

## ***Interactive comment on “Can ocean community production and respiration be determined by measuring high-frequency oxygen profiles from autonomous floats?” by Christopher Gordon et al.***

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Received and published: 30 April 2020

In this paper by Gordon et al., the authors present and discuss (1) a method to determine effective response times from consecutive up- and downcasts, and (2) how to discern between physically- and biologically-driven diel variations in  $O_2$  observations and the limits to derive gross primary production GPP and respiration R from them.

The paper is structured logically and is written excellently. The math around the time response correction is particularly well presented, and the time response part is applicable not only to  $O_2$  optode sensors and BGC-Argo floats, but to any sensor on any profiling platform. The discussion around GPP/R estimation shows a

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high degree of critical assessment of sensor data accuracy, which is a good example and should happen more often. I recommend to publish this paper with minor revisions.

Comments:

(1) The authors refer to Bittig et al. (2014), who studied oxygen optode time response and found flow and temperature to be the main factors modulating response times. As the authors write, flow around the optode modulates the water boundary layer thickness through which  $O_2$  has to diffuse, thus slowing down sensor response. The authors discuss the impact of flow and conclude that flow variations are of second order importance in their application and that they can assume a uniform (or at least common) flow regime and thus one effective response time. Given the variations in profiling speed, varying over an order of magnitude, this could be argued. But the desire for simplicity and the results give justification to this approach.

What the authors do not discuss and do not include by using a uniform effective  $\tau$  is the variation in response time induced by temperature. Bittig et al. (2014) show that a temperature change from 5 °C to 25 °C (deep vs. surface waters in the Gulf of Mexico) can reduce the response time by 33 % within the same profile. Could that explain some part of (a) the uncertainty in the calculation of one uniform, effective response time for the entire profile (e.g., table 2) and (b) leading to incomplete correction of the time response thus adding uncertainty/bias in the  $O_2$  gradient region and preventing the GPP/R analysis in part 4?

By using a simple two-layer diffusional model, Bittig et al. (2014) show that the temperature effect can be removed, leaving one parameter (the boundary layer thickness) to characterize the temperature-dependent response time at a given flow regime.

Can the authors (I) modify their approach to not neglect the temperature influence on response time? Bittig and Körtzinger (2017) provide the data of Bittig et al. (2014) as

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look-up table (LUT) in their supplementary material (`T_IL_tau_3830_4330.dat`<sup>1</sup>). The authors could either use this LUT to find the corresponding boundary layer thickness for their effective response time at a certain temperature, and modify the response time applied for the correction according to the LUT's temperature dependence. Or, they could optimize for an effective boundary layer thickness  $l_L$  instead and apply the response time for correction according to the LUT.

Can the authors then (IIa) discuss whether that reduced the spread in response times per float, and (IIb) whether that reduced RMSEs between up- and downcasts and whether physical imprints on diel  $O_2$  variations (in isopycnal space) are reduced, thus permitting the GPP/R analysis of part 4? If that is not the case, can the authors explain or speculate why?

The authors write that they do not strive to fully characterize and understand the flow around the sensor. Neither do I. The suggestion to optimize for one effective boundary layer thickness instead of one effective response time means only to take the demonstrated temperature-dependence of the response time into account.

(2) Barone et al. (doi: 10.1002/lom3.10340) recently published a work where glider measurements were used to estimate GPP/R from diel  $O_2$  variations in the subtropical North Pacific. The method proposed in that work provides daily GPP/R values and Barone et al. state that the method “resolved variability on time scales of approximately 1 week”. Could the authors apply these methods to their data, or comment on Barone et al.'s findings?

(3) Data availability: The float data are not available under the link provided. <https://data.gulfresearchinitiative.org/data/R5.x275.000:0002> gives some float data,

```
1in=dlmread('T_IL_tau_3830_4330.dat');    IL=in(1,2:end);    T=in(2:end,1);    tau100=in(2:end,2:end);  
[IL,T]=meshgrid(IL,T); clear in
```

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however, only for the first set of continuous mode profiling during the first couple of days, as far as I can tell. Moreover, they do not include measurement times, which the authors rightfully state as being important.

(4) The authors provide code to re-apply their approach to determine response times to other or similar data, which is excellent. However, the authors should also comment on the parameters they used. Notably, whether they used the full depth range to find the optimal  $\tau$  (implicit from the paper, as not stated otherwise), or limited the optimization to the upper  $O_2$  gradient (default depth range of 25-175 dbar in the code).

(5) The standard deviations of the in-air gains are very high, about an order of magnitude higher than observed usually for other (APEX) floats (see Argo, Bittig et al. 2018, or others)! What's the reason for this large scatter? Do the authors still have confidence in the in-air corrections given these large variations? The optode attachment on a short stalk looks comparable to other (APEX) floats.

Remarks:

- p.3 l.26: “No depth binning was performed.” Depth resolution should be stated here.
- p.5 table 1: Please verify numbers. E.g., f7941 has about the same  $N_{cont}$  as f7939 but 100 profiles more in total. Still about the same start and end date? This does not match the float operation modes.
- Check references. Bittig and Körtzinger (2016) (discussion paper) should be Bittig and Körtzinger (2017) (published paper).
- p.12 l.30: “based on theoretical considerations of flow-dependent boundary layer thickness” Not quite. Response times of Bittig and Körtzinger (2017) are based on an in-situ comparison between two optodes, one with well-defined time response (pumped

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optode), the other one with variable response time (unpumped) as in this study. Response time determination was empirical as in this study. The boundary layer thickness as well was empirical and a mere tool to eliminate the temperature-dependence. Moreover, the range of response times in the application of Bittig and Körtzinger (2017) is stated as 60-95 s. The range of 70-140 s given in Bittig et al. (2018) covers the global range of possible scenarios, including very cold, polar surface waters with longer response times. The present setting in the Gulf of Mexico is better comparable to the subtropical setting of Bittig and Körtzinger (2017).

- p.13 l.41: “the impact of this difference on the correction is likely small” Speculation. rather: “unknown”?

- Figure 8: Why was the mean taken from 25-150 dbar and not from the surface-150 dbar?

Typos:

- p.12 l.37: -that

- p.16 l.26: -and

- p.21 eq.C2 and C3: Can you check the sign in the numerator?

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Interactive comment on Biogeosciences Discuss., <https://doi.org/10.5194/bg-2020-119>, 2020.