compost from green waste	GWC
		CC + WS + MM II_3	3 days old compost from a mixture of cotton cardings, wheat straw and meat and bone meal	CMC II
		CC + WS + MM III_9	9 days old compost from a mixture of cotton cardings, wheat straw and meat and bone meal	CMC III
		CC + WS + MM M_92	92 days old compost from a mixture of cotton cardings, wheat straw and meat and bone meal	CMC M
		CC + WS + BLM + HHM II_3	3 days old compost from a mixture of cotton cardings, wheat straw, blood meal and hoof and horn meal	CBC II
		CC + WS + BLM + HHM III_9	9 days old compost from a mixture of cotton cardings, wheat straw, blood meal and hoof and horn meal	CBC III
Bioenergy by-products	BE	CC + WS + BLM + HHM IV_21	21 days old compost from a mixture of cotton cardings, wheat straw, blood meal and hoof and horn meal	CBC IV
		CC + WS + BLM + HHM M_92	92 days old compost from a mixture of cotton cardings, wheat straw, blood meal and hoof and horn meal	CBC M
Anaerobic digestates	AD	Bioethanol residue	wheat starch by-product from bioethanol production	BR
		Rapeseed meal	meal from biodiesel production	RSM
Meat and bone meals	MM	Pig slurry digestate	anaerobic digestate of pig slurry	PS
		TPOMW + manure digestate	mesophilic anaerobic digestates of two-phase olive mill waste and liquid manure	OW 1
		TPOMW + manure digestate (55 °C)	thermophilic anaerobic digestates of two-phase olive mill waste and liquid manure	OW 2
		Liquid manure digestate	anaerobic digestate of liquid manure	OW 3
Animal residues	AR	TPOMW digestate	anaerobic digestate of two-phase olive mill waste	OW 4
		Bovine MM 1	bovine meat and bone meal	BV1
		Bovine MM 2	bovine meat and bone meal	BV2
		Swine MM	swine meat and bone meal	SW
		Mixed swine bovine MM	mixture of swine and bovine meat and bone meal	SB
Crop residues	CR	Defatted bovine MM	defatted bovine meat and bone meal	DE
		Hydrolyzed leather	organic fertiliser derived from hydrolysed animal proteins	HL
		Blood meal	organic fertiliser from spray drying at low temperatures fresh whole blood from animal processing plants	BLM
Agro-industrial wastes	AW	Horn and Hoof meal	organic fertiliser produced by the drying of horns and hooves from animal processing plants	HHM
		Cotton cardings	waste derived from the process of preparing the fibers of cotton ( <i>Gossypium</i> spp., L.) for spinning	CC
Sewage sludges	SS	Wheat straw	winter wheat ( <i>Triticum aestivum</i> L.) straw collected after harvesting	WS
		Two-phase olive mill waste	semisolid sludge generated during the extraction of olive oil by the two-phase centrifugation system	TPOMW
Biochars	BC	Wastewater sludge	sewage sludge from an urban wastewater treatment plant	WW
		Green waste biochar	biochar produced by continuous slow pyrolysis of green waste at 550 °C	GWB

813 CC: cotton cardings; WS: wheat straw; MM: meat and bone meal; BLM: blood meal; HHM: hoof and horn meal; TPOMW: two-phase olive mill  
 814 waste. Compost: roman numerals refer to stages of the process, numbers refer to days of composting, M: mature compost.

**Table 4.** Main chemical characteristics of exogenous organic matter (EOM) used for incubations.

EOM group	EOM group code	EOM type	EOM type code	pH	OM (%)	TOC (%)	N <sub>TOT</sub> (%)	TOC/N <sub>TOT</sub>	WSC (g kg <sup>-1</sup> )	WSN (g kg <sup>-1</sup> )	NH <sub>4</sub> <sup>+</sup> (mg kg <sup>-1</sup> )	NO <sub>3</sub> <sup>-</sup> (mg kg <sup>-1</sup> )
Compost	CO	Vine shoots compost	VSC	7.7	65.4	34.5	1.5	23.2	9.8	0.6	101	2018
		Household waste compost	HWC	8.3	64.2	34.4	2.3	14.9	5.9	0.7	226	1777
		Green waste compost	GWC	7.5	51.9	28.2	2.2	12.8	6.8	2.2	1400	800
		CC + WS + MM II_3	CMC II	7.9	90.6	42.7	1.6	27.2	23.1	2.7	627	2397
		CC + WS + MM III_9	CMC III	7.9	89.3	41.3	2.1	19.6	28.3	3.7	96	2821
		CC + WS + MM M_92	CMC M	8.1	82.2	39.9	3.5	11.3	12.4	1.8	254	2195
		CC + WS + BLM + HHM II_3	CBC II	7.7	93.3	43.5	1.7	25.7	20.3	1.9	434	1901
		CC + WS + BLM + HHM III_9	CBC III	7.9	91.2	42.9	1.9	22.0	21.9	2.4	281	2256
		CC + WS + BLM + HHM IV_21	CBC IV	7.9	87.5	42.3	2.8	15.2	23.6	2.5	134	2155
		CC + WS + BLM + HHM M_92	CBC M	7.7	83.2	40.6	3.7	10.9	11.3	3.4	59	4169
Bioenergy by-products	BE	Bioethanol residue	BR	4.2	91.9	48.5	6.2	7.8	202.5	12.8	1153	1.9
		Rapeseed meal	RSM	6.2	92.5	45.9	6.0	7.7	74.4	2.4	180	13.4
Anaerobic digestates	AD	Pig slurry digestate	PS	8.5	74.6	37.9	4.4	8.7	38.7	11.6	5361	2.5
		TPOMW + manure digestate	OW 1	8.2	75.8	43.6	3.4	13.0	23.1	1.78	17322	11048
		TPOMW + manure (55 °C) digestate	OW 2	8.1	76.7	48.7	3.5	13.9	25.1	1.81	20118	14318
		Liquid manure digestate	OW 3	8.2	68.6	44.1	3.1	14.5	13.6	0.94	690	7902
		TPOMW digestate	OW 4	7.9	76.9	49.1	3.0	16.1	17.7	1.07	18744	10905
Meat and bone meals	MM	Bovine MM 1	BV1	6.5	70.9	38.5	8.4	4.6	52.1	12.4	631	1692
		Bovine MM 2	BV2	6.3	65.5	33.9	8.2	4.1	35.7	9.0	410	1314
		Swine MM	SW	6.7	78.6	41.4	9.0	4.6	114.5	29.0	530	4721
		Mixed swine bovine MM	SB	5.9	81.8	43.1	9.4	4.6	60.5	17.1	359	4165
		Defatted bovine MM	DE	6.4	59.4	29.9	8.4	3.6	34.3	9.9	435	1714
Animal residues	AR	Hydrolyzed leather	HL	5.2	80.0	42.0	13.2	3.2	34.7	23.2	6360	3135
		Blood meal	BLM	6.7	90.8	52.6	16.4	3.2	118.9	37.9	122	3547
		Horn and Hoof meal	HHM	7.5	80.0	51.3	17.0	3.0	13.7	5.0	1887	1058
Crop residues	CR	Cotton cardings	CC	6.2	88.0	45.2	1.5	30.5	37.8	2.4	303	2005
		Wheat straw	WS	6.5	89.1	49.6	0.3	198	15.7	0.8	66	879
Agro-industrial wastes	AW	Two-phase olive mill waste	TPOMW	5.3	94.1	53.0	1.3	41.1	4.1	1.1	122	0
Sewage sludges	SS	Wastewater sludge	WW	6.8	70.9	38.4	4.8	8.0	7.97	1.64	1677	2286
Biochars	BC	Green waste biochar	GWB	7.5	98.3	86.3	0.3	345	0.1	0.0	17	0.4
		<i>Mean</i>		7.1	80.1	43.8	5.0	30.6	36.3	6.8	2670	3107
		<i>Minimum</i>		4.2	51.9	28.2	0.3	3.0	0.1	0.0	17	0.0
<i>Maximum</i>		8.5		98.3	86.3	17.0	345	203	37.9	20118	14318	

816 EOM: exogenous organic matter; OM: organic matter; TOC: total organic C; N<sub>TOT</sub>: total N; WSC: water soluble C; WSN: water soluble N CC: cotton  
 817 cardings; WS: wheat straw; MM: meat and bone meal; BLM: blood meal; HHM: hoof and horn meal; TPMOW: two-phase olive mill waste.  
 818 Compost: roman numerals refer to stages of the process, numbers refer to days of composting, M: mature compost.  
 819 For EOM group and type code refer to Table 3.

820 **Table 5.** Cumulative extra CO<sub>2</sub>-C emitted in amended soil (% of added C) for exogenous organic matter (EOM) group for all incubations and  
 821 incubations performed under standard conditions.

EOM group	All incubations				Standard conditions incubations*			
	Mean	Min	Max	n	Mean	Min	Max	n
	CO <sub>2</sub> -C (%)				CO <sub>2</sub> -C (%)			
Biochar	0.02	0.01	0.04	4	0.02	0.01	0.04	4
Compost	3.7	0.9	11.1	34	3.0	0.9	6.6	19
Bioenergy by-products	12.9	6.9	16.8	20	12.8	6.9	16.8	10
Anaerobic digestates	3.8	0.8	7.2	27	4.0	0.8	7.1	10
Meat and bone meals	16.8	7.8	38.6	93	21.3	18.1	25.9	3
Animal residues	13.1	5.0	21.1	33	16.8	11.0	21.1	14
Crop residues	8.5	3.0	18.4	10	10.4	5.1	18.4	6
Agro-industrial wastes	10.0	6.0	17.5	3	6.3	6.0	17.5	3
Sewage sludges	4.8	3.8	6.0	4	4.8	3.8	6.0	4
<b>Total cases</b>	<b>228</b>				<b>69</b>			

822 \* 20 °C, 40 % soil water holding capacity, 0.5 % EOM application rate and 30 days incubation period.  
 823

824 **Table 6.** Values of root squared mean error (RMSE),  $\Delta\text{AICc}$  and LER (logarithm of Evidence Ratio) of respiration curves fitting performed with  
 825 standard and modified RothC.  
 826

EOM group	Model	RMSE (%)	$\Delta\text{AICc}$	LER	n
Compost	modified	3.0	0	0	18
	standard	19	586	127	
Bioenergy by-products	modified	2.7	0	0	20
	standard	27	619	134	
Anaerobic digestate	modified	1.9	0	0	13
	standard	17	557	121	
Meat and bone meal	modified	3.0	0	0	12
	standard	21	430	93	
Animal residues	modified	5.1	0	0	9
	standard	21	411	89	
Crop residues	modified	3.4	0	0	8
	standard	16	536	116	
Agroindustrial wastes	modified	1.9	0	0	2
	standard	19	761	165	
Sludges	modified	1.5	0	0	4
	standard	22	1029	223	
<b>Average</b>	<b>modified</b>	<b>2.9</b>	<b>0</b>	<b>0</b>	<b>86</b>
	<b>standard</b>	<b>22</b>	<b>616</b>	<b>132</b>	

827 EOM: exogenous organic matter;  $\Delta\text{AICc}$ :  $\text{AICc}_{(i)} - \text{AICc}_{\text{best}}$ , AICc: Aikake information criterion corrected for small sample size,  $\text{AICc}_{(i)}$ , AICc of method  
 828  $_{(i)}$ ,  $\text{AICc}_{\text{best}}$ ; lowest AICc value; n: number of cases.  
 829

830

831 **Table 7.** Mean, minimum and maximum values of statistical indicators of model goodness of the fit between measured and simulated data (n =  
 832 224).

	<b>RMSE</b>	<b>R</b>	<b>E</b>	<b>M</b>
	%	%		$\mu\text{g CO}_2\text{-C g}^{-1}$
<b>Mean</b>	4.5	0.995	-1.1	-1.2
<b>Min</b>	0.7	0.794	-16.4	-44.8
<b>Max</b>	37.2	0.9999	3.5	2.9

833 RMSE: root mean square error; R: sample correlation coefficient; E: relative error M: mean difference between measured and simulated data.

**Table 8.** Mean RothC exogenous organic matter (EOM) pool parameters for different EOM types.

EOM group	EOM type code	N.	Exc.	Inc.	$f_{DEOM}$	$f_{REOM}$	$f_{HEOM}$	$K_{DEOM}$	$K_{REOM}$	$f_{DEOM}$	$f_{REOM}$	$f_{HEOM}$	$K_{DEOM}$	$K_{REOM}$	$f_{DEOM}$	$f_{REOM}$	$f_{HEOM}$	$K_{DEOM}$	$K_{REOM}$	
							Mean value					Standard error (SE)					Coefficient of variation of SE (%)			
Compost	VSC	4	0	4	0.01	0.39	0.59	119	0.23	0.005	0.032	0.03	42.09	0.04	41.1	8.1	5.7	35.3	19.2	
	HWC	14	0	14	0.02	0.33	0.65	78	0.28	0.002	0.018	0.02	13.46	0.05	8.5	5.3	2.7	17.3	18.8	
	GWC	2	0	2	0.01	0.31	0.69	145	0.45	0.001	0.043	0.04	45.50	0.07	10.0	14.0	6.6	31.5	15.9	
	CMC II	2	0	2	0.05	0.87	0.08	42	0.34	0.009	0.025	0.02	3.18	0.03	16.6	2.9	20.3	7.6	8.2	
	CMC III	2	0	2	0.06	0.63	0.32	29	0.35	0.005	0.006	0.00	1.20	0.02	8.2	1.0	0.5	4.1	6.6	
	CMC M	2	0	2	0.004	0.26	0.74	83	0.46	0.002	0.047	0.04	21.77	0.11	58.3	18.1	6.0	26.1	22.8	
	CBC II	2	0	2	0.08	0.73	0.19	22	0.28	0.014	0.015	0.00	0.24	0.05	17.4	2.1	0.6	1.1	17.2	
	CBC III	2	0	2	0.07	0.62	0.31	20	0.26	0.001	0.031	0.03	1.47	0.10	2.0	5.0	9.8	7.4	39.3	
	CBC IV	2	0	2	0.05	0.56	0.39	16	0.22	0.001	0.012	0.01	0.66	0.01	2.2	2.2	2.6	4.0	5.1	
	CBC M	2	0	2	0.01	0.31	0.69	145	0.45	0.001	0.043	0.04	45.50	0.07	10.0	14.0	6.6	31.5	15.9	
Bioenergy by products	BR	6	1	5	0.12	0.88		129	0.47	0.007	0.007		7.36	0.07	5.8	0.8		5.7	14.4	
	RSM	14	2	12	0.13	0.87		76	0.27	0.007	0.007		6.51	0.03	5.5	0.8		8.5	9.6	
Anaerobic digestates	PS	14	2	12	0.05	0.70	0.25	57	0.25	0.004	0.024	0.02	4.92	0.03	7.4	3.5	9.1	8.6	12.9	
	OW	13	0	13	0.01	0.74	0.25	220	0.20	0.002	0.018	0.02	23.34	0.03	13.7	2.5	7.2	10.6	13.5	
Meat and bone meals	BV1	26	0	26	0.19	0.81		78	0.47	0.011	0.011		2.68	0.08	5.5	1.3		3.4	16.7	
	SB	16	0	16	0.29	0.71		56	0.33	0.043	0.043		5.51	0.06	14.8	6.0		9.8	17.9	
	BV2	40	4	36	0.16	0.84		81	0.29	0.005	0.005		2.24	0.03	3.3	0.6		2.8	10.3	
	DE	10	0	10	0.32	0.68		59	0.39	0.031	0.031		5.29	0.12	9	5		9	31.5	
Animal residues	HLM	3	0	3	0.15	0.85		67	0.67	0.030	0.030		19.82	0.22	19.7	3.6		29.4	32.5	
	BLM	15	1	14	0.10	0.90		164	0.40	0.012	0.012		14.27	0.07	11.2	1.3		8.7	17.0	
	BLM2	3	0	3	0.13	0.87		217	0.90	0.034	0.034		50.12	0.16	25.3	3.9		23.1	17.3	
	HHM	12	2	10	0.23	0.77		16	0.19	0.027	0.027		1.42	0.02	11.7	3.6		8.6	9.6	
Vegetal residues	CC	5	1	4	0.05	0.95		87	0.35	0.012	0.012		24.14	0.11	25.0	1.2		27.9	30.1	
	WS	5	1	4	0.05	0.95		39	0.19	0.011	0.011		4.34	0.04	23.1	1.1		11.2	18.2	
Agro-industrial wastes	TPOMW	3	1	2	0.04	0.78	0.19	126	0.56	0.011	0.011	0.0001	6.76	0.25	28.7	1.5	0.1	5.4	44.3	
Sewage sludge	WW	4	0	4	0.04	0.96		63	0.22	0.002	0.002		7.75	0.04	4.7	0.2		12.3	18.5	
<b>Total (N.)</b>		223	15.0	208	0.09	0.70	0.41	86	0.37						mean	15.0	4.2	6.0	13.5	18.6
<b>Total (%)</b>		100	6.7	93.3	0.004	0.26	0.08	16	0.19						minimum	2.0	0.2	0.1	1.1	5.1
					0.32	0.96	0.74	220	0.90						maximum	58.3	18.1	20.3	35.3	44.3

835 EOM: exogenous organic matter; N.: number of incubations; Exc./Inc.: number of incubations excluded/include from the mean calculation;

836 DEOM: decomposable EOM; REOM: resistant EOM; HEOM: humified EOM; f: partitioning factor; K: decomposition constant rate ( $\text{y}^{-1}$ ).

837 For EOM group and type code refer to Table 3.

838 **Table 9.** Mean RothC exogenous organic matter (EOM) pool parameters for different EOM groups.

EOM group	EOM group code	N.	Excl.	Incl.	Mean value				Standard error (SE)				Coefficient of variation of SE (%)						
					f <sub>DEOM</sub>	f <sub>REOM</sub>	f <sub>HEOM</sub>	K <sub>DEOM</sub>	K <sub>REOM</sub>	f <sub>DEOM</sub>	f <sub>REOM</sub>	f <sub>HEOM</sub>	K <sub>DEOM</sub>	K <sub>REOM</sub>	f <sub>DEOM</sub>	f <sub>REOM</sub>	f <sub>HEOM</sub>	K <sub>DEOM</sub>	K <sub>REOM</sub>
Compost	CO	34	0	34	0.03	0.44	0.53	79	0.30	0.004	0.031	0.034	11	0.027	14.6	6.9	6.4	13.8	8.8
Bioenergy by-products	BE	20	3	17	0.13	0.87		92	0.33	0.006	0.006		8	0.035	4.3	0.6		8.5	10.4
Anaerobic digestates	AD	27	2	25	0.03	0.74	0.25	220	0.20	0.004	0.018	0.018	23	0.027	14.9	2.5	7.2	10.6	13.5
Meat and bone meals	MM	93	4	89	0.21	0.79		74	0.41	0.011	0.011		2	0.039	5.1	1.4		2.8	9.5
Animal residues	AR	33	3	30	0.15	0.85		110	0.41	0.015	0.015		16	0.056	10.0	1.8		14.5	13.7
Crop residues	CR	10	2	8	0.05	0.95		63	0.27	0.007	0.007		15	0.060	15.7	0.8		23.2	22.0
Agro-industrial wastes	AW	3	1	2	0.04	0.78	0.19	126	0.56	0.011	0.011	0.0001	7	0.249	28.7	1.5	0.1	5.4	44.3
Sewage Sludges	SS	4	0	4	0.04	0.96		63	0.22	0.002	0.002		8	0.040	4.7	0.2		12.3	18.5
<b>Total (N.)</b>		224	15	209										mean	12.2	2.0	4.6	11.4	17.6
<b>Total (%)</b>		100	6.7	93										minimum	4.3	0.2	0.1	2.8	8.8
														maximum	28.7	6.9	7.2	23.2	44.3

839 EOM: exogenous organic matter; N.: number of incubations; Exc./Inc.: number of incubations excluded/included from the mean calculation;

840 DEOM: decomposable EOM; REOM: resistant EOM; HEOM: humified EOM; f: partitioning factor; K: decomposition constant rate ( $y^{-1}$ ).

841 For EOM code refer to Table 3.

## Figure captions

Figure 1. Diagram of the automated chromatographic system for soil CO<sub>2</sub> sampling and  
845 measurement.

Figure 2. Structure of the standard (a) and modified (b) RothC model. DPM: decomposable plant  
material; RPM: resistant plant material; EOM: exogenous organic matter; DEOM: decomposable EOM;  
REOM: resistant EOM; HEOM: humified EOM; BIO: soil microbial biomass; HUM: humified soil organic matter; IOM: inert organic matter; f: partitioning  
850 factor; K: decomposition constant rate ( $y^{-1}$ ).

Figure 3. Rate (a) and net cumulative measured and simulated (b) CO<sub>2</sub> emission from Llano de la  
Perdiz soil amended with amendments of different degree of degradability during a 30 days  
laboratory incubation. For the rate of respiration only the first 10 days of the incubation are  
reported. Simulated net cumulative respiration curves are represented as dotted lines.  
Respiratory curves are presented on Y axis with different scale for better visualization.  
855

Figure 1

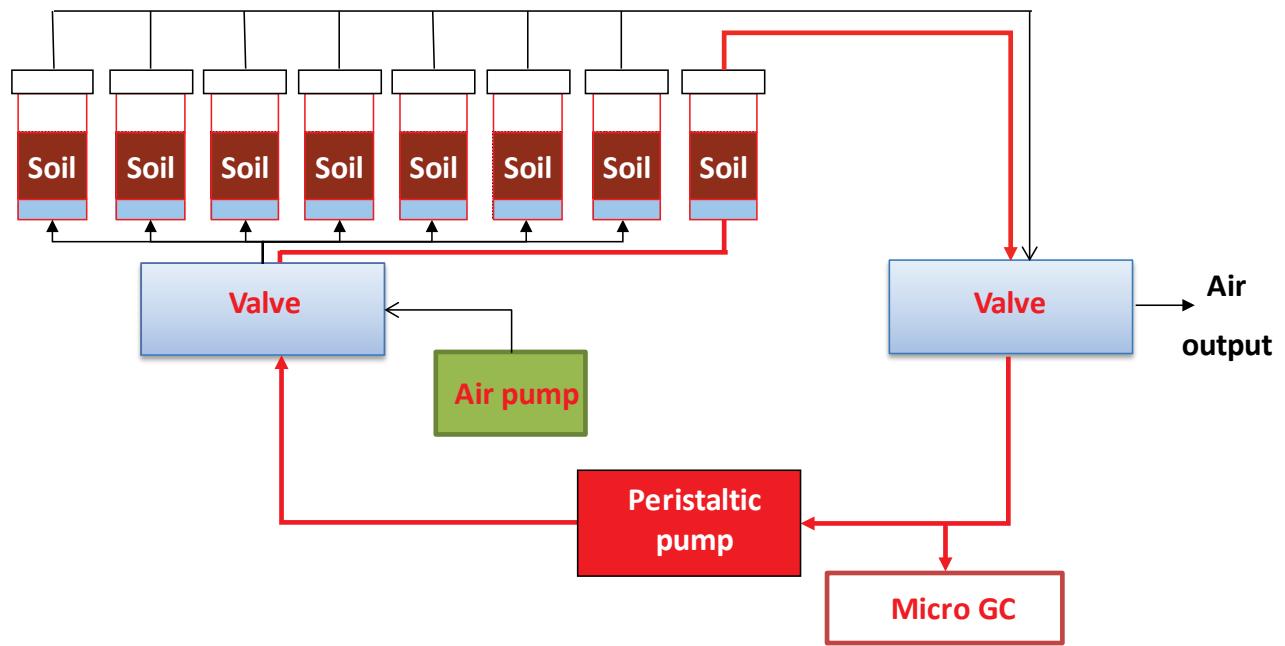


Figure 2

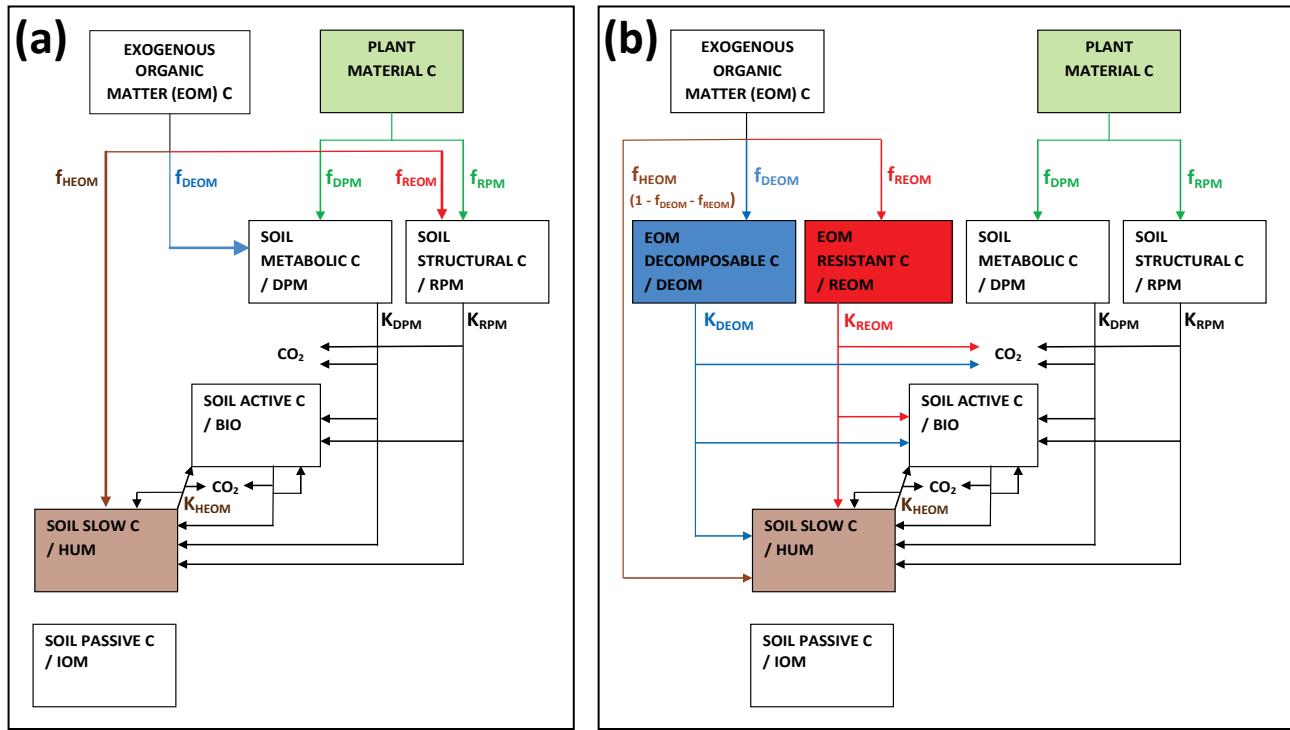


Figure 3

